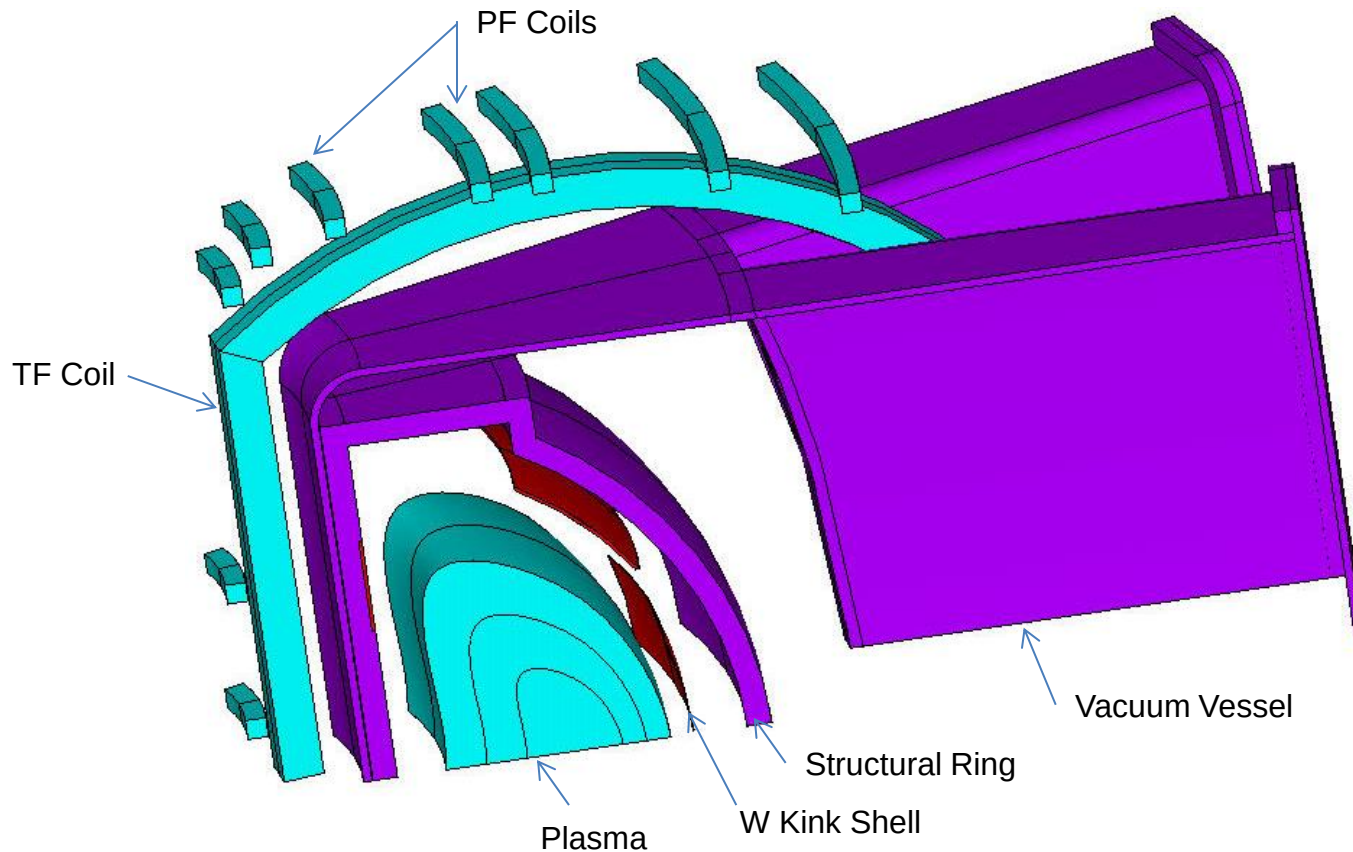


Revised E&M Disruption Calculations

Jake Blanchard
UW-Madison
September 2013

Recent Modeling Enhancements

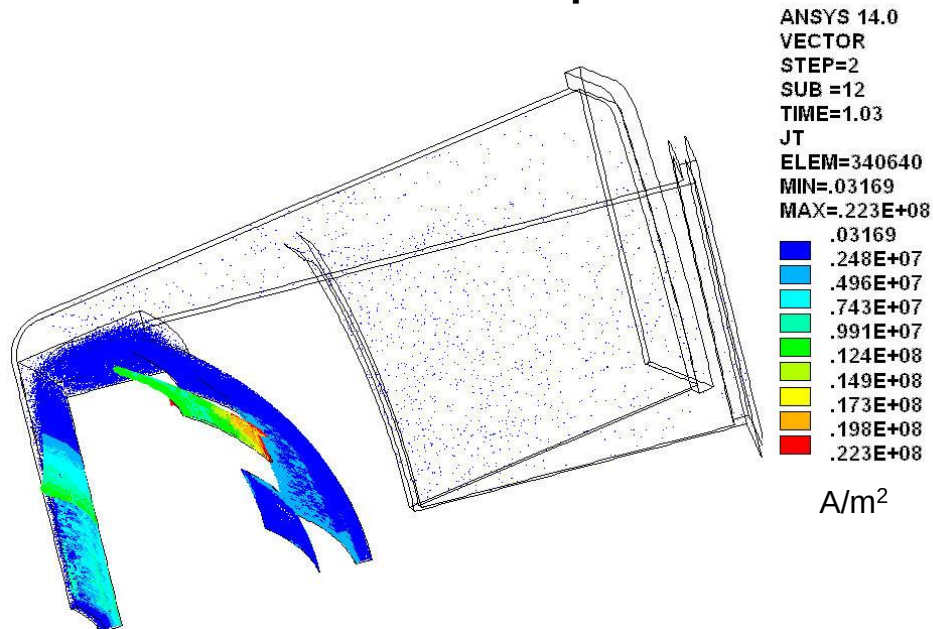
- Realistic plasma shape and current distribution incorporated
- Toroidal field effects included in structural analysis
- Inclusion of tungsten stabilizing and kink shells



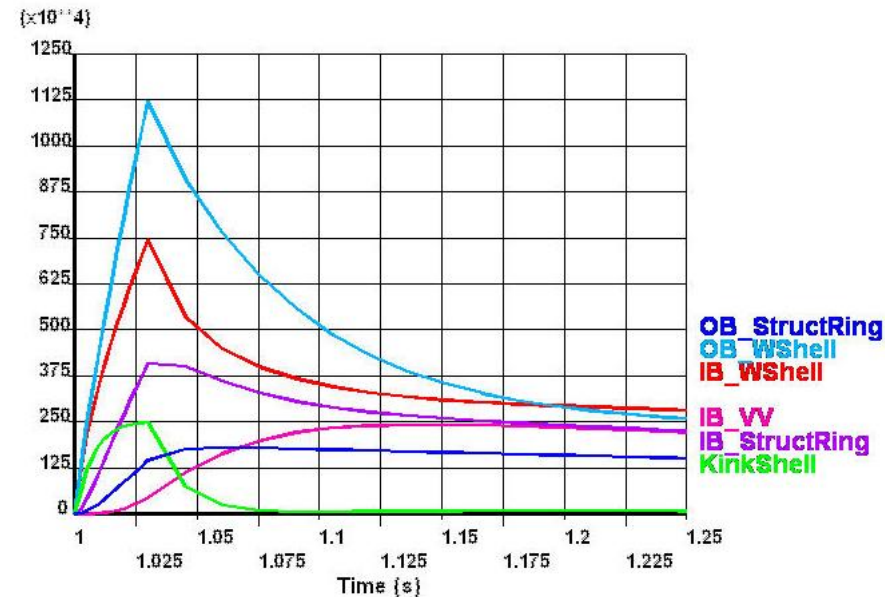
Current Densities at End of Plasma Ramp-down

- Plasma assumed to ramp down in 0.03 sec.

At End of Plasma Ramp-down

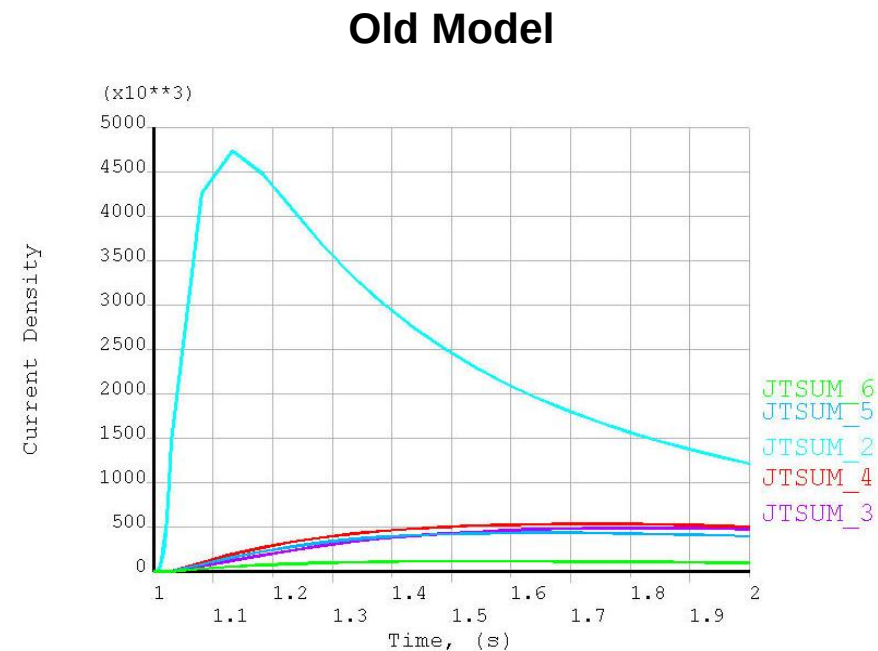
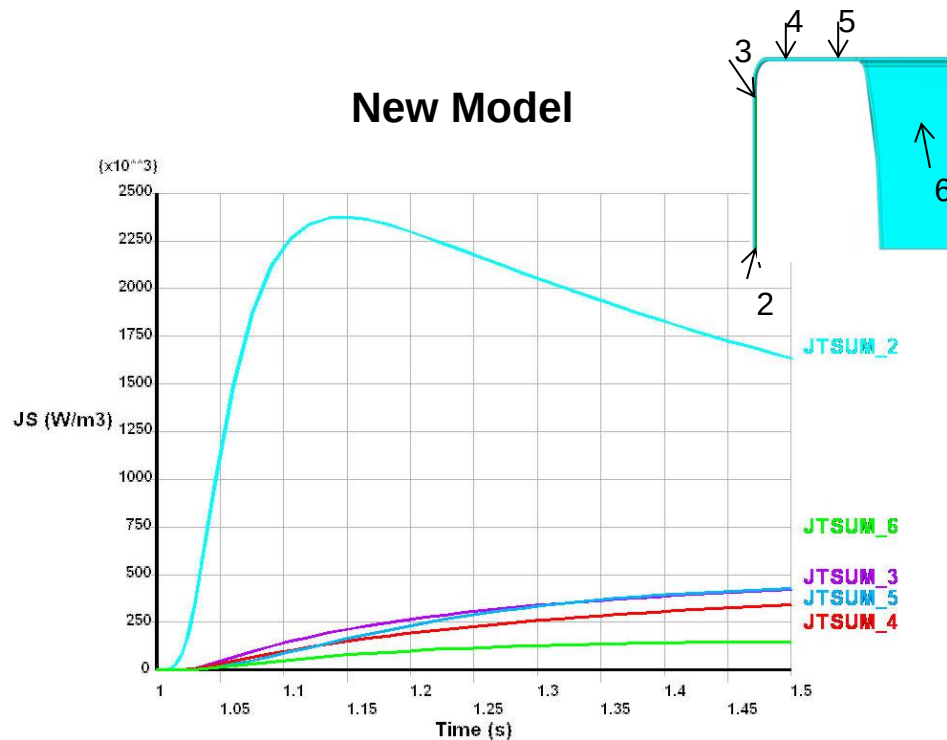


Time history in Various Components



Comparison of VV Current Densities for Old and New Models

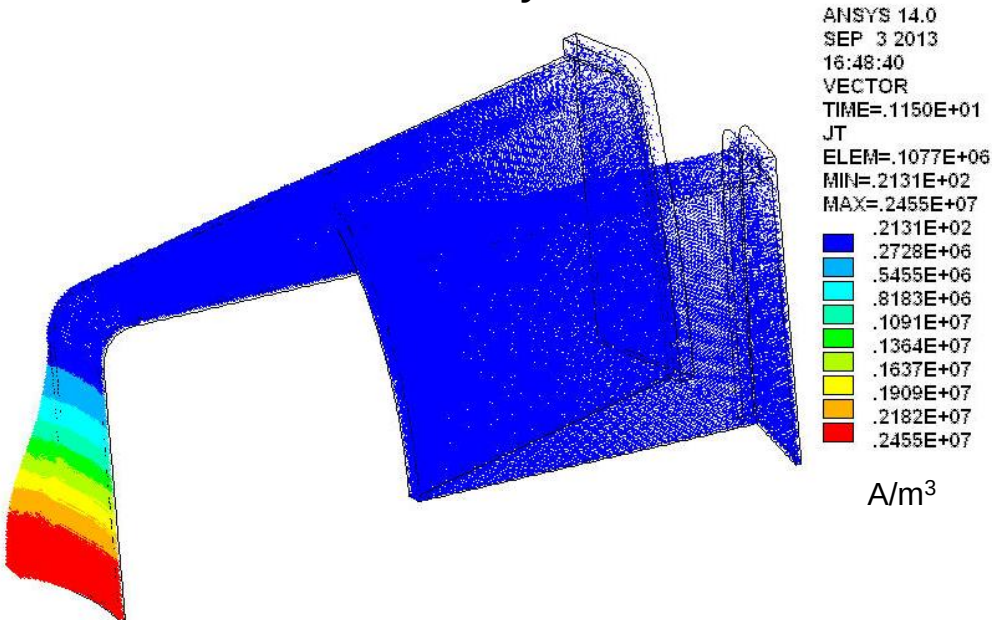
- Current density at IB centerline cut in half, but similar at other points.
- Largest effect is change in plasma current shape



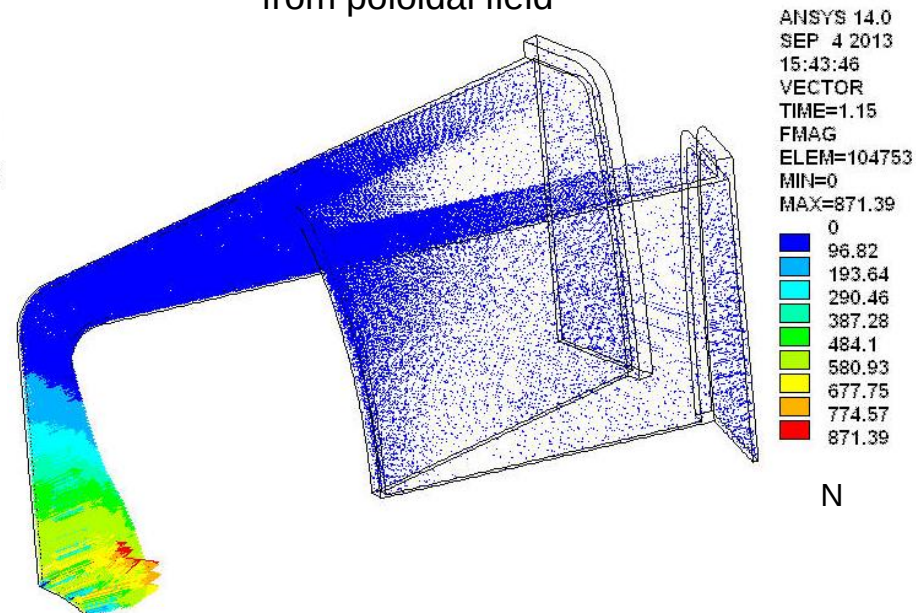
Maximum Current Density and Poloidal Field Magnetic Forces

- Maximum currents occur ~0.15 s after start of plasma ramp down.
- Maximum currents and magnetic forces occur at inboard region near mid-plane.

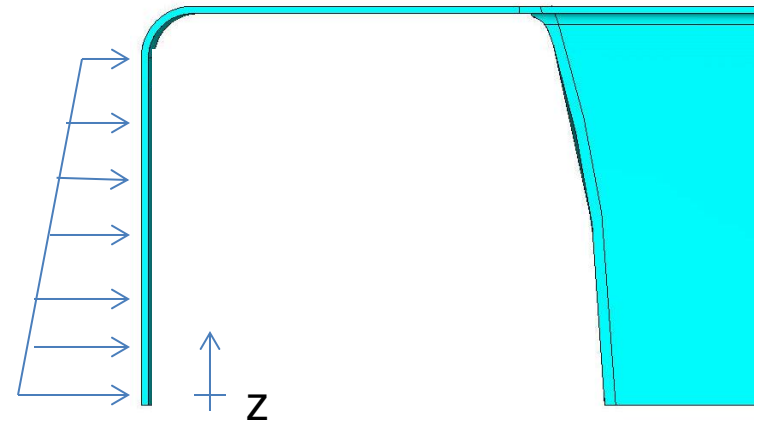
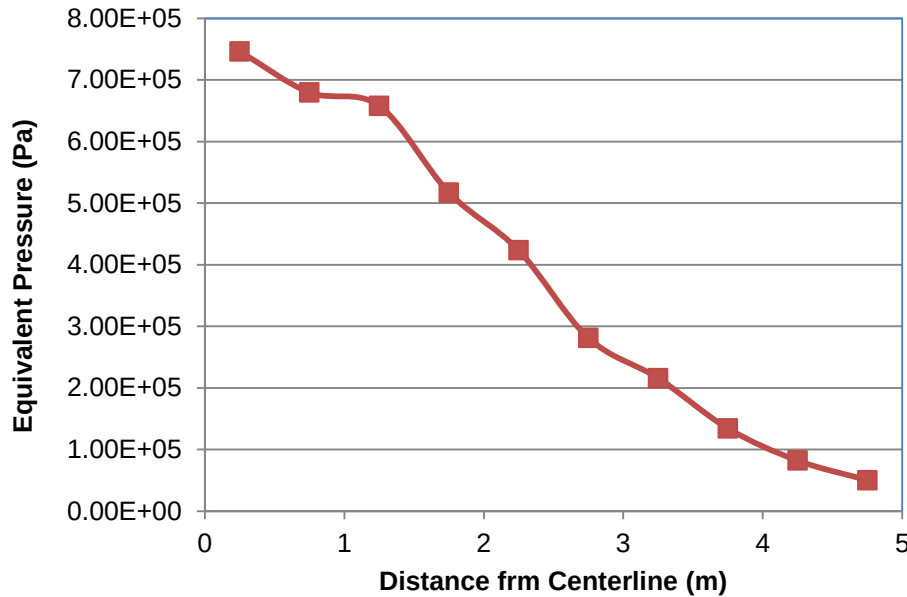
Current Density



Magnetic Forces
from poloidal field



Magnetic Forces Approximated as Equivalent Pressure on Inner Wall of the Vacuum Vessel

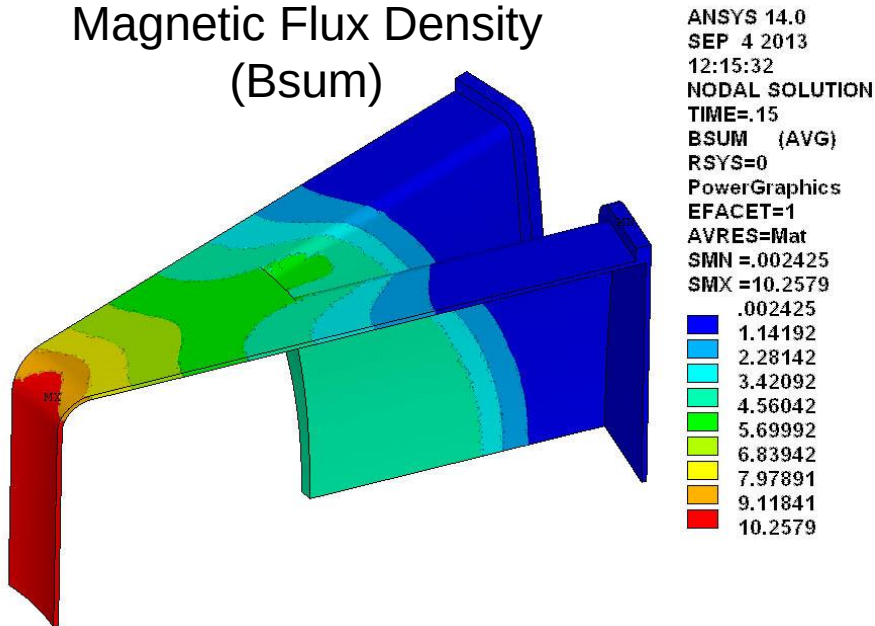


“old” pressure peaked at 5 MPa

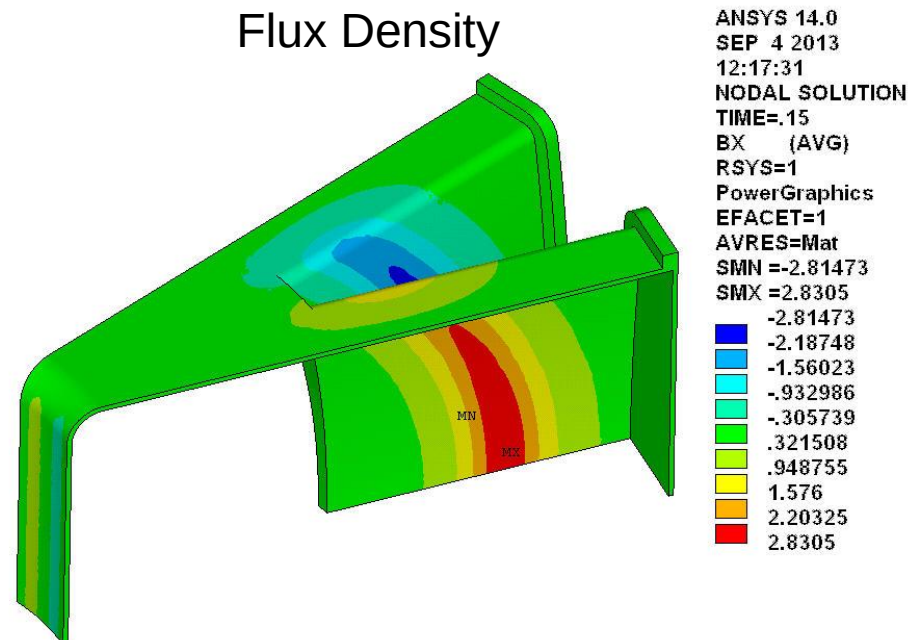
Magnetic Flux Density in VV from Toroidal Field Coils

- Magnetic fields from poloidal and toroidal coils cannot be modeled simultaneously with a sector model (incompatible b.c.'s)
- Hence, we calculated them separately and manually calculated resulting forces

Magnetic Flux Density
(Bsum)



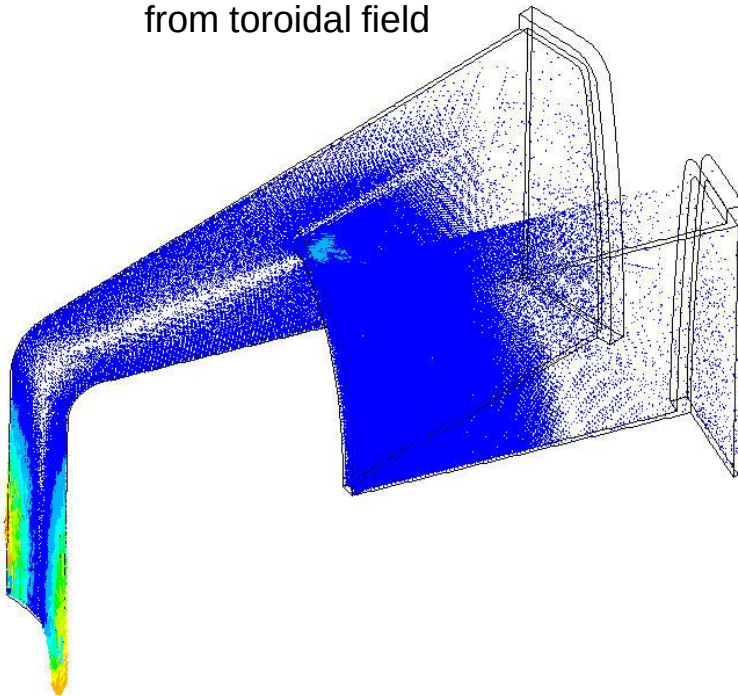
Radial Component of Magnetic
Flux Density



Magnetic Forces From Toroidal Field

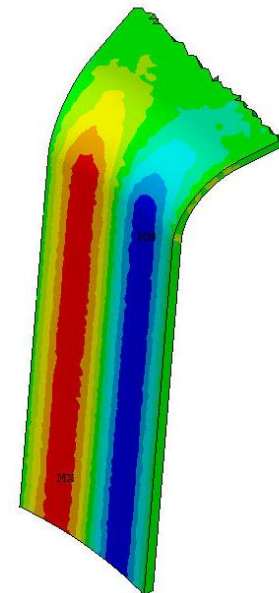
- Maximum forces result from radial variation in field around inboard toroidal coil.
- Forces are perpendicular to forces from poloidal field.

Magnetic Forces
from toroidal field



ANSYS 14.0
AUG 29 2013
15:57:24
VECTOR
TIME=.15
FMAG
ELEM=141276
MIN=.536E-15
MAX=418.37
.536E-15
46.4855
92.971
139.457
185.942
232.428
278.913
325.399
371.884
418.37

Radial Component of Magnetic
Flux Density

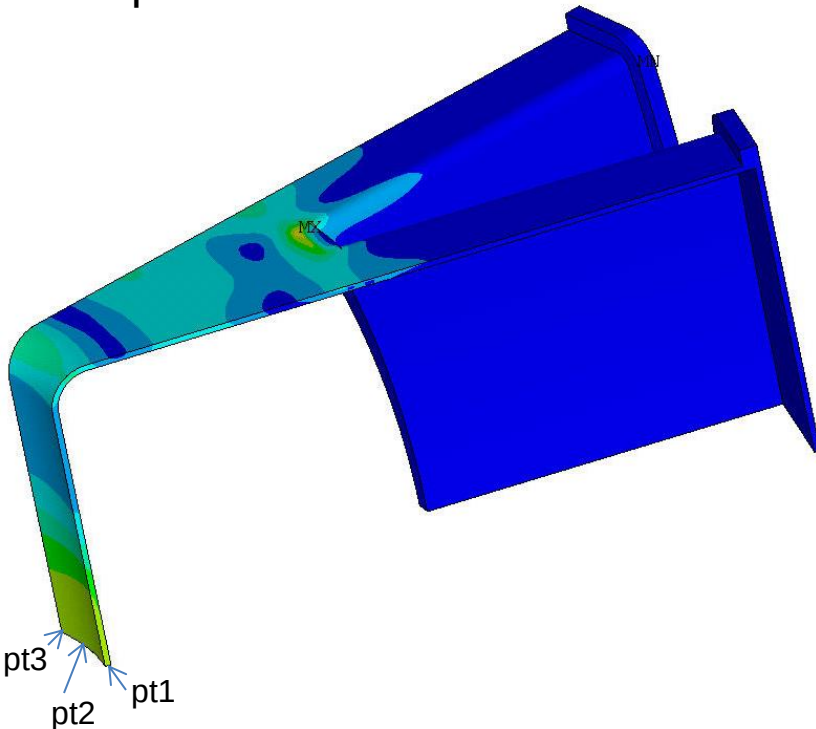


ANSYS 14.0
SEP 4 2013
17:09:49
NODAL SOLUTION
TIME=.15
BX (AVG)
RSYS=1
PowerGraphics
EFACET=1
AVRES=Mat
SMN =-.445998
SMX =.452651
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-.346149
-.246299
-.146449
-.046599
.053251
.153101
.252951
.352801
.452651

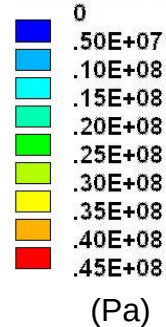
Transient Structural Analysis Results

- Poloidal and toroidal force results linearly combined.
- Inclusion of toroidal field forces produces some asymmetry in stress results.
- Ignore inertial effects.

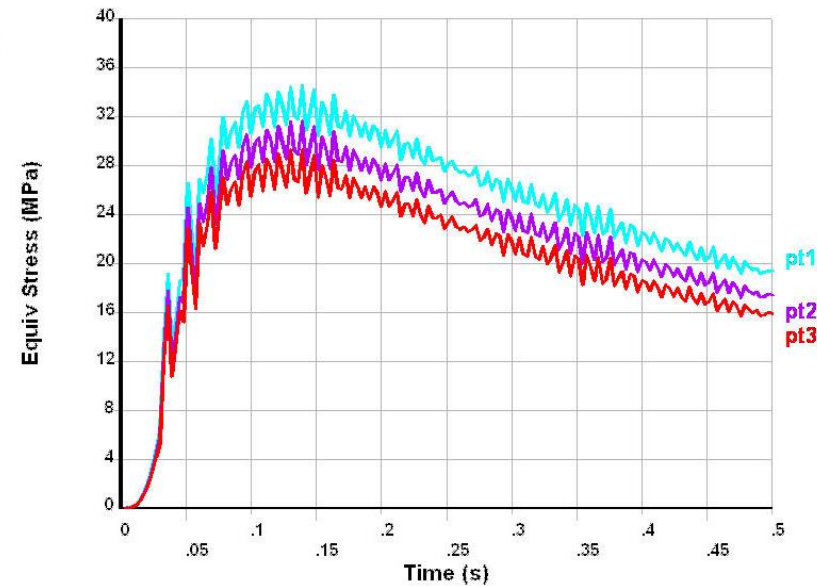
Equivalent Stresses at $t=0.15s$



ANSYS 14.0
SEP 5 2013
12:12:30
NODAL SOLUTION
STEP=20
SUB =5
TIME=.15E+00
SEQV (AVG)
PowerGraphics
EFACET=1
AVRES=Mat
DMX =.26E-02
SMN =.65E+04
SMX =.16E+09

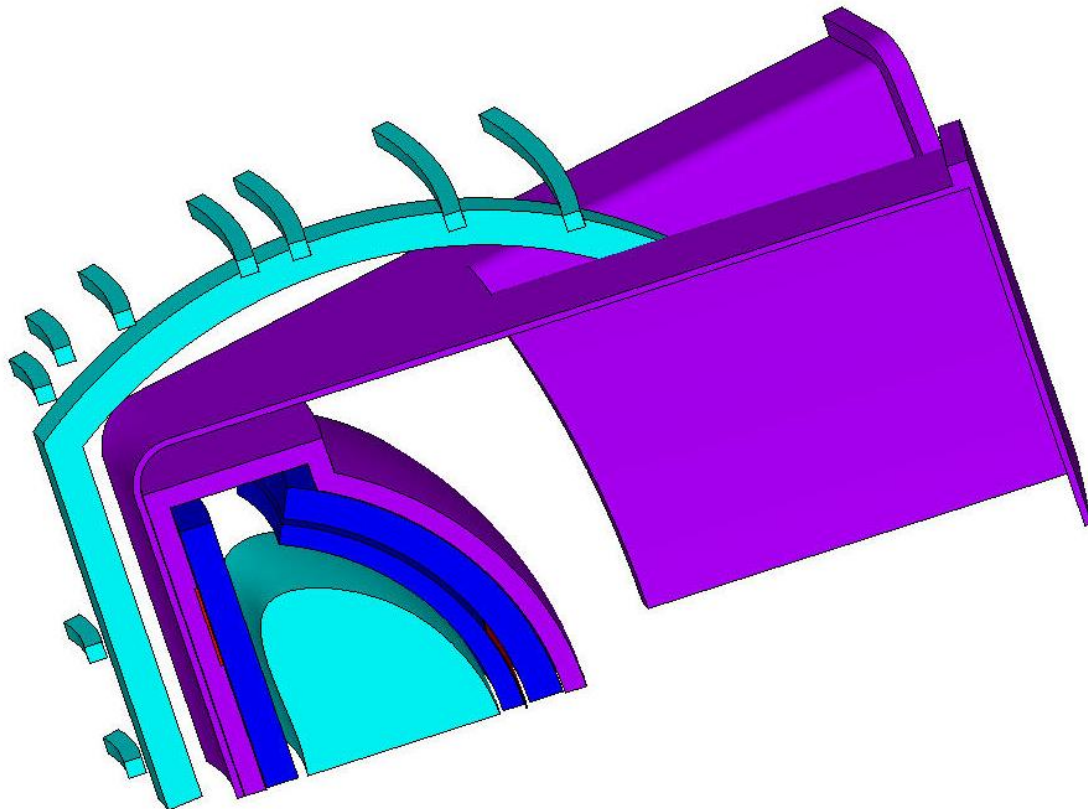


Transient Stresses at Midplane



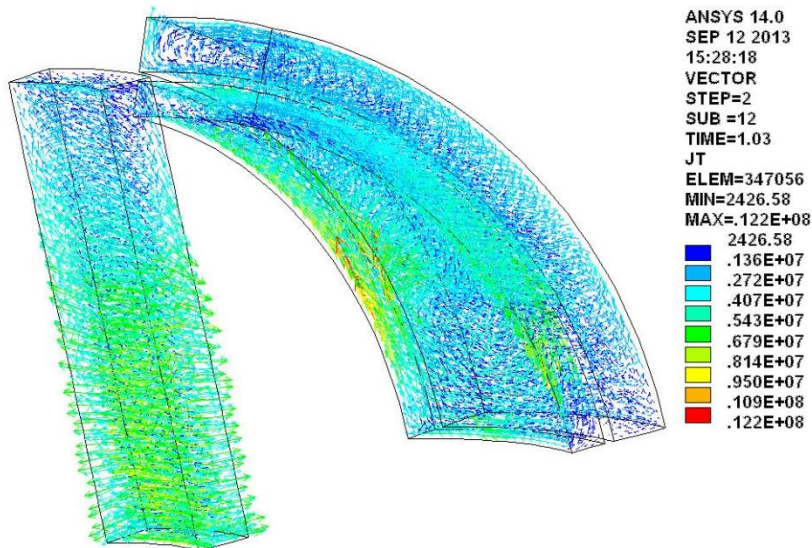
Approximation of Blanket Structure Added to Model

- Solid blocks of appropriate thickness used to investigate potential effects of blankets on VV currents and forces.
- Blanket modules are not electrically continuous.
- Initial models use effective electrical conductivity of steel for blankets.

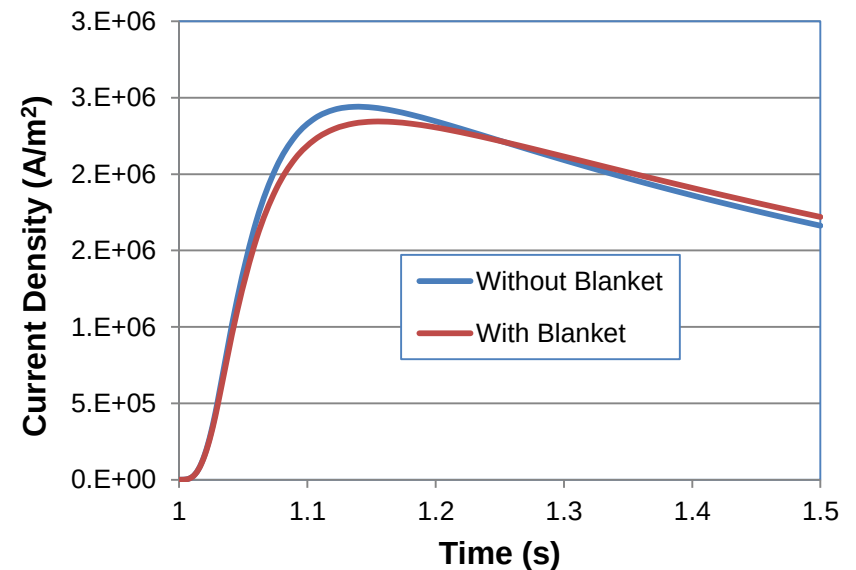


Vacuum Vessel Currents are not Greatly Affected by Blankets

Current Density in Blankets at End of Plasma Ramp down



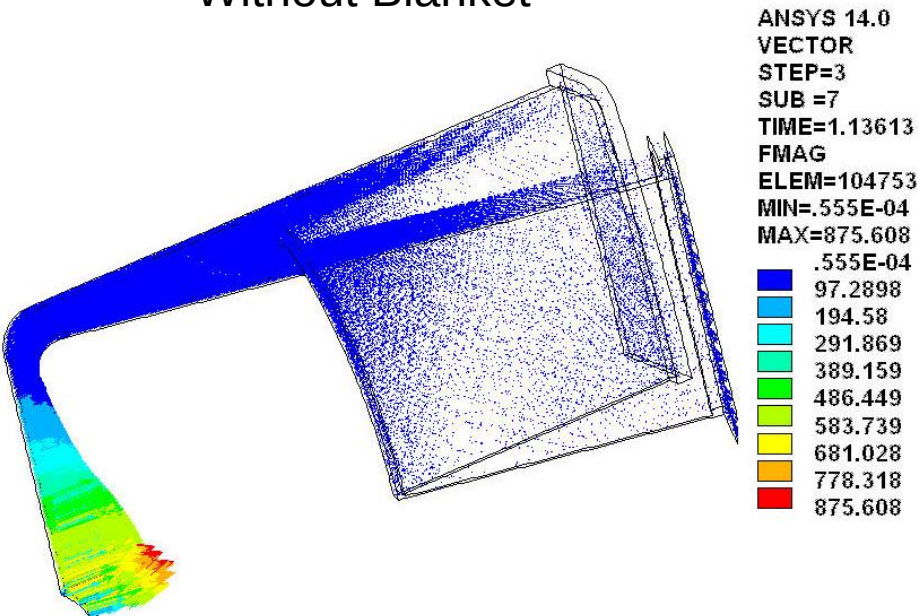
Current Density at VV Inboard Midplane With and Without Blanket



Vacuum Vessel Magnetic Forces are Only Slightly Reduced with Inclusion of Blanket

Magnetic Forces in VV 0.15 sec After Start of Ramp Down

Without Blanket



With Blanket

