



# Fracture of Divertor Structures

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ARIES Meeting

April 2011

# Outline

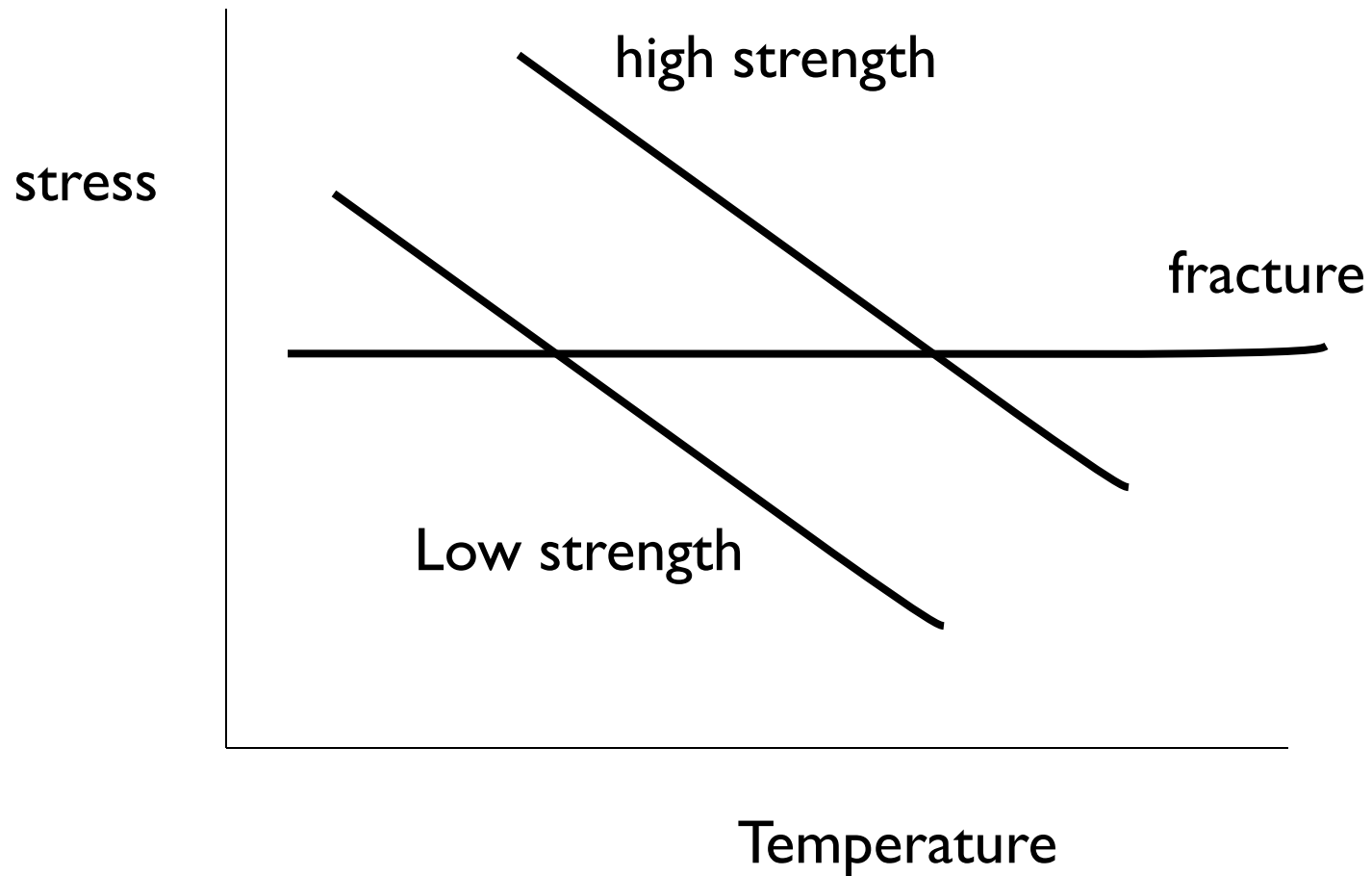
- Primer on Fracture Mechanics
- Preliminary Results for Divertor Structures
- Future Plans

# Design of Engineering Structures

- In early 20<sup>th</sup> century, design of metal structures was strictly stress based
- Onset of high performance ships (Liberty ships, WWII) changed things



# What happened?



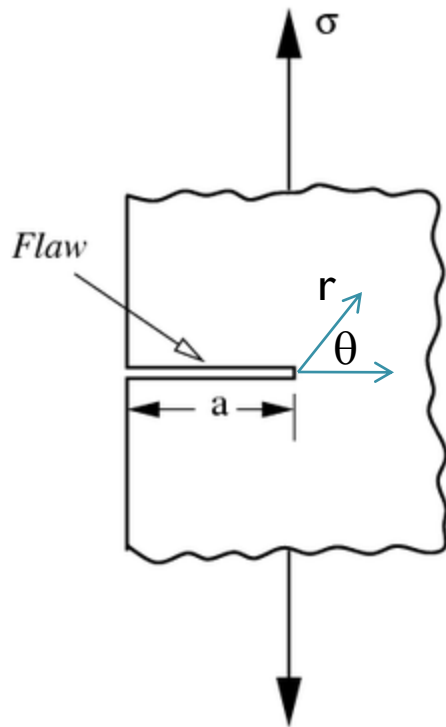
# Fracture Mechanics

- Size and Orientation of Cracks
- Stress Fields
- Material Properties

# Crack Tip Stress Fields (Elastic)

- Consider a sharp crack in an elastic material

$$\sigma_{ij} \approx \left( \frac{K}{\sqrt{2\pi r}} \right) f_{ij}(\theta)$$



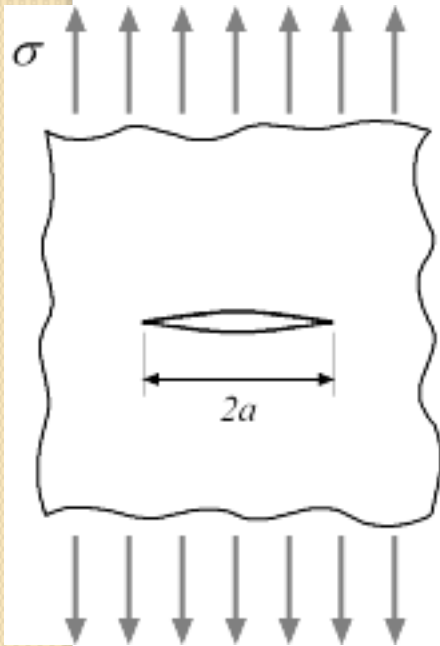
- $K$  is stress intensity factor
- Function of geometry and loading
- Fracture occurs when  $K$  reaches critical value ( $K_{IC}$  – fracture toughness)

# An Example

- Consider an infinite plate with a through crack

$$K_I = \sigma \sqrt{\pi a} = K_{IC}$$

$$\sigma_{allow} = \frac{K_{IC}}{\sqrt{\pi a}}$$



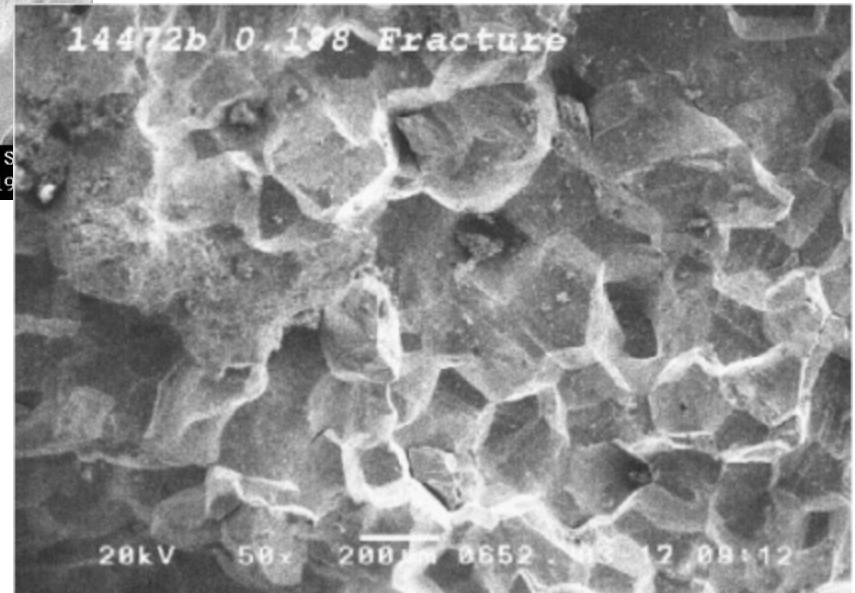
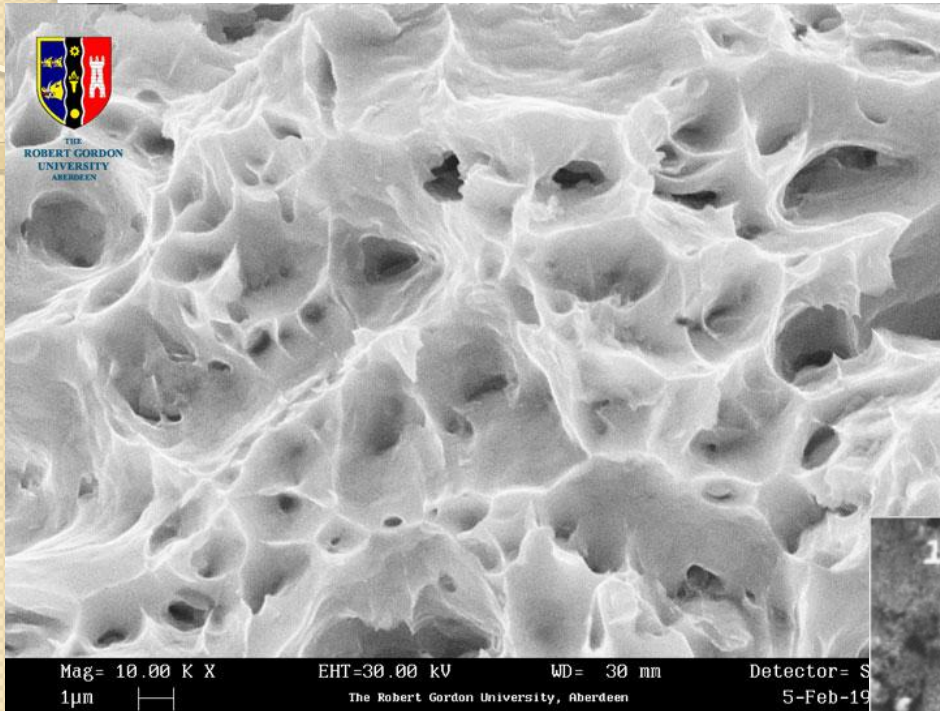
- Glass:  $K_{IC} = 1 \text{ MPa-m}^{0.5}$
- Al:  $K_{IC} = 20 \text{ MPa-m}^{0.5}$
- For  $a = 100$  microns, fracture stresses are 56 MPa for glass and 1,100 MPa for Al

# Fracture Toughness (room temp)

| Material                   | Toughness (MPa – m <sup>0.5</sup> ) |
|----------------------------|-------------------------------------|
| 7075 Aluminum              | 24                                  |
| 4340 Steel                 | 50                                  |
| Silicon Carbide            | 4                                   |
| Polystyrene                | 1                                   |
| Tungsten (polycrystalline) | 5                                   |
| Beryllium                  | 10                                  |

These values depend strongly on processing.

# Ductile vs. Brittle



# Temperature Dependence

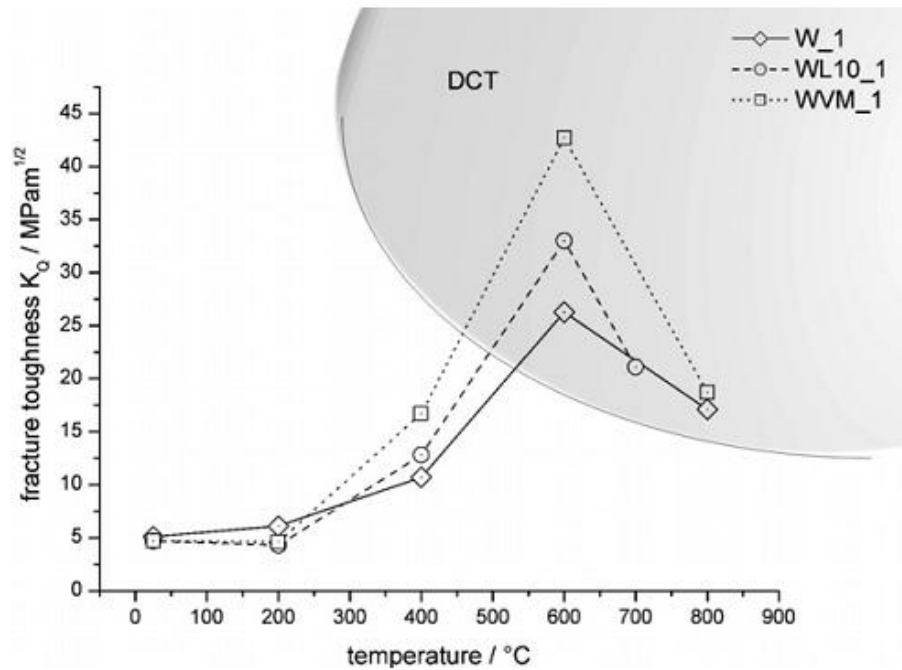


Fig. 1. Fracture toughness of tungsten alloys in the as sintered condition (DCT). The grey area marks the region where linear fracture mechanics is no longer valid.

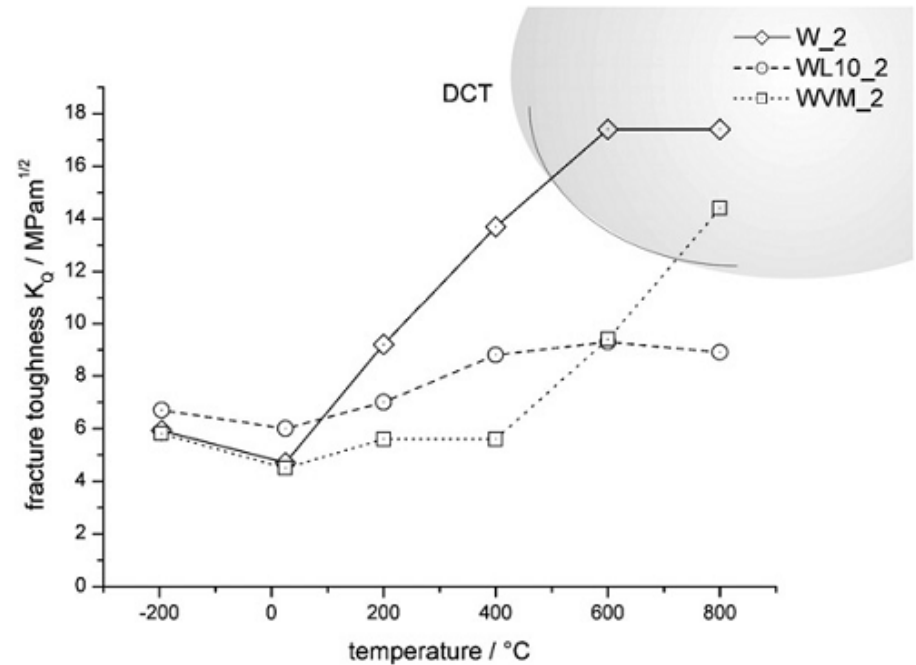
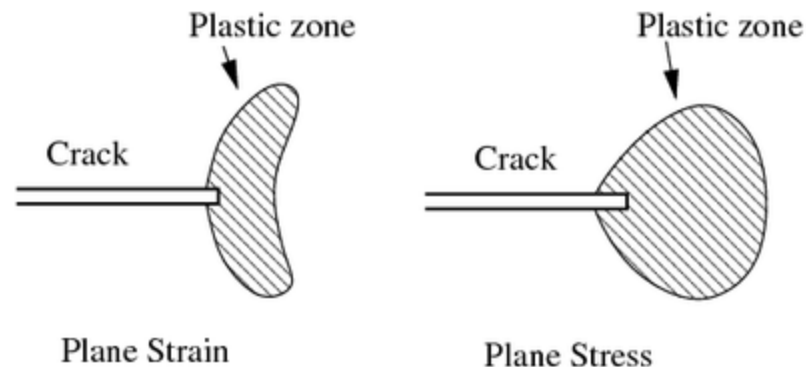


Fig. 2. Fracture toughness of tungsten alloys in the as-rolled condition (60% reduction, DCT). The grey area marks the region where linear fracture mechanics is no longer valid.

# Stress Fields in Ductile Materials

- Ductile materials will develop plastic deformation at crack tips
- This toughens material and resists catastrophic crack growth
- Previous analysis is not valid
- Analysis uses integral around crack tip, rather than stress intensity factor

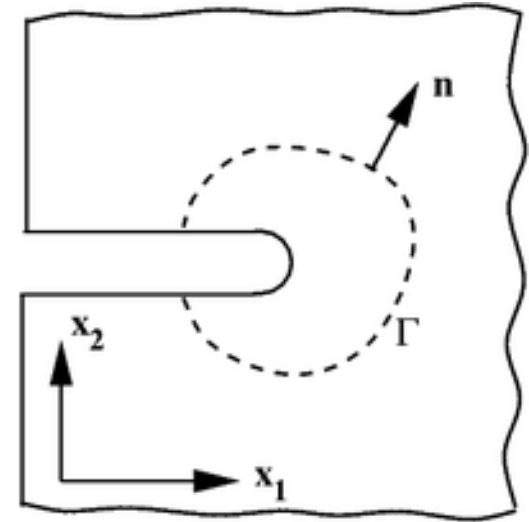


# Failure Criterion for Ductile Materials

- Base failure prediction on work required to create fresh fracture surface
- Write as line integral

$$J_I = \int_{\Gamma} \left( W dx_2 - t \cdot \frac{\partial u}{\partial x_1} ds \right)$$

$$J_{IC} = K_{IC}^2 \left( \frac{1 - \nu^2}{3E} \right)$$



W=strain energy density

T=tractions

U=displacement

# Irradiated Materials

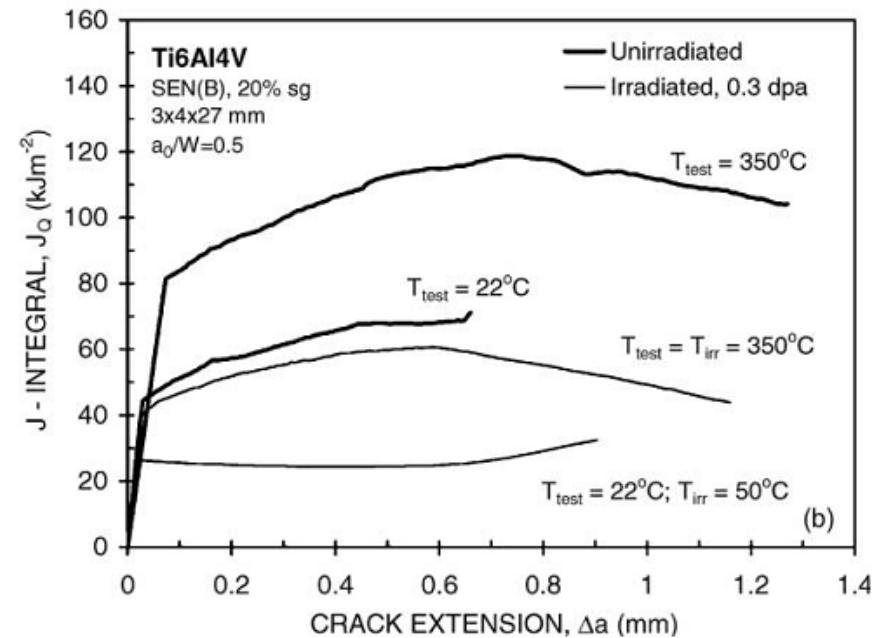
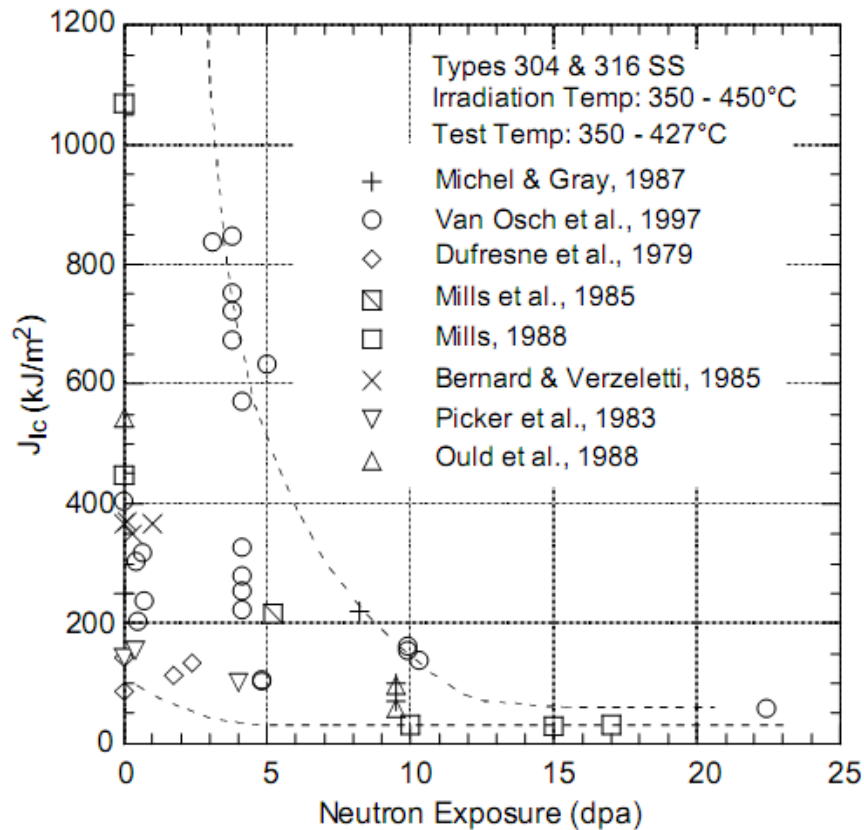
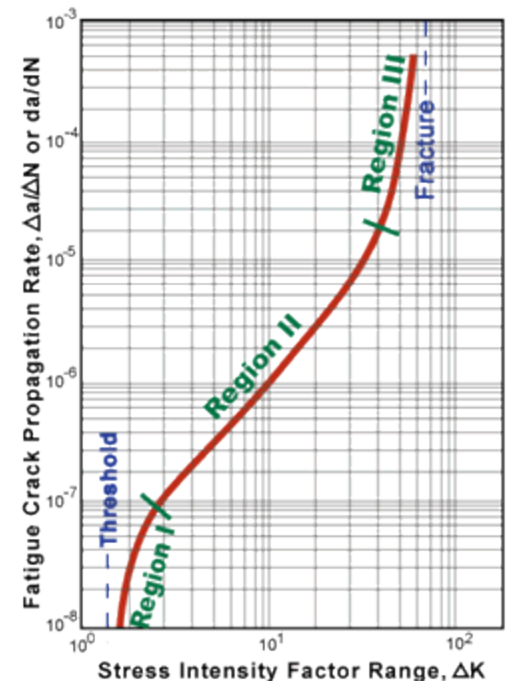
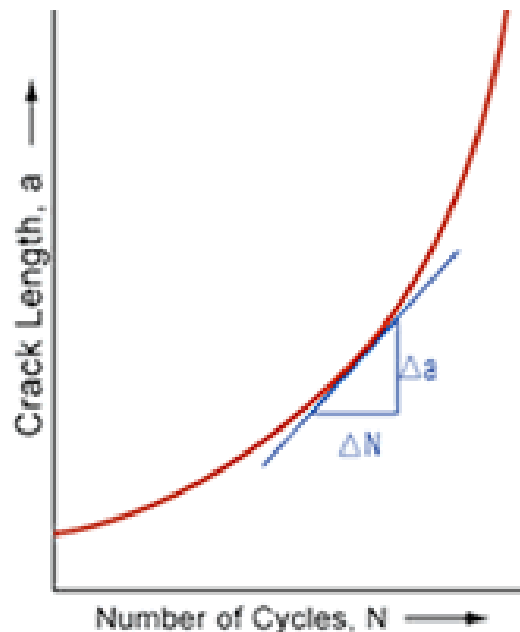


Fig. 3. Fracture resistance curves of (a) Ti5Al2.5Sn ( $\alpha$ ) alloy and (b) Ti6Al4V ( $\alpha + \beta$ ) alloy at different test temperatures in unirradiated and neutron irradiated (0.3 dpa) conditions.

# Fatigue Crack Growth

- Previous analyses refer to catastrophic, unstable crack growth
- Repeated application of loads can lead to incremental crack growth



# Characterizing Cracks

- Key Question: What is initial crack size?
- We need non-destructive examination (NDE)
- Options:
  - Dye penetrant
  - Ultrasound
  - X-rays
  - Eddy currents
  - Thermography
  - Etc.
- Costs and capabilities vary

# ITER Structural Design Criteria

- Primary Loads

$$K_I < 0.33K_C$$

- Primary + Secondary Loads

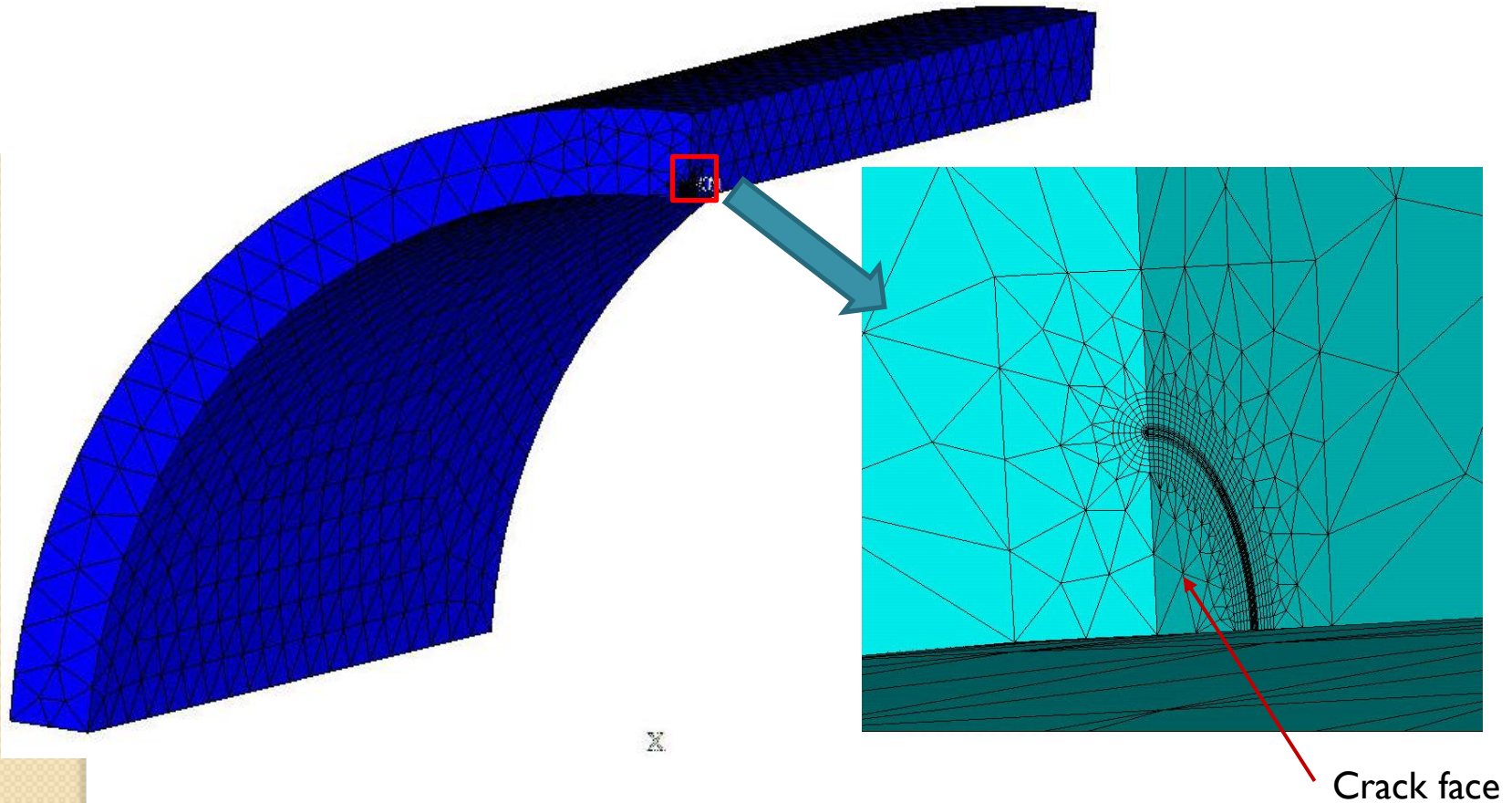
$$K_I < 0.67K_C$$

- Elasto-Plastic Analysis

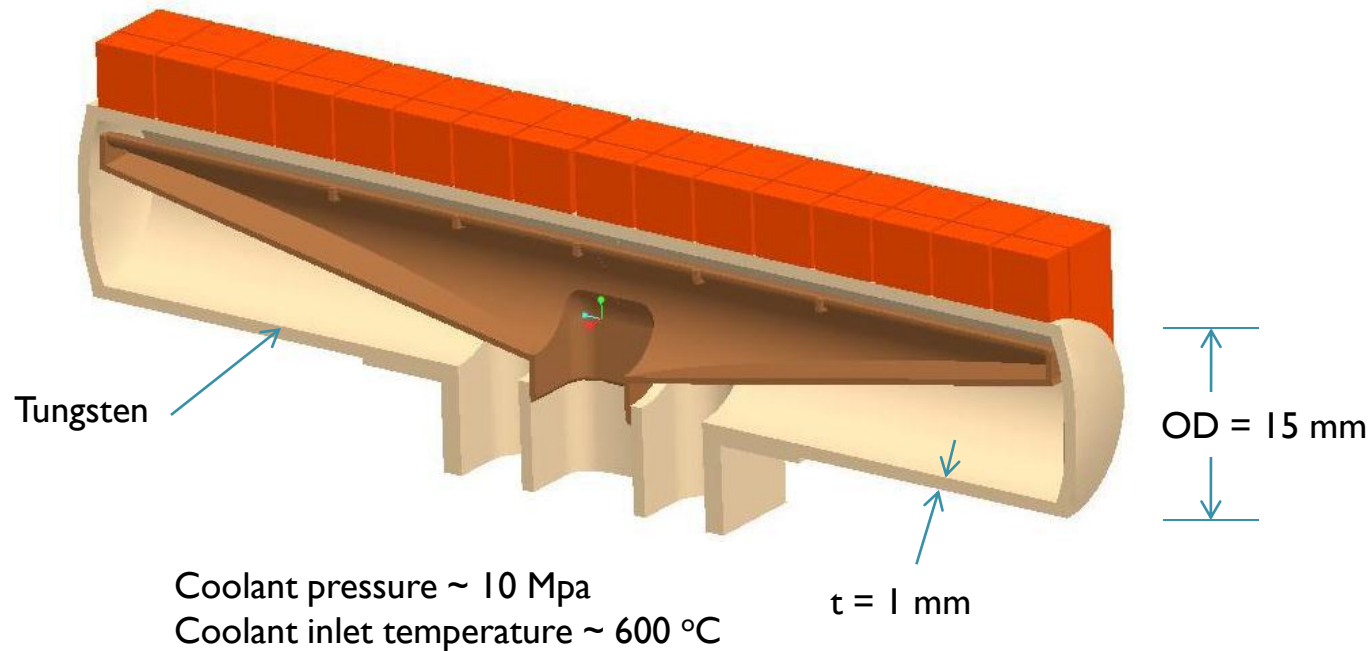
$$J_I < 0.67J_C$$

# ANSYS Finite Element Model of Circumferential Crack

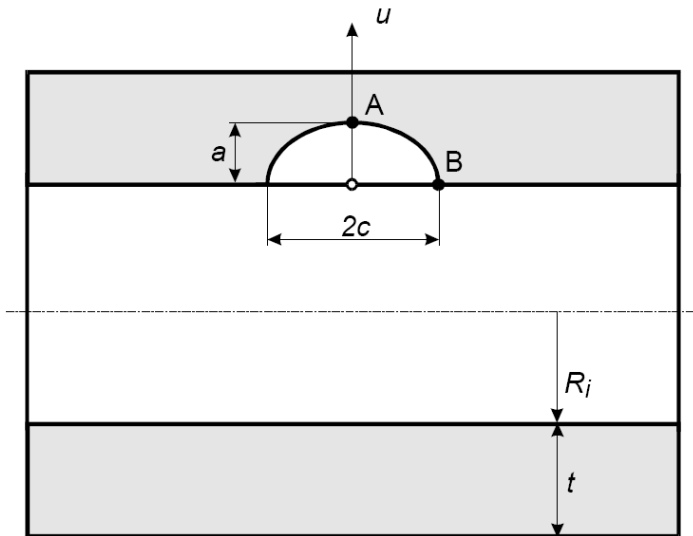
- Stress intensities along crack face using the ANSYS CINT command
- Elastic-Plastic material properties for Tungsten used
- Currently only pressure loads are considered, but thermal stresses to be included



# Initial Fracture Studies Based on T-Tube Geometry and Pressure Loads



# Initial Studies Compute Stress Intensities for Axial Cracks in Pressurized Cylinder



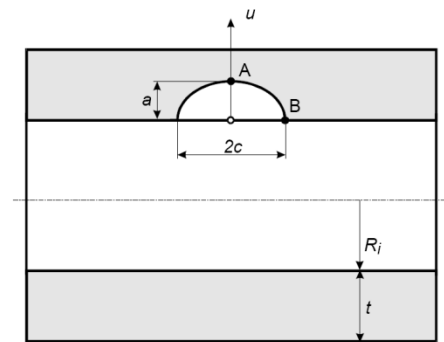
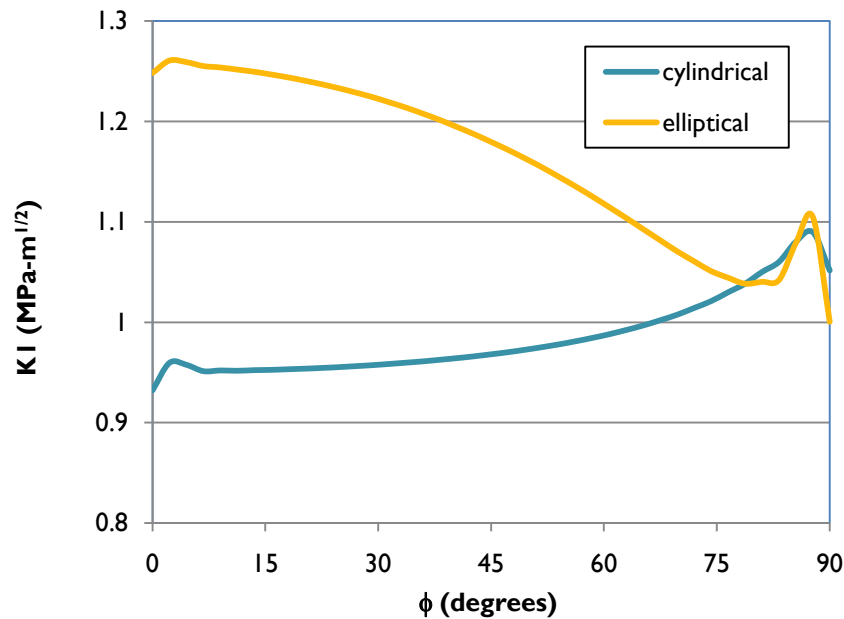
Case 1: Circular crack;  $c/a=1$

Case 2: Elliptical crack;  $c/a=2$

Use elastic-plastic properties for tungsten.

Calculate  $J_I$  and then report equivalent  $K_I$ .

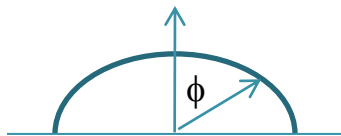
# Variation of Stress Intensity with Location along Crack Tip ( $a = 0.1$ mm)



Case 1: Circular crack;  $c/a=1$

Case 2: Elliptical crack;  $c/a=2$

$a = 0.1$  mm



# Maximum Stress Intensity as a Function of Crack Depth

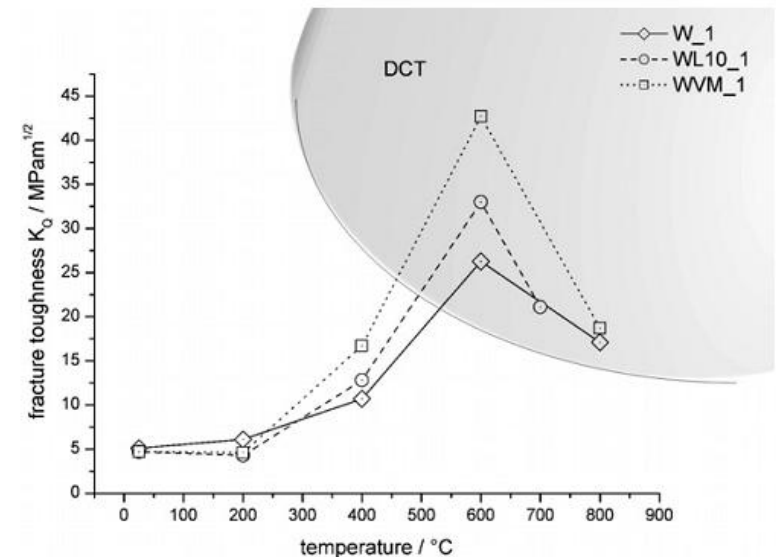
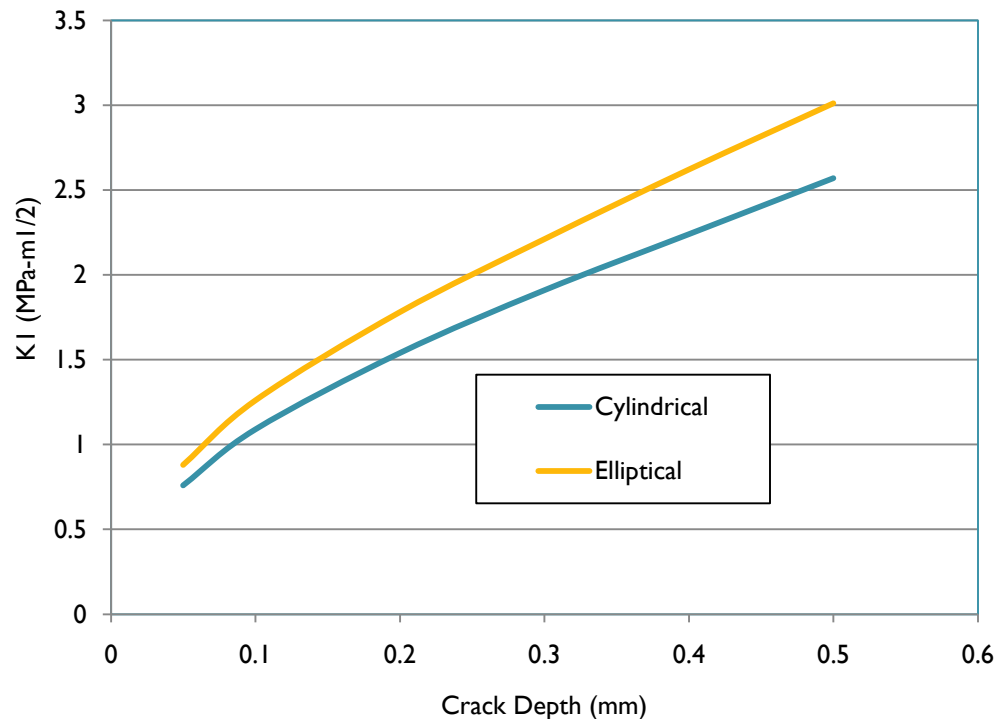


Fig. 1. Fracture toughness of tungsten alloys in the as sintered condition (DCT). The grey area marks the region where linear fracture mechanics is no longer valid.

# Conclusions

- We've got to include fracture in our design analysis, particularly when using materials with limited ductility
- So far, there are no major red flags
- We will include thermal stresses in the future