

Power Core Engineering: Design Updates and Trade-Off Studies

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Engineering and Trade-Off Studies

- **Power cycle choice: Rankine vs Brayton (done, UCSD)**
- **Impact of tritium breeding requirement on fuel management and control (done, UW/UCSD)**
- **Evaluation of different He-cooled divertor concepts based on thermo-mechanical performance and initial reliability assessment (in progress, UCSD/INL/Georgia Tech.)**
- **Assessment of off-normal conditions for a power plant**
 - **how to avoid disruptions and other off-normal events (in progress, GA)**
 - **impact of off-normal events on power plant (thermal impact presented here, UCSD)**
- **Impact of design choice on reliability, availability and maintenance (L. Waganer)**
- **Lead lithium based blanket as example development pathway (DCLL design updates and discussion at this meeting)**



Vapor Pressure and Heat of Dissociation of SiC

Heat of sublimation of Si = 454 kJ/mol (108.4 kcal-mol⁻¹)

(from S. G. Davis, et al., Journal of Chemical Physics, Vol. 34, No. 2, p659-663, Feb 1961)

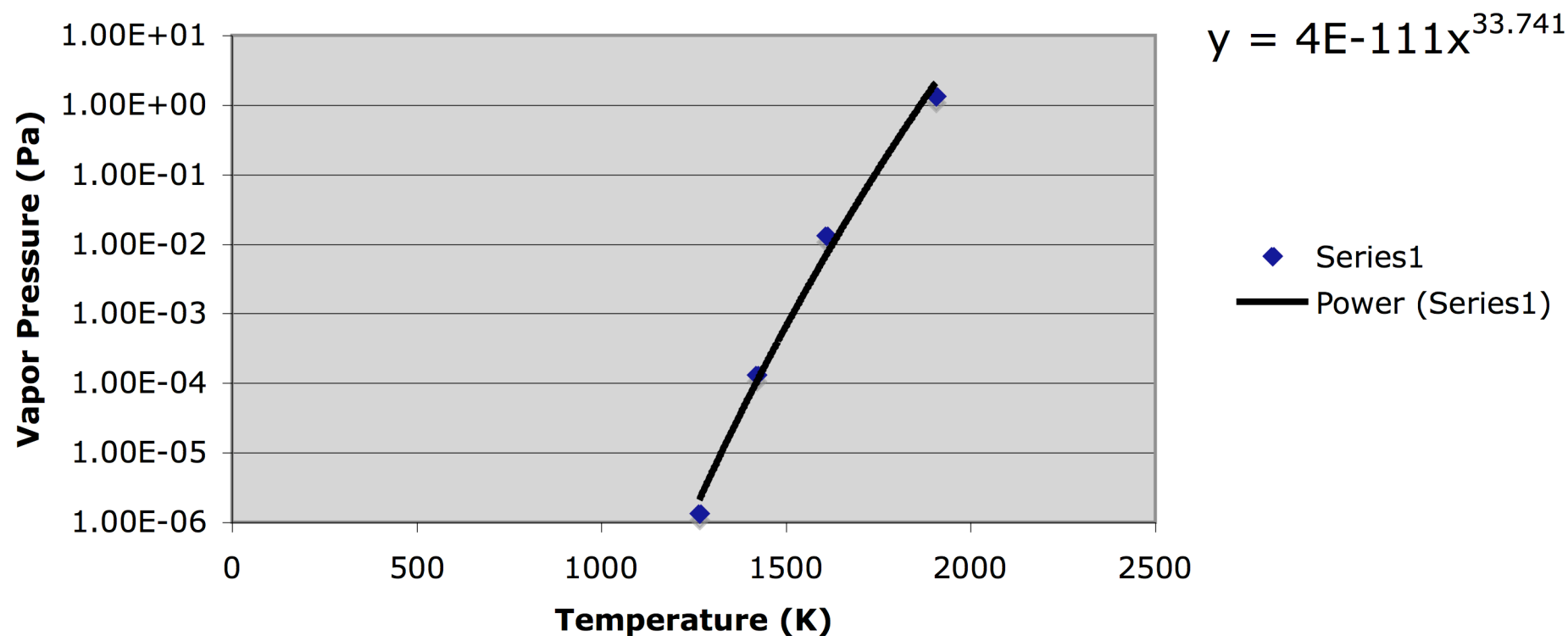
Heat of formation of SiC = 62.85 kJ/mol (15 kcal-mol⁻¹)

Heat of dissociation of SiC = 516.9 kJ/mol

Si melting point/boiling point= 1412°C/2355°C

C sublimation point >3500°C

Si Vapor Pressure as a function of Temperature

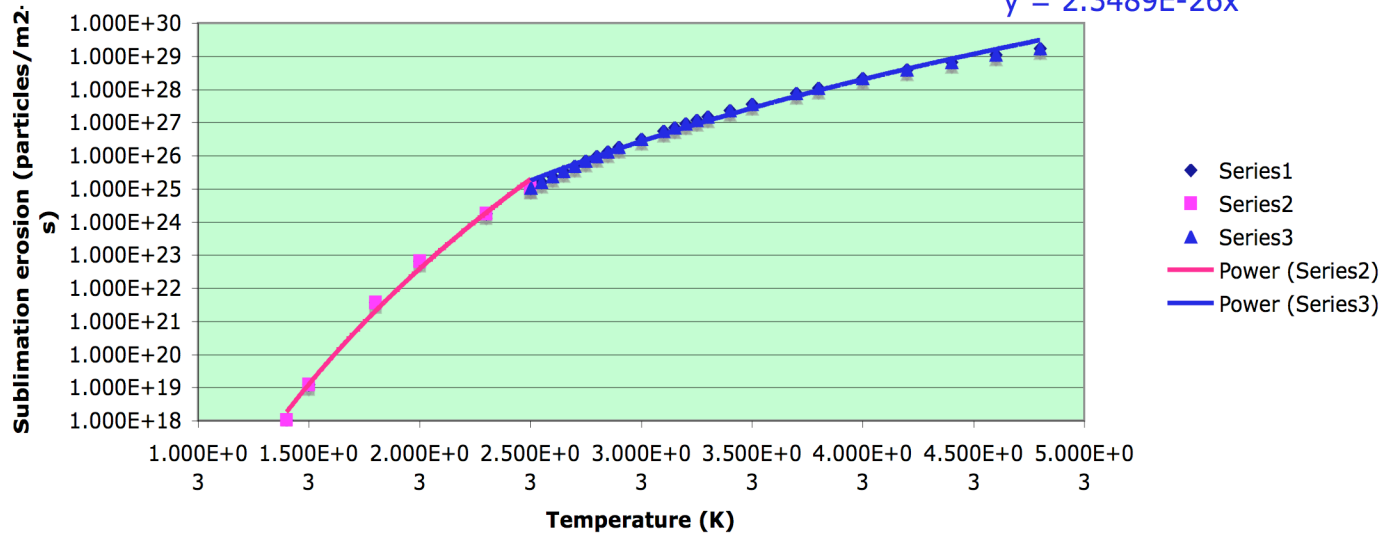


SiC Dissociation

SiC Dissociation erosion as a function of temperature

$$y = 3.0675E-70x^{2.7897E+01}$$

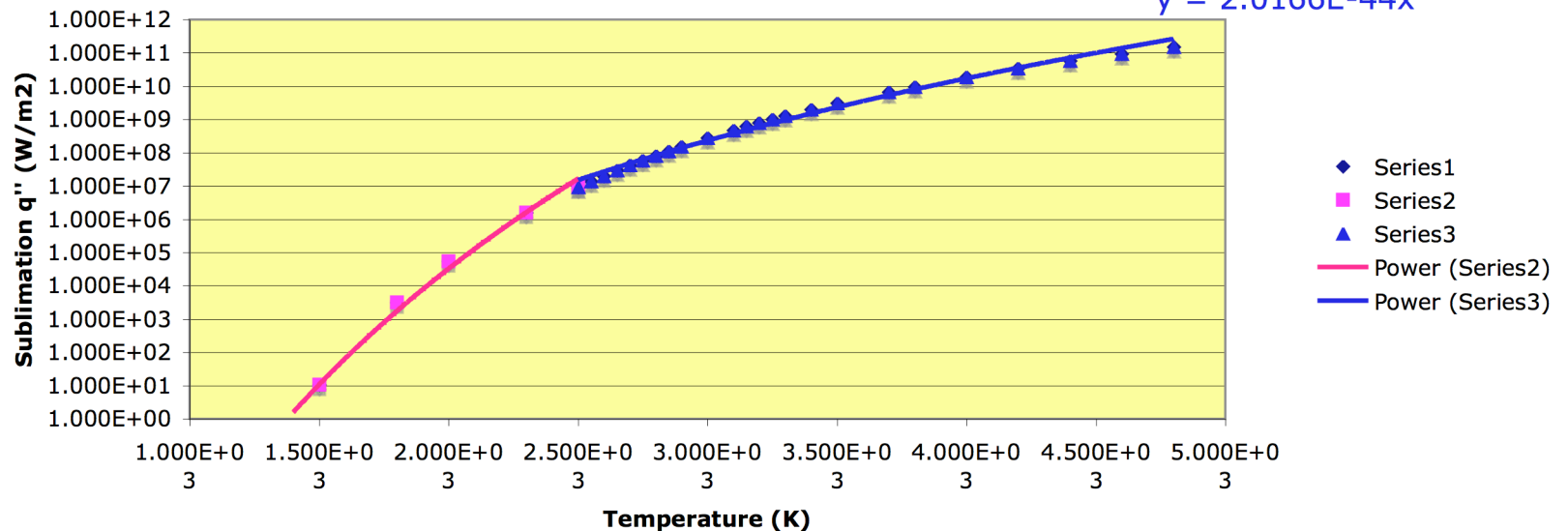
$$y = 2.3489E-26x^{1.4971E+01}$$



SiC Dissociation q'' as a function of temperature

$$y = 2.6337E-88x^{2.7897E+01}$$

$$y = 2.0166E-44x^{1.4971E+01}$$



Off-Normal Thermal Loads for Analysis with RACLETTE Code

From ITER

(from PID and C. Lowry's presentation at last ITER WG8 Design review Meeting)

- **Disruptions:**

- Parallel energy density for thermal quench = 28-45 MJ/m² near X-point
- Deposition time ~ 1-3 ms
- Perpendicular energy deposition will be lower, depending on incidence angle (at least 1 order of magnitude lower)
- Parallel energy deposition for current quench = 2.5 MJ/m²
- For power plant, fusion energy is ~ 4x higher than ITER and the energy deposition will also be higher
- Parametric analysis over 1-10 MJ/m² and 1-3 ms

- **VDE's:**

- Energy deposition = 60 MJ/m²
- Deposition time ~ 0.2 s

- **ELMS:**

- Parallel energy density for thermal quench (controlled/uncontrolled) ~ 0.77/3.8 MJ/m²
- Deposition time ~ 0.4 ms

Frequency (controlled/uncontrolled) = 4/1 Hz

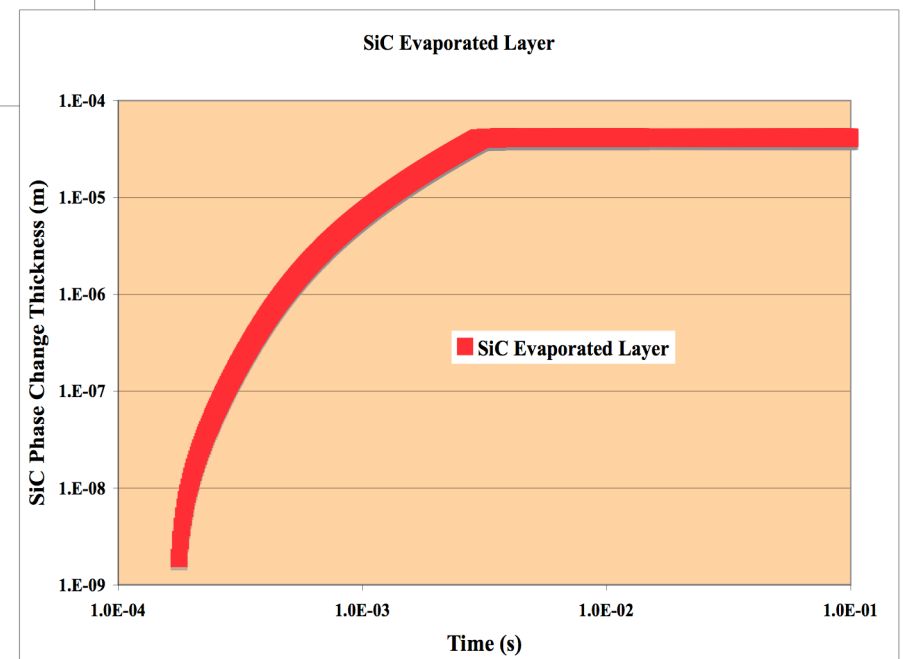
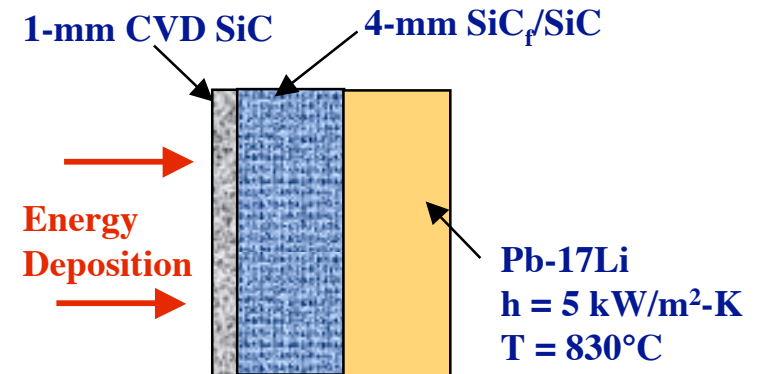
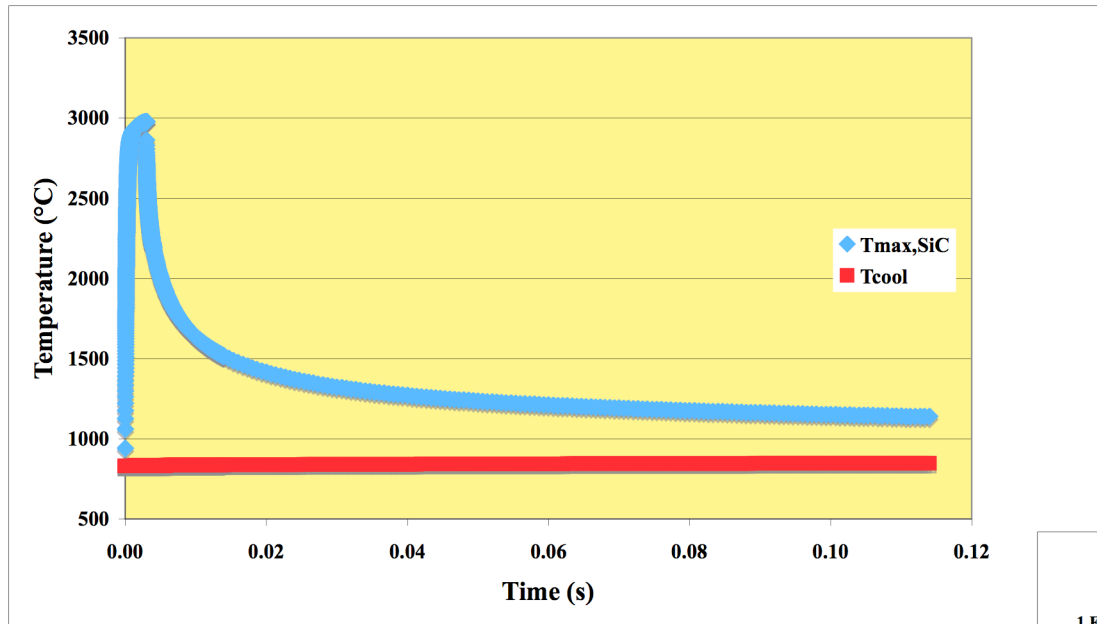
Assumed power plant case ~0.3/1.5 MJ/m² incident energy deposition over 0.4 ms



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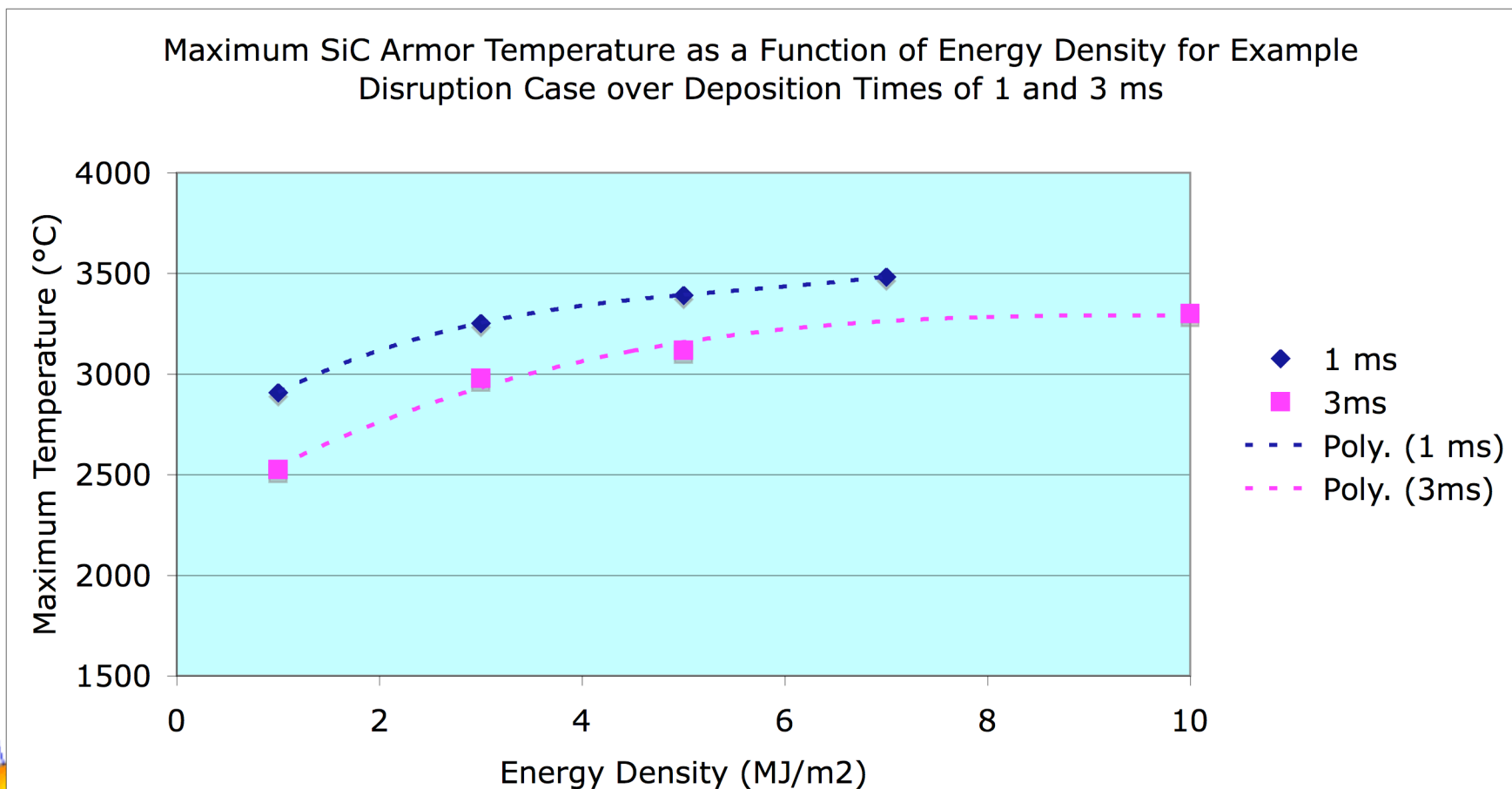
Example Disruption Case for Power Plant with SiC FW

- Disruption simulation: $q''=10^9$ W/m² over 3 ms (~3 MJ/m²)
- 1 mm CVD SiC armor on 4-mm SiC_f/SiC FW by Pb-17Li at 830°C with $h=5$ kW/m²-K



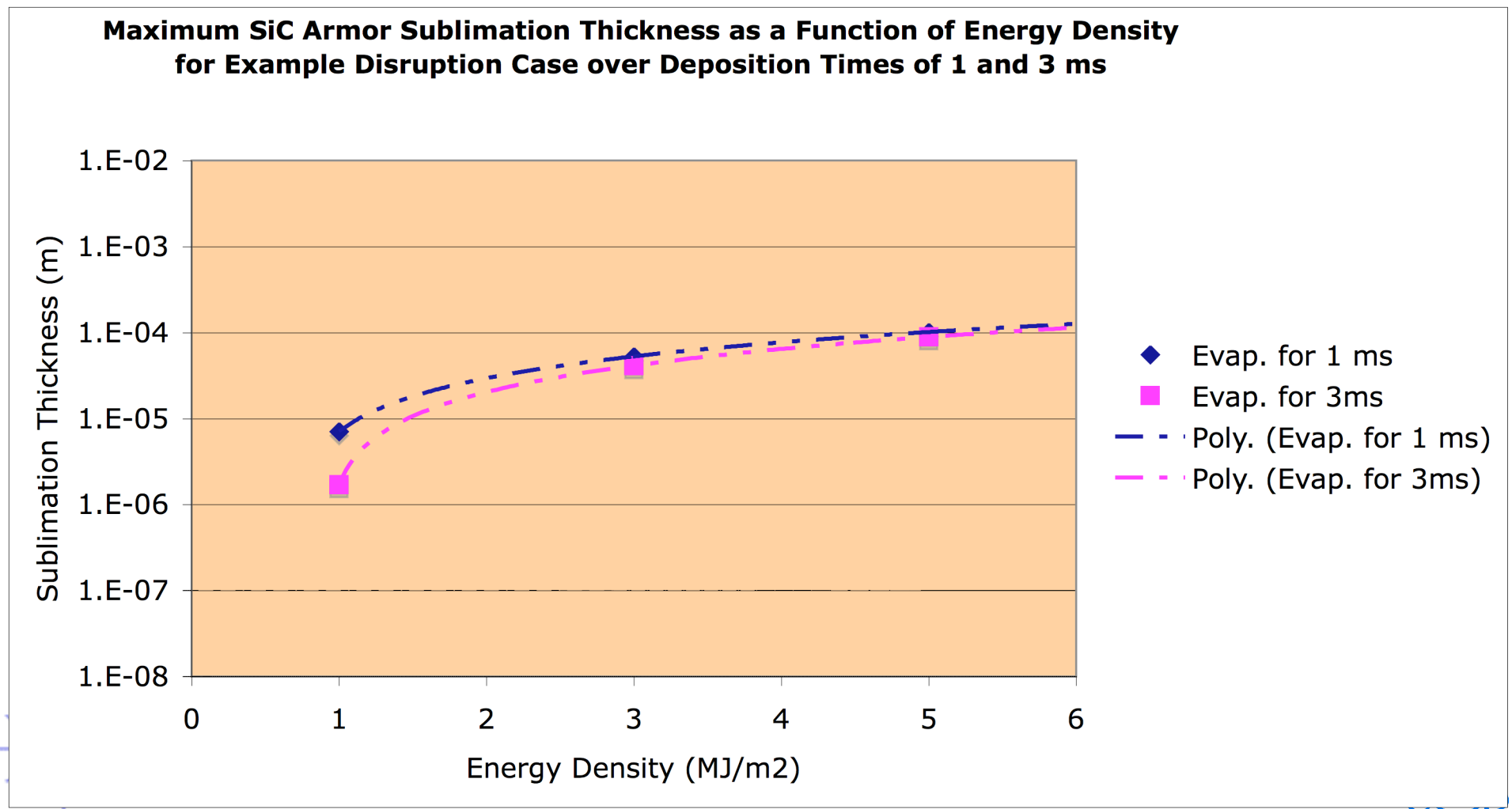
Parametric Study of Maximum SiC FW Temperature for Different Disruption Scenarios

- 1 mm armor (CVD SiC) on 4-mm SiC_f/SiC FW by Pb-17Li at 830°C with $h=5 \text{ kW/m}^2\text{-K}$



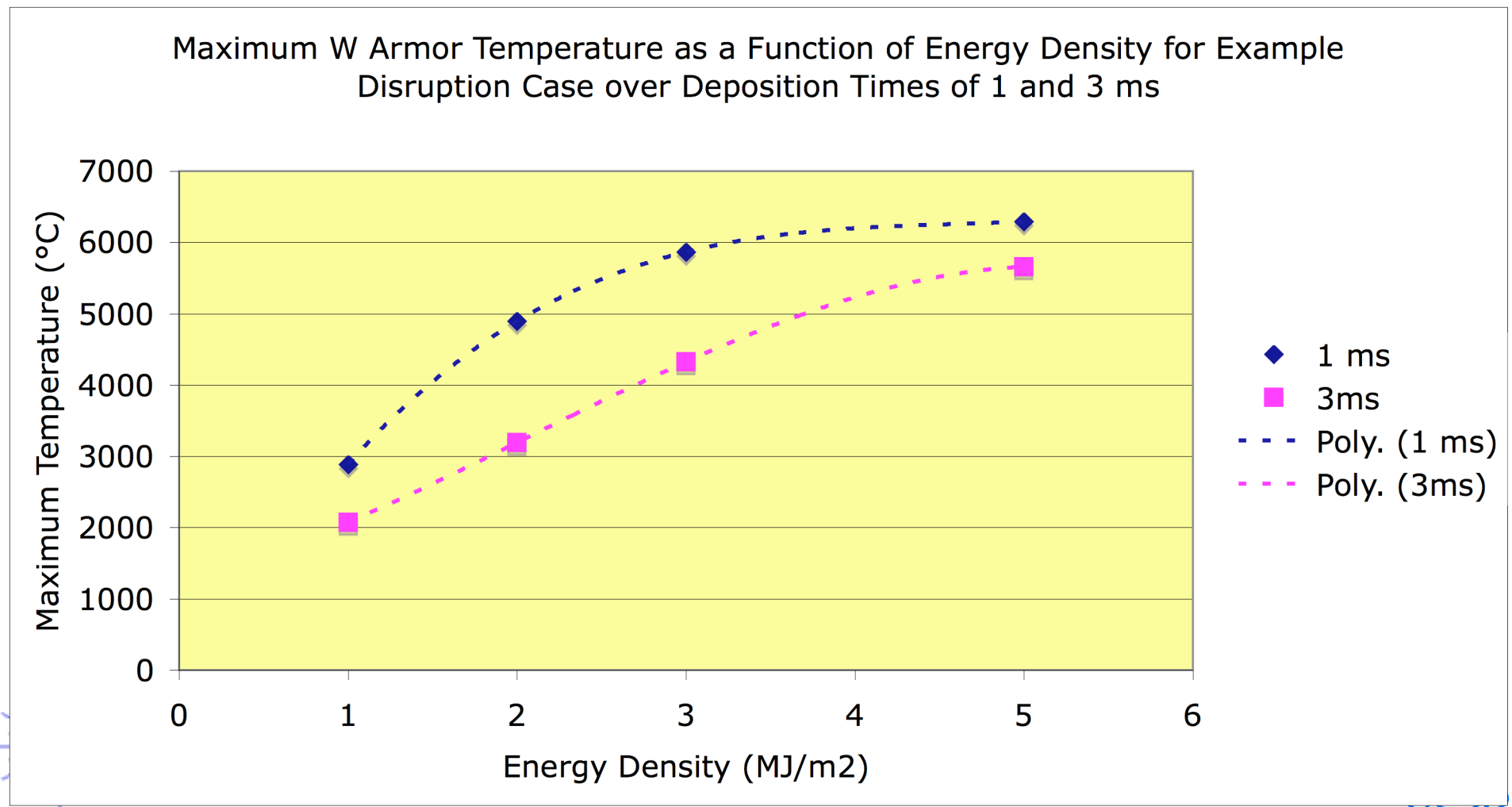
Parametric Study of Maximum Sublimation Thickness of a SiC FW Temperature for Different Disruption Scenarios

- 1 mm armor (CVD SiC) on 4-mm SiC_p/SiC FW by Pb-17Li at 830°C with $h=5 \text{ kW/m}^2\text{-K}$
- Up to $\sim 0.1 \text{ mm}$ lost per event
- Only a few events allowable based on erosion lifetime



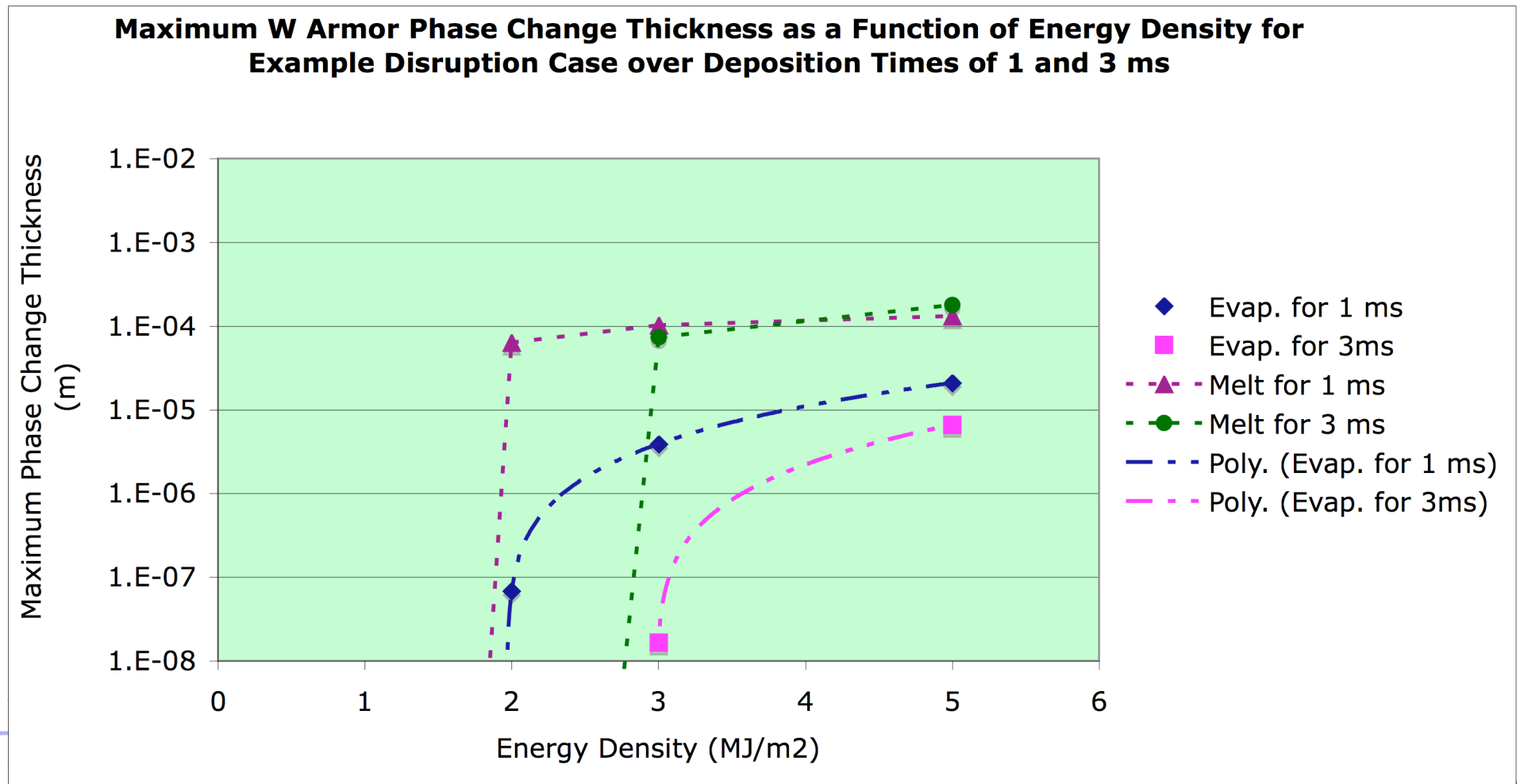
Parametric Study of Maximum W FW Temperature for Different Disruption Scenarios

- 1 mm armor (W) on 4-mm SiC_f/SiC FW by Pb-17Li at 830°C with $h=5$ kW/m²-K
- W MP = 3422°C; BP = 5555°C



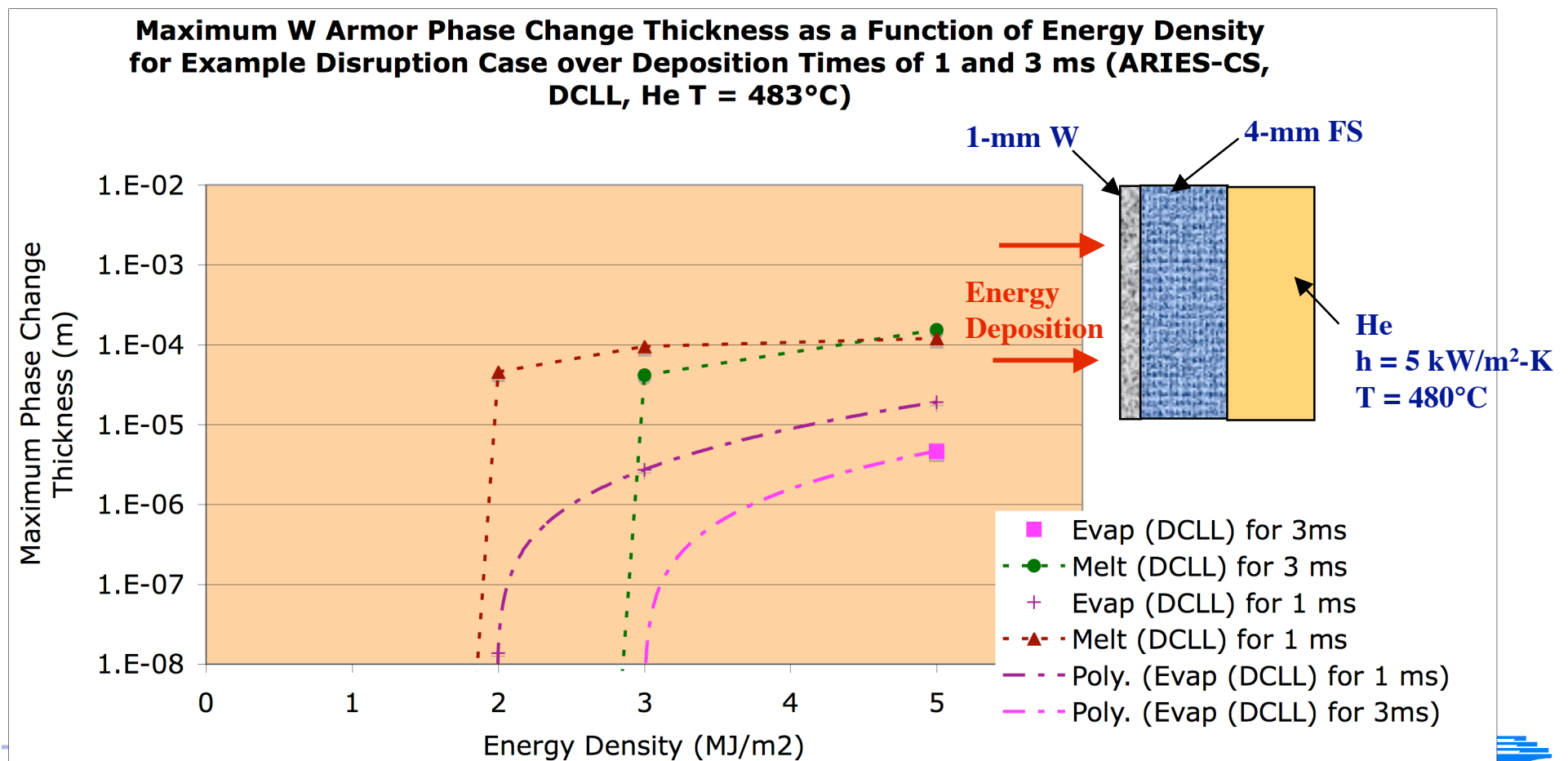
Parametric Study of Maximum Phase Change Thickness of a W FW Temperature for Different Disruption Scenarios

- 1 mm armor (W) on 4-mm SiC_f/SiC FW cooled by Pb-17Li at 830°C with $h=5 \text{ kW/m}^2\text{-K}$
- Up to $\sim 0.1 \text{ mm}$ melt layer and $\sim 0.01 \text{ mm}$ evaporation loss per event
- Again, only a few events allowable based on erosion lifetime



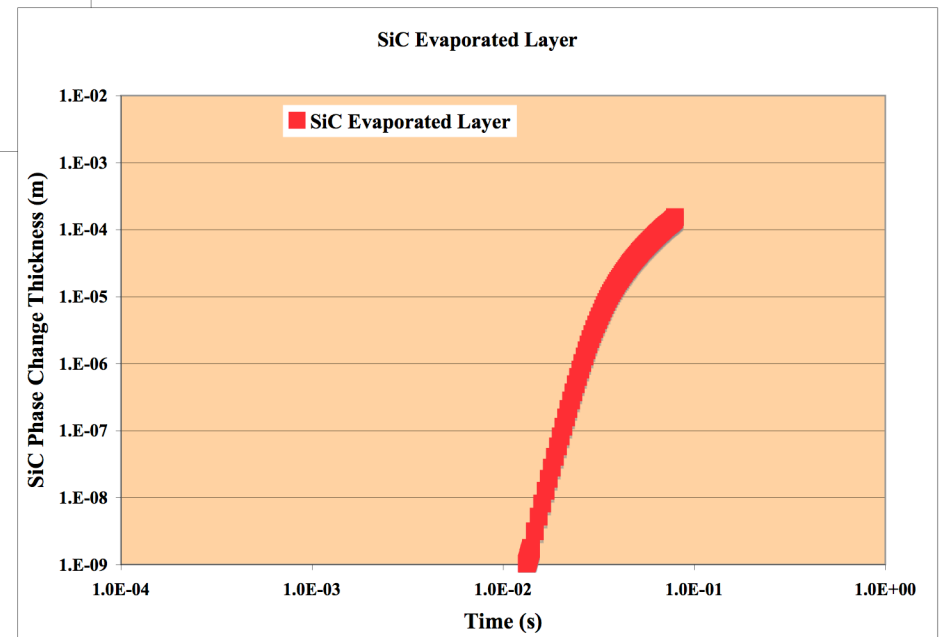
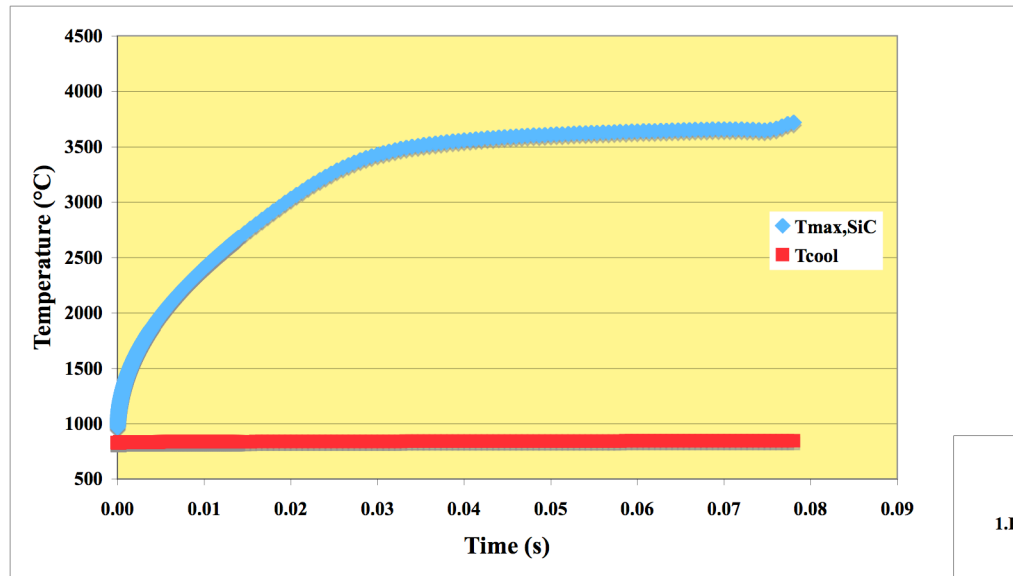
Parametric Study of Maximum Phase Change Thickness of a W FW Temperature for Different Disruption Scenarios (DCLL Case)

- 1 mm armor (W) on 4-mm FS FW cooled by He at 483°C with $h=5.2 \text{ kW/m}^2\text{-K}$
- Up to $\sim 0.1 \text{ mm}$ melt layer and $\sim 0.01 \text{ mm}$ evaporation loss per event
- Again, only a few events allowable based on erosion lifetime depending on energy density



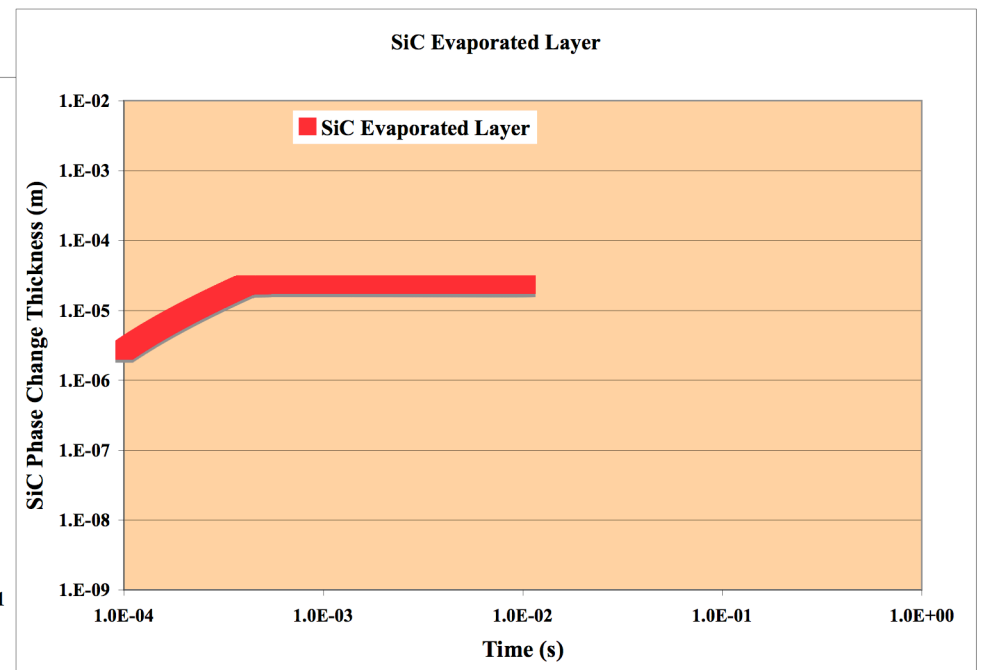
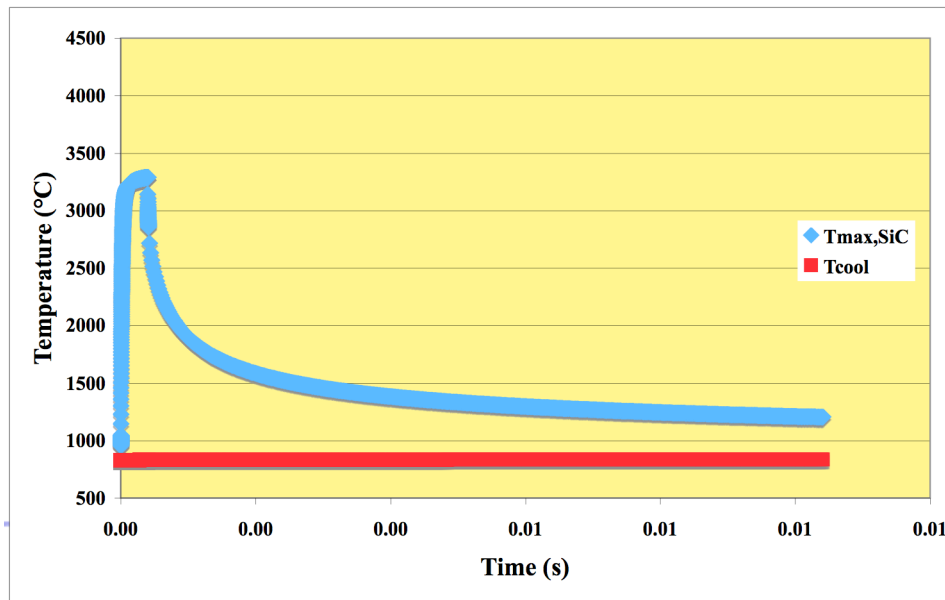
Example VDE Case for Power Plant with SiC FW

- VDE simulation: $q'' = 3 \times 10^8 \text{ W/m}^2$ over 0.2 s (60 MJ/m²)
- 1 mm CVD SiC armor on 4-mm SiC_f/SiC FW by Pb-17Li at 830°C with $h = 5 \text{ kW/m}^2\text{-K}$
- Even 1 event is not acceptable (complete loss of armor)
- Same conclusion for W armor



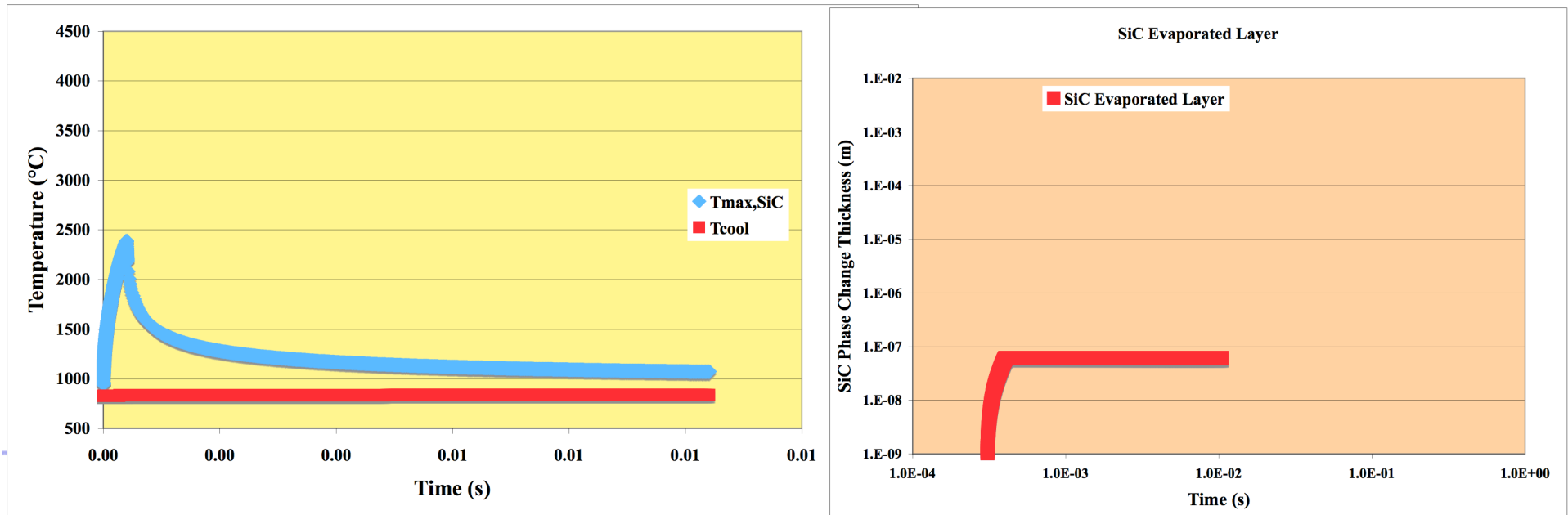
Example Uncontrolled ELM Case for Power Plant with SiC FW

- ELM simulation: $q'' = 3.75 \times 10^9 \text{ W/m}^2$ over 0.4 ms (1.5 MJ/m²)
- 1 mm CVD SiC armor on 4-mm SiC_f/SiC FW by Pb-17Li at 830°C with $h = 5 \text{ kW/m}^2\text{-K}$
- ~0.02 mm of armor loss per event (1 Hz frequency)
- Not acceptable (complete loss of armor after 50 such events)
- Similar conclusion for W armor
 - $T_{\text{max}} = 5512^\circ\text{C}$; $5 \times 10^{-5} \text{ m}$ melt; $3 \times 10^{-7} \text{ m}$ evaporation loss per event
 - Complete loss of armor after 3333 such events even without melt loss



Example Controlled ELM Case for Power Plant with SiC FW

- ELM simulation: $q'' = 7.5 \times 10^8 \text{ W/m}^2$ over 0.4 ms (0.3 MJ/m²)
- 1 mm CVD SiC armor on 4-mm SiC_f/SiC FW by Pb-17Li at 830°C with $h = 5 \text{ kW/m}^2\text{-K}$
- $\sim 0.08 \text{ }\mu\text{m}$ of armor loss per event (5 Hz frequency)
- Complete loss of SiC armor after 1.25×10^7 such events (~ 1 month if occurring at same location) - Not acceptable
- OK for W armor ($T_{\text{max}} = 1872^\circ\text{C}$; no melt; 10^{-20} m evaporation loss per event)



Summary of Assessment of Off-Normal Energy Deposition on FW (based on assumed scenarios)

- Focus on thermal effects
- EM effects will be important for DCLL but not as much for ARIES-AT with resistive FW (SiC_f/SiC)
- Only a few disruptions can be accommodated (depending on the energy density)
- DCLL slightly better than ARIES-AT (because of lower base temperature of FW)
- VDE cannot be accommodated
- Only limited number of uncontrolled ELM cases can be accommodated
- Controlled ELM's would limit the lifetime of SiC armor but might be acceptable for W armor

