



Assessment of Power Core Parameters and Related Costs (Part-III)

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ARIES-CS Project Meeting

April 27 - 28, 2006

UW

Contents

- **Revised costing accounts (in 2004\$):**
 - # 21: Structures & Site Facilities**
 - # 21.2: Reactor Building
 - # 22: Reactor Plant Equipment**
 - # 22.1.5 Primary Structure
 - # 22.1.6: Vacuum System
- Shield vs NWL scaling law.
- Cryogenic heat load to magnet.
- Sensitivity of COE to availability and LSA.
- Radwaste volume comparison
- Future plan.

Account # 21.2 (Reactor Building)

ARIES-CS building volume V_{RB} (in m^3) = $1.3 \times 10^5 \times 1.3^\#$, per Les and Xueren

Old costing algorithm (R. Miller):

$$\text{Cost (2004 M\$)} = [77.1 (V_{RB}^\# / 80,000)^{0.62}] \times \text{LSA Factor} \times 1.256^*$$

New costing algorithm (L. Waganer):

$$\text{Cost (2004 M\$)} = [33 + 0.00025 \times V_{RB}] \times \text{LSA Factor}$$

ARIES-	RS	AT	CS	
LSA	2	1	2	
21.2 Reactor Bldg (M\$ - 2004\$)	~ 160 old	~ 100 old	~ 140 old	~ 68 new

New costing algorithm results in factor of 2 lower building cost

Correction factor to account for unaccounted buildings.

* 2004\$ = 1992\$ x 1.256, per Les.

Account # 22.1.5 (Primary Structure)

$$\text{Cost (2004 M\$)} = [\text{volume} \times \text{steel density (7.8 gm/cm}^3\text{)} \times \text{vol. fract. (0.95)} \\ \times \text{unit cost (~25 \$/kg)}] \times \text{LSA Factor} \times 1.256$$

$$\text{Volume} = 18.4\% \text{ FPC volume}$$

$$\text{FPC volume}^* = \text{actual volume of FW + blanket + divertor + shield + VV} \\ + \text{winding pack + coil structure (including bucking structure)} \\ \approx 400 \text{ m}^3$$

ARIES-	RS	AT	CS	
			1/06	3/06
LSA	2	1	2	
21.1.5 Primary Str. (M\$- 2004\$)	67	34	46	~ 90

* Should not include primary structure, cryostat, bioshield, nor buildings.

Account # 22.1.6 (Vacuum System)

Includes cost of VV, cryostat, and pumping system

ARIES- LSA	RS	AT	CS		
			9/05	1/06	3/06
VV	62 (20-30 cm)	922 (25-40 cm)	53 (28 cm)	55 (28 cm)	? (~55) (28 cm)
Cryostat	100 (4.3 cm)	9 (0.4 cm)	0 (0 cm)	? (~75) (8 cm)	? (~50) (5 cm)
Pumping System*	38	23	81	?	?
21.1.6 Vacuum System (M\$- 2004\$)	200	124	134	96 (should be >130)	? (should be >100)

ARIES-CS pumping system is too expensive. Why?

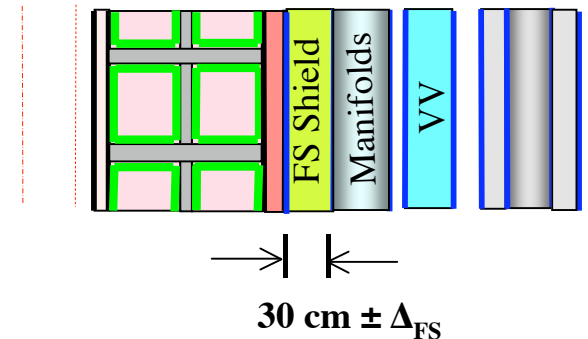
* Depends on plasma parameters.

Shield vs NWL Scaling Law

(Near-final radial build; average $\bar{\phi} \sim 3 \text{ MW/m}^2$)

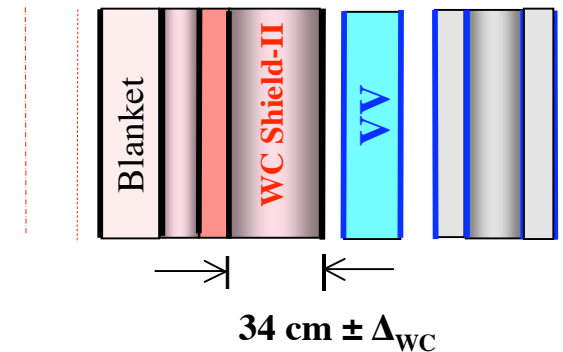
- Incremental change to nominal 30 cm FS shield:

$$\Delta_{\text{FS-shield}} = 7.3 \ln(\bar{\phi} / 3)$$



- Incremental change to 34 cm WC shield-II @ Δ_{min} :

$$\Delta_{\text{WC-shield-I}} = 5.9 \ln(\bar{\phi} / 3)$$



* Δ in cm and average $\bar{\phi}$ in MW/m^2 .



Cryogenic Heat Load to Magnet

(Near-final radial build; average $\dot{Q} \sim 3 \text{ MW/m}^2$)

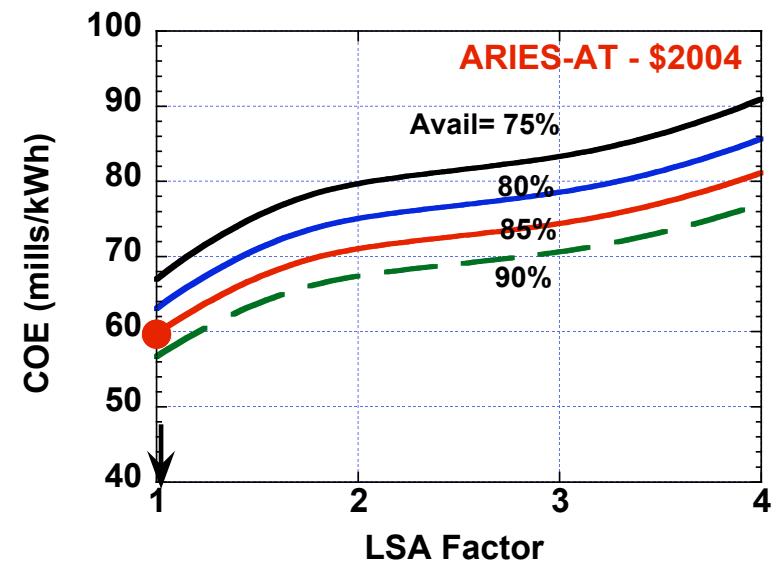
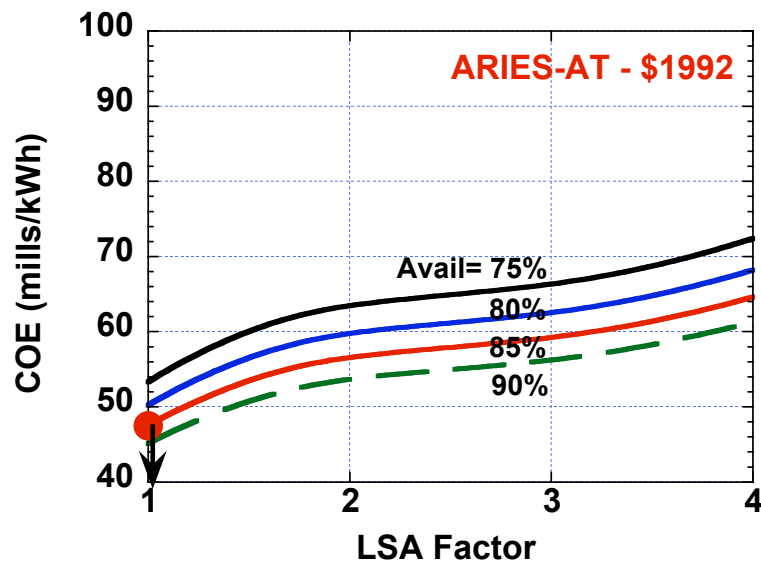
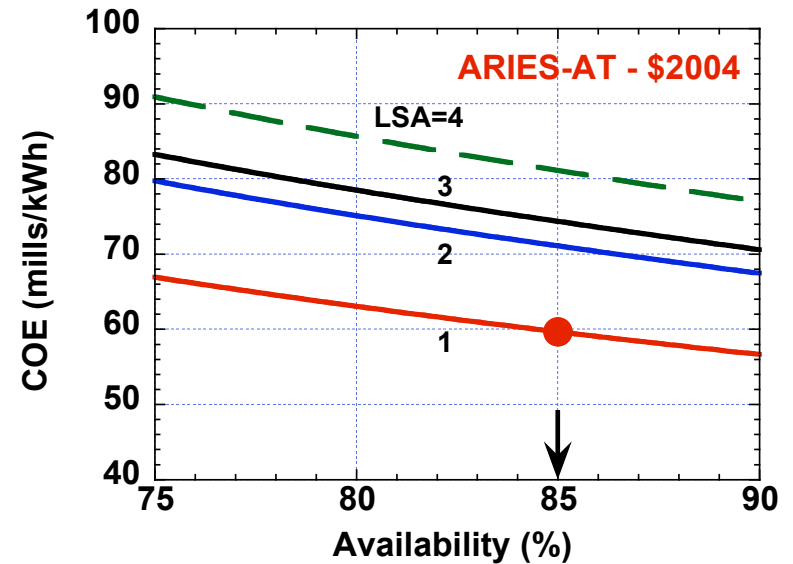
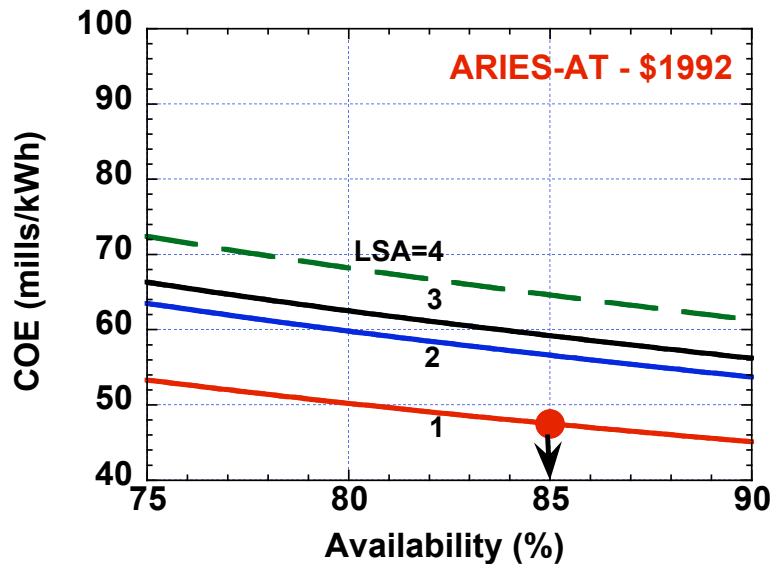
Assumptions:

- Winding packs (WP) cover 32% of area.
- Inter-coil structure covers 68% of area.
- WP and structure @ 4K.
- 300 W_e to remove 1 W of nuclear heating.

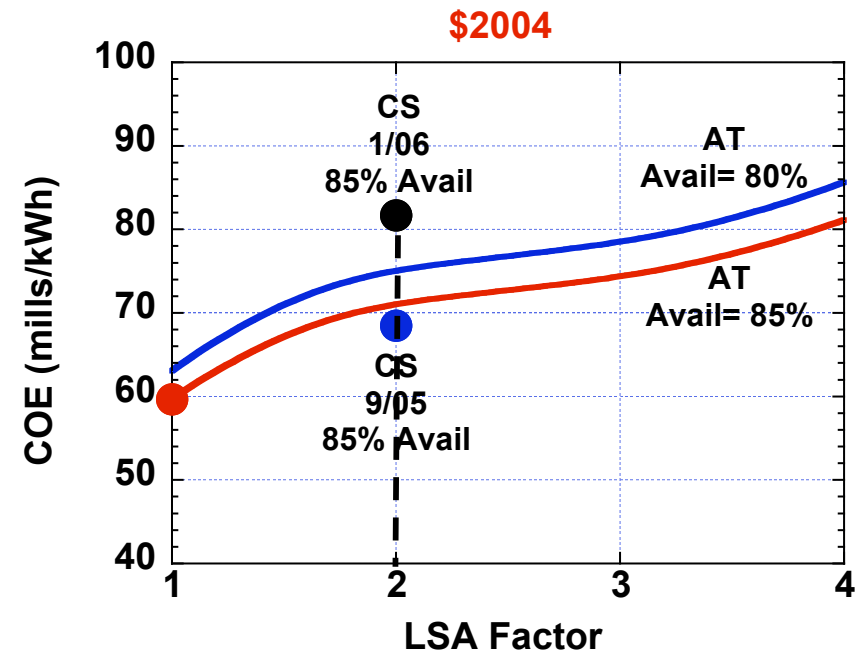
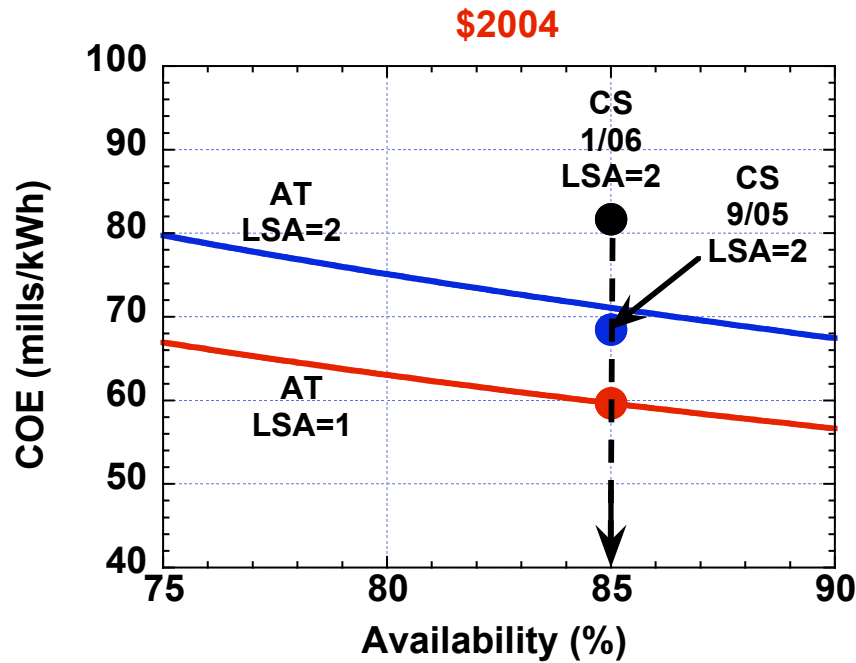
	Nuclear Heating (kW)	Cryogenic Load (MW _e)
2 cm Coil Case	2.0	0.6
18 cm Winding Pack	2.9	0.7
66 cm External Structure*	0.07	0.02
subtotal	<u>5</u>	<u>1.5</u>
35 cm Inter-coil Structure	10.7	3.2
Total	16 kW	~ 5 MW_e

* Behind WP only.

Sensitivity of **ARIES-AT** COE to Availability and LSA

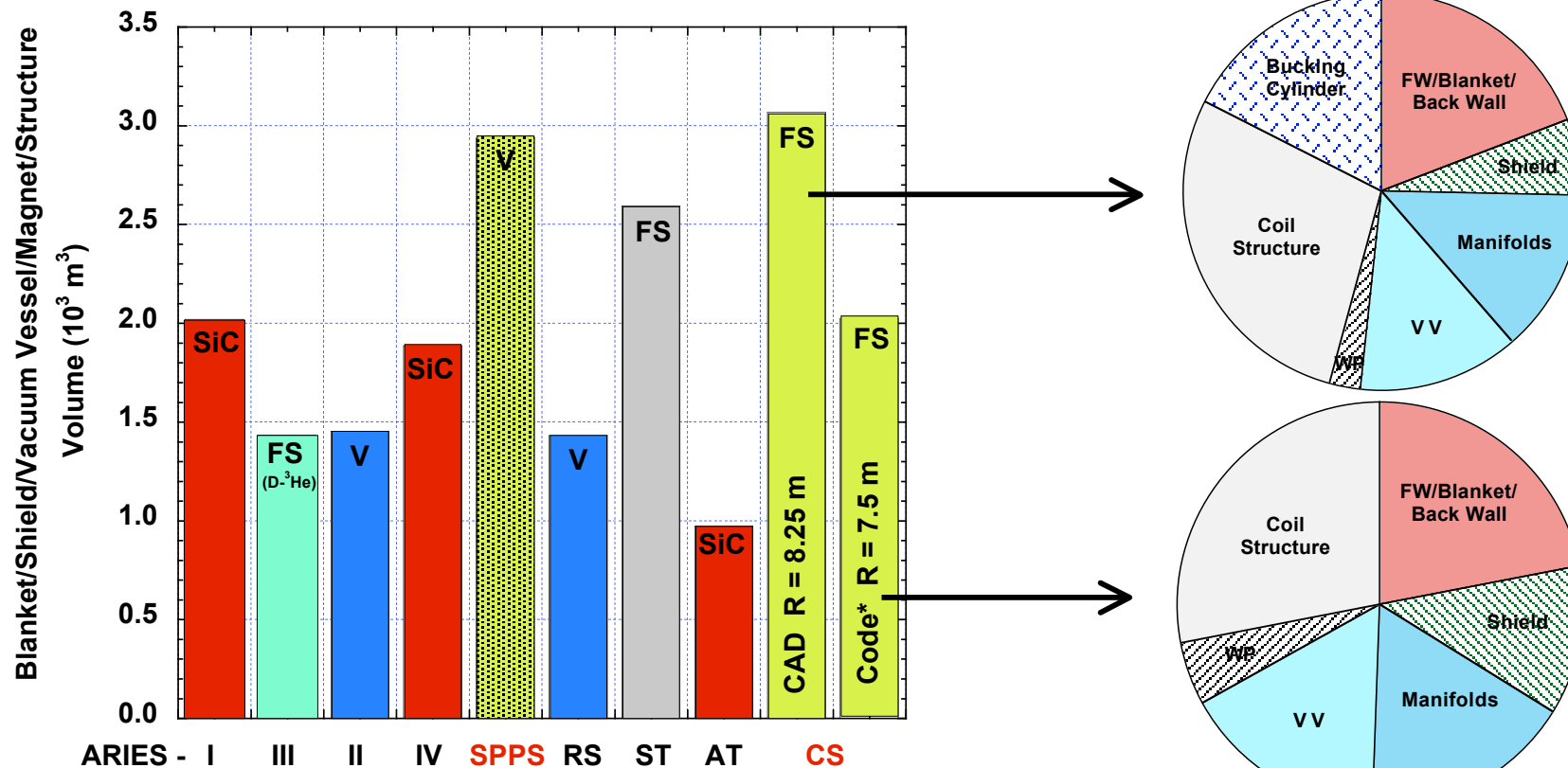


Sensitivity of COE to Availability and LSA



Radwaste Volume Comparison

(not compacted, no replacements)
(cryostat and bioshield excluded)



Compared to 8.25 m machine, more compact 7.5 m ARIES-CS
and removal of bucking cylinder reduced waste volume by 30%

Future Plan

- Changes to Systems code:
 - 30 \$/kg of WC, per Les
 - availability: 80 or 85% ? TBD.
- Provide radial build for **LiPb/SiC design** to systems code
- Provide radial build for **2 FP configuration** to systems code