

Design Definition of Stellarator Coil Systems

L. Bromberg, J.H. Schultz

MIT Plasma Science and Fusion Center

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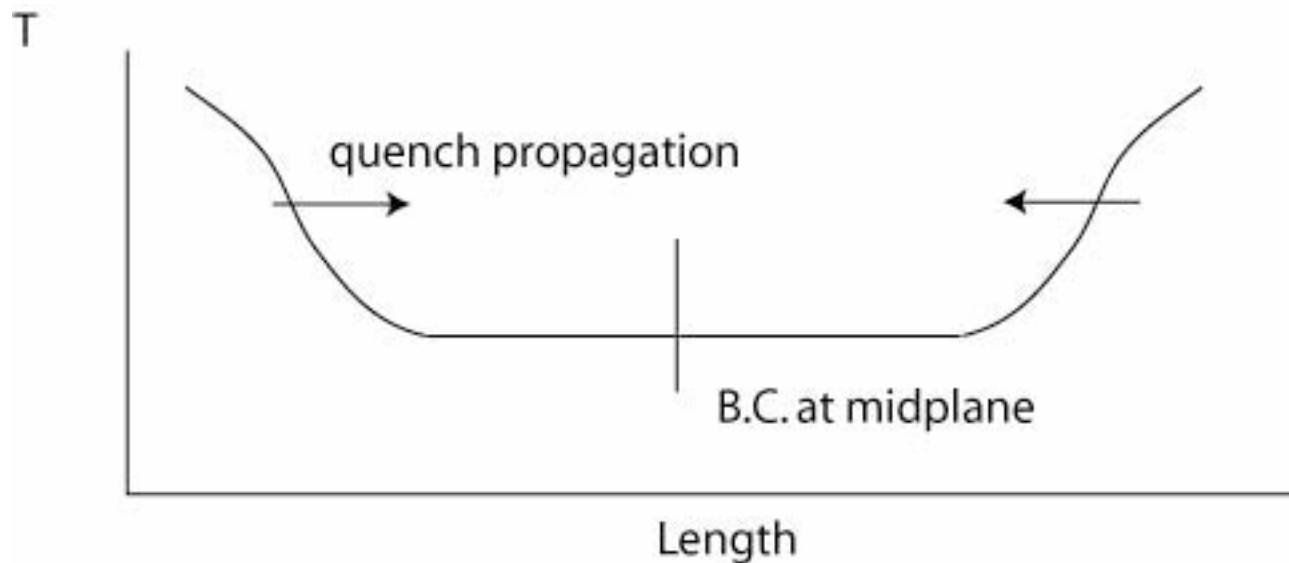
Review of SC options

- High T_c
 - Epitaxial on structure
- Nb_3Sn
 - Wind and react
- Nb_3Sn
 - React and wind
 - “Heresy” proposed at the last meeting

Magnet protection

- Large amount of energy needs to be removed from the magnet
 - Difficult to do with low current (implies high voltage)
- Large magnets for HEP are designed for internal dump, as well as MRI magnets
- Requires conductor heating from a resistive heater (over most of the magnet) to drive conductor normal
 - Requirement $T_{\text{conductor}} \sim 10\text{K}$ (for Nb_3Sn , Nb_3Al), requiring $\sim 20 \text{ J/kg}$ (0.4 J/cm^3)
 - Energy required $\sim 100 \text{ m}^3$ of conductor $\sim 100 \text{ MJ}$
 - For 0.2 s initiation of quench, 100 MW

Superconducting coil protection by use of periodic heaters

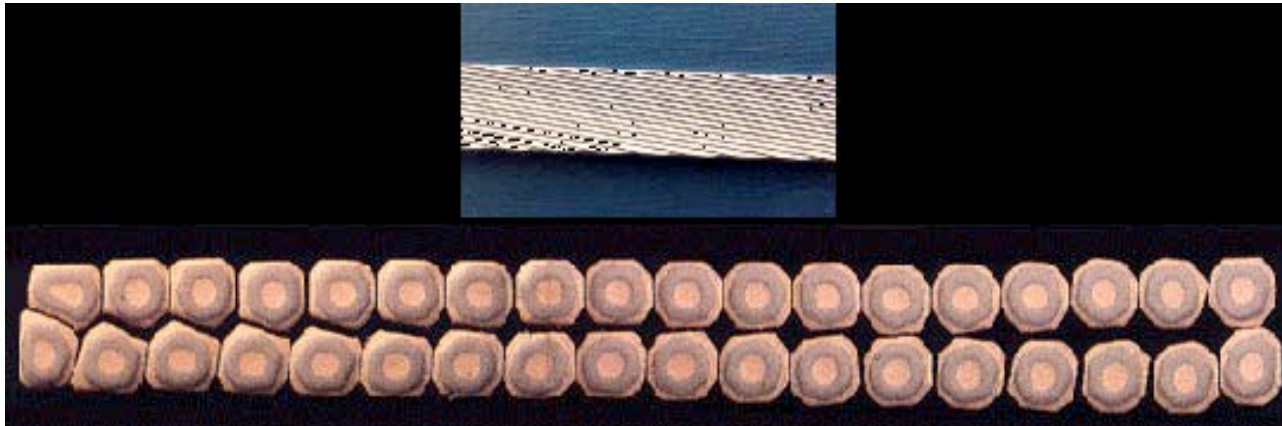


Resistive quench in internal dump

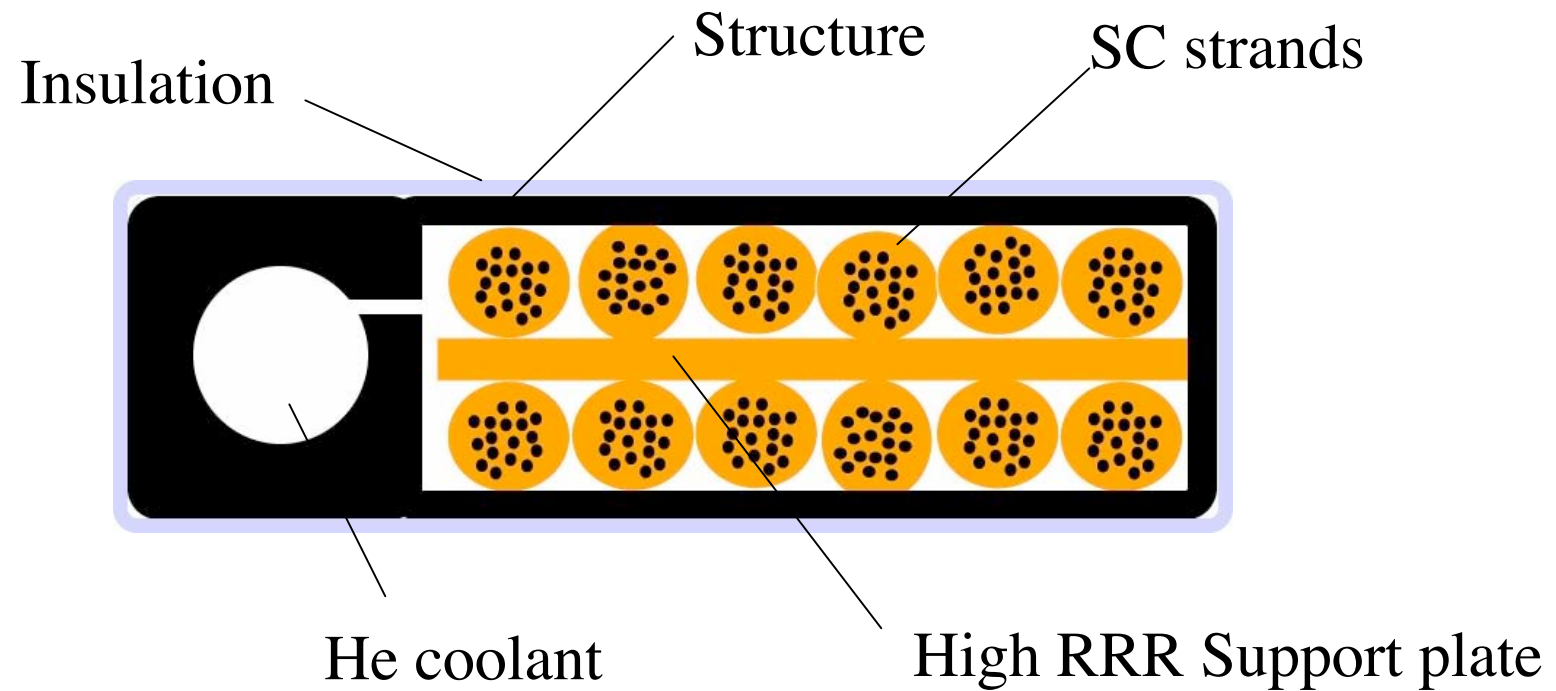
- Low temperature superconductors have relatively high normal zone propagation velocity
 - Several m/s
 - 1 m/s for highly protected SC
 - 10 m/s for lightly protected
- If locally the conductor is heated in a zone smaller than the minimum propagation zone, the normal zone will shrink (recover)
 - Minimum propagation zone in SC is ~ 1 cm.
 - Produce local heating in SC magnet, and depending in quench propagation to fill in through the rest of the coil
 - Does result in increased temperature uniformity, but has the advantage of reducing power required
 - Heater has high resistivity elements about 1 cm long, spaced about 1 m
 - Power decreased by 2 orders of magnitude!

Conductor implications of internal quench

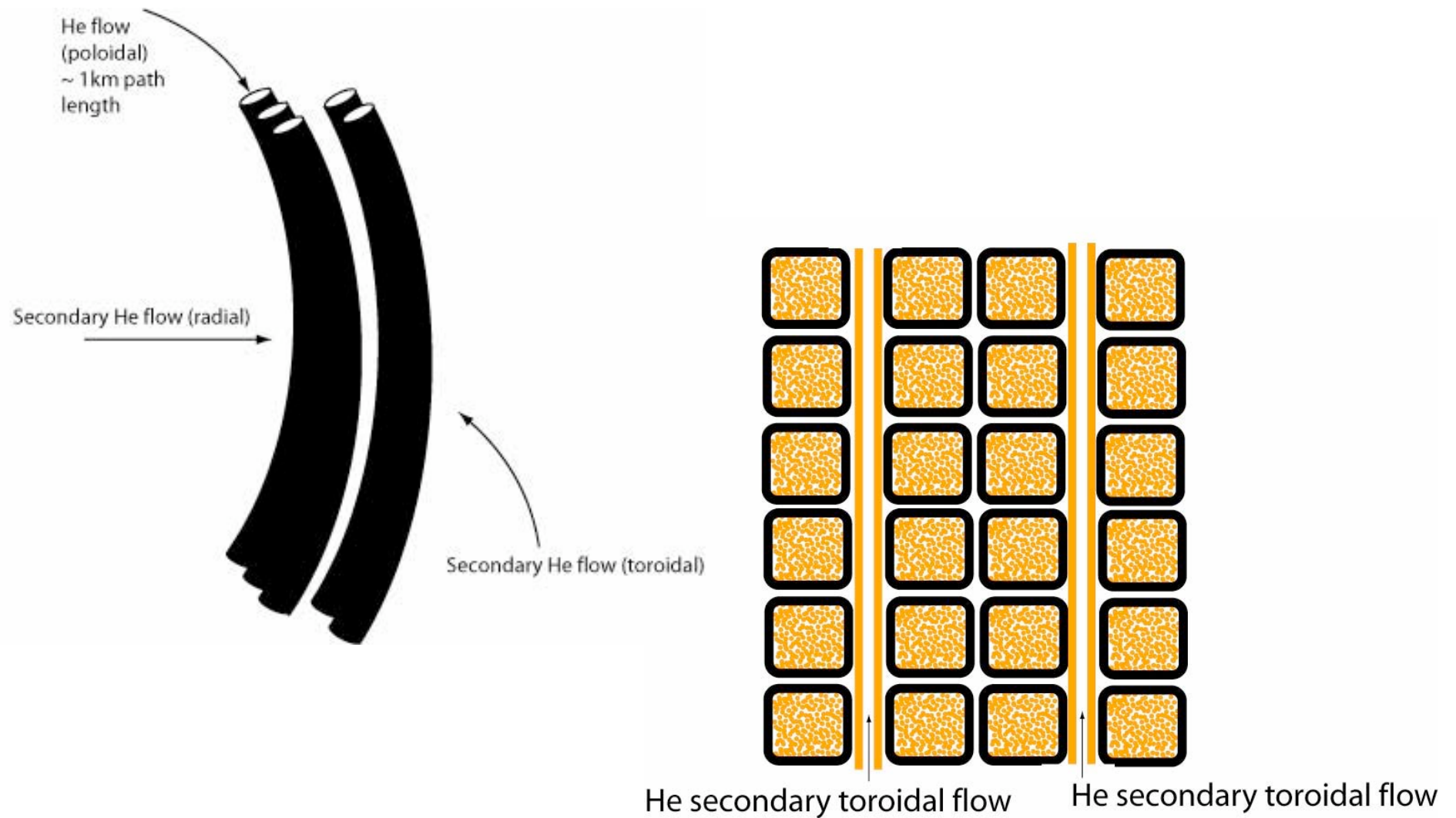
- Low current, small conductor, can use react and wind!
- Can use Rutherford-like cables (conventional high performance cables used in accelerators)
- Largest Rutherford cable made from 60 strands (vs ~ 1000 strands for CICC).
- If quench is symmetrical, no voltages are induced
 - Inductive voltage balances resistive voltage
 - If non-uniform heating, uncanceled voltages will appear
 - Need to determine actual voltages



Cooled-Rutherford cable



Multi-loop cooling



Quench propagation code under development

- Comparable temperature between He and conductor
- Detailed electrical properties of materials (heat capacity of metal ignored)
- He properties from tables
 - Heat capacity, density
- Problem:
 - Boundary condition $v = 0$ changes the problem to eigenvalue problem

Analytical model

- For short coils (with pressure relieve)

$$V_q = \sqrt[3]{\frac{2dR}{fL_{\text{coil}}} L_{IQZ} \alpha_0 J^2} \quad X_q = \left[\left(\frac{L_{IQZ}}{2} \right)^{3/2} + (V_q t)^{3/2} \right]^{2/3}$$

- For long coils (and high pressure):

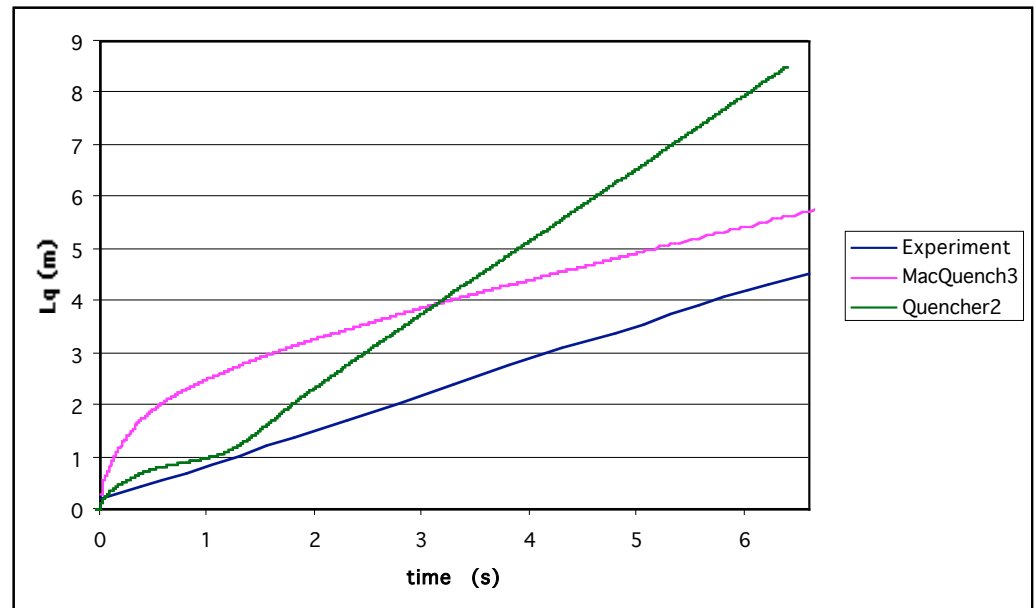
$$V_q = 0.613 \left(\frac{2d_h}{f} \right)^{1/5} \left(\frac{RL_{IQZ} \alpha_0 J^2}{c_0} \right)^{2/5} \frac{1}{t^{1/5}}$$

Preliminary data

- Initial velocities for ARIES CS ~ 5 m/s
 - If distance between normal IPZ ~ 1 m , 200 ms for quench
 - Need to determine temperature differential
 - dump to occur in ~ 2 s, so 200 ms is substantial
 - Fast rate of decrease of field provides additional heating of conductor
 - Hysteresis, AC coupling, eddy current losses

Quencher2 vs MacQuench preliminary simulations with wrong B.C.

- Quencher2 is better for earlier times
- This is the region of interest (times < 1 s)
- Checked with data of SULTAN (cryogenic EU test) for ITER



Model of quench

- Because of symmetry, at midplane between heating zones:
 - $dT/dx = 0$
 - $v_{\text{He}} = 0$
- These boundary conditions are very different from previous models of quench in CICC
 - $dT/dx = 0$ with v non-zero results in boundary layers at the ends
 - $d^2T/dx^2 = 0$ is used in the most modern quench propagation codes.

Structural issues

- Helium is not going anywhere
 - Thus, large pressure increase when heated
 - Constant volume heating of He results in increases in pressure of ~ 300 to room temperature
 - Initial He pressure ~ 0.6 MPa (6 bar, 4.5 K, above critical point of He).
 - Final pressure, if 150 K temperature, of 80 MPa
 - Sheath around superconductor should be able to support these pressures
 - Typical numbers: 10 mm wide (32 strands), 1 mm sheath, 400 MPa stresses
 - Detailed stress analysis in progress.

Future work

- Finish work on code for modeling quench propagation in Rutherford-like CICC with distributed heaters
 - Get approximate velocities of propagation for ARIES-CS, even if full model is not working
- Paper accepted at Applied Superconductivity Conference
- MIT reviewing patent disclosure on periodic localized heater for large superconducting coils