

Status ARIES-AT Blanket and Divertor Design

The ARIES Team

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ARIES Project Meeting
University of California, San Diego
March 20-21, 2000

Presentation Outline

- **Blanket**
 - Geometry and coolant routing
 - Analysis
 - MHD flow considerations
 - Temperature and thermal stress
 - Pressure stress
- **Divertor**
 - Configuration with LiPb as coolant
 - Preliminary flow analysis
- **Future Work**

ARIES-AT Machine and Power Parameters Used for Analysis

Power and Neutronics Parameters

• Fusion Power	1737 MW
• Neutron Power	1390 MW
• Alpha Power	347 MW
• Current Drive Power	41 MW
• Transport Power to Divertor	289 MW
• Fraction of Divertor Power Radiated Back to FW	0.2
• Overall Energy Multiplication	1.1
• Total Thermal Power	1927 MW
• Average FW Surface Heat Flux	0.5 MW/m ²
• Max. FW Surface Heat Flux	0.7 MW/m ²
• Max. Divertor Surf. Heat Flux	5 MW/m ²
• Average Wall Load	4.3 MW/m ²
• Maximum O/B Wall Load	6.1 MW/m ²
• Maximum I/B Wall Load	4.0 MW/m ²

Machine Geometry

• Major Radius	4.8 m
• Minor Radius	1.2 m
• FW Location at O/B Midplane	6 m
• FW Location at Lower O/B	4.8
• I/B FW Location	3.6 m

Toroidal Magnetic Field

• On-axis Magnetic Field	7.5 T
• Magnetic Field at I/B FW	10 T
• Magnetic Field at O/B FW	6 T

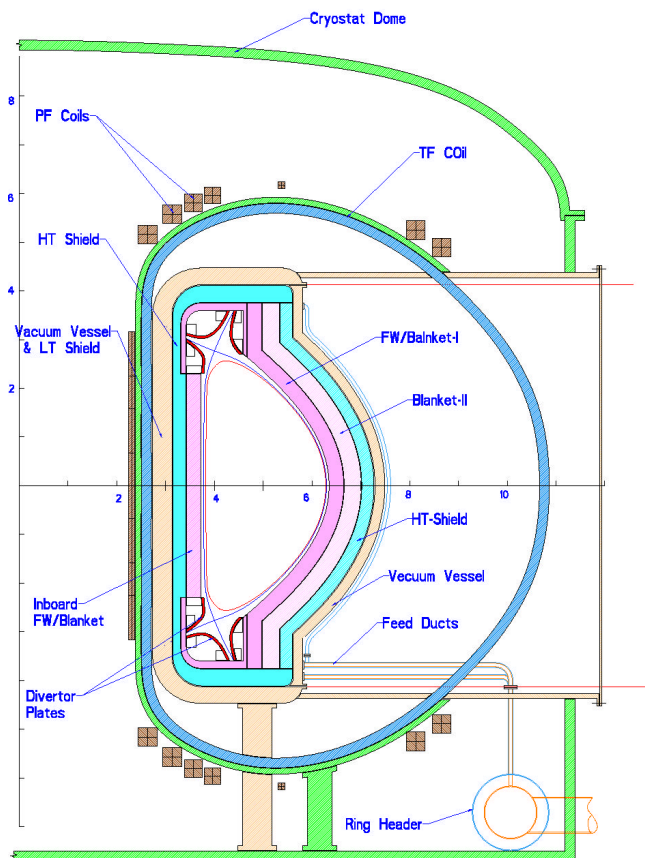
SiC/SiC Properties Used for Design Analysis

(Consistent with SiC/SiC Town Meeting Suggestion)

• Density	~3200 kg/m ³
• Density Factor	0.95
• Young's Modulus	~200-300 GPa
• Poisson's ratio	0.16-0.18
• Thermal Expansion Coefficient	4 ppm/°C
• Thermal Conductivity in Plane	~20 W/m-K
• Therm. Conductivity through Thickness	~20 W/m-K
• Maximum Allowable Combined Stress	~190 MPa
• Maximum Allowable Operating Temperature	~1000 °C
• Max. Allowable SiC/LiPb Interface Temperature	~1000°C
• Maximum Allowable SiC Burnup	~ 3%

Cross-Section of ARIES-AT Showing Power Core Components and Coolant Routing (Preliminary)

Cross-Section of ARIES-AT Power Core



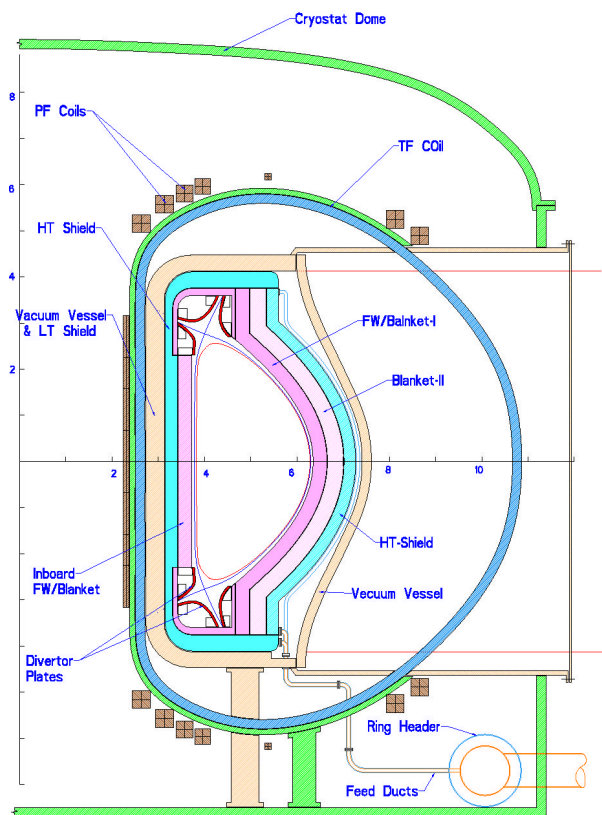
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- **LiPb Coolant**
 - Inlet/Outlet Temperatures 653/1100 °C
 - Inlet Pressure ~2.5 MPa (Divertor-dependent)
- **Circuit 1 - Lower Divertor + I/B Blkt Region**
 - Thermal Power 535 MW
 - Mass Flow Rate 6500 kg/s
- **Circuit 2 - Upper Divertor + 1st O/B Blkt Region**
 - Thermal Power 1040 MW
 - Mass Flow Rate 12,700 kg/s
- **Circuit 3 - Hot Shield + 2nd O/B Blkt Region**
 - Thermal Power 352 MW
 - Mass Flow Rate 4270 kg/s

Cross-Section of ARIES-AT Showing Power Core Components and Alternate Coolant Routing

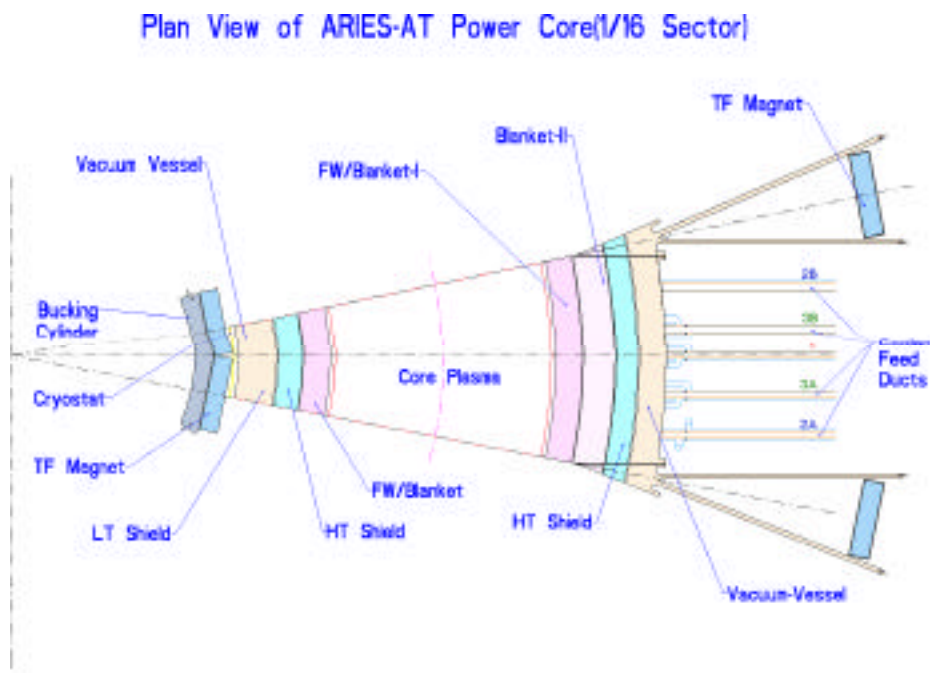
Cross-Section of ARIES-AT Power Core



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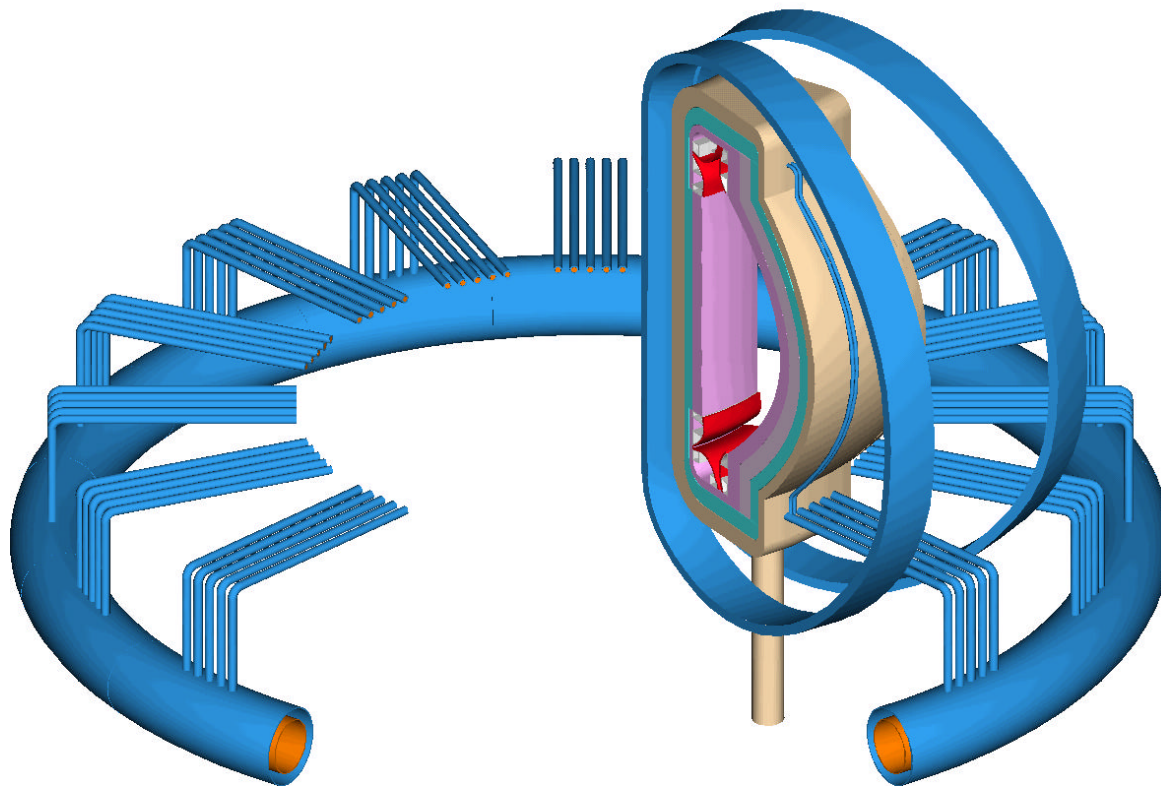
Plan View of ARIES-AT Power Core (Preliminary)



- **Circuit 1 - Lower Divertor + I/B Blkt Region**
 - Thermal Power 535 MW
 - Mass Flow Rate 6500 kg/s
- **Circuit 2A - Upper Divertor + 1st O/B Blkt Region**
 - Thermal Power 587 MW
 - Mass Flow Rate 7168 kg/s
- **Circuit 2B - 1st O/B Blkt Region**
 - Thermal Power 453 MW
 - Mass Flow Rate 5532 kg/s
- **Circuit 3A - I/B Hot Shield + 2nd O/B Blkt Region**
 - Thermal Power 188 MW
 - Mass Flow Rate 2282 kg/s
- **Circuit 3B - O/B Hot Shield + 2nd O/B Blkt Region**
 - Thermal Power 164 MW
 - Mass Flow Rate 1988 kg/s

Example Coolant Manifold for ARIES-AT Power Core

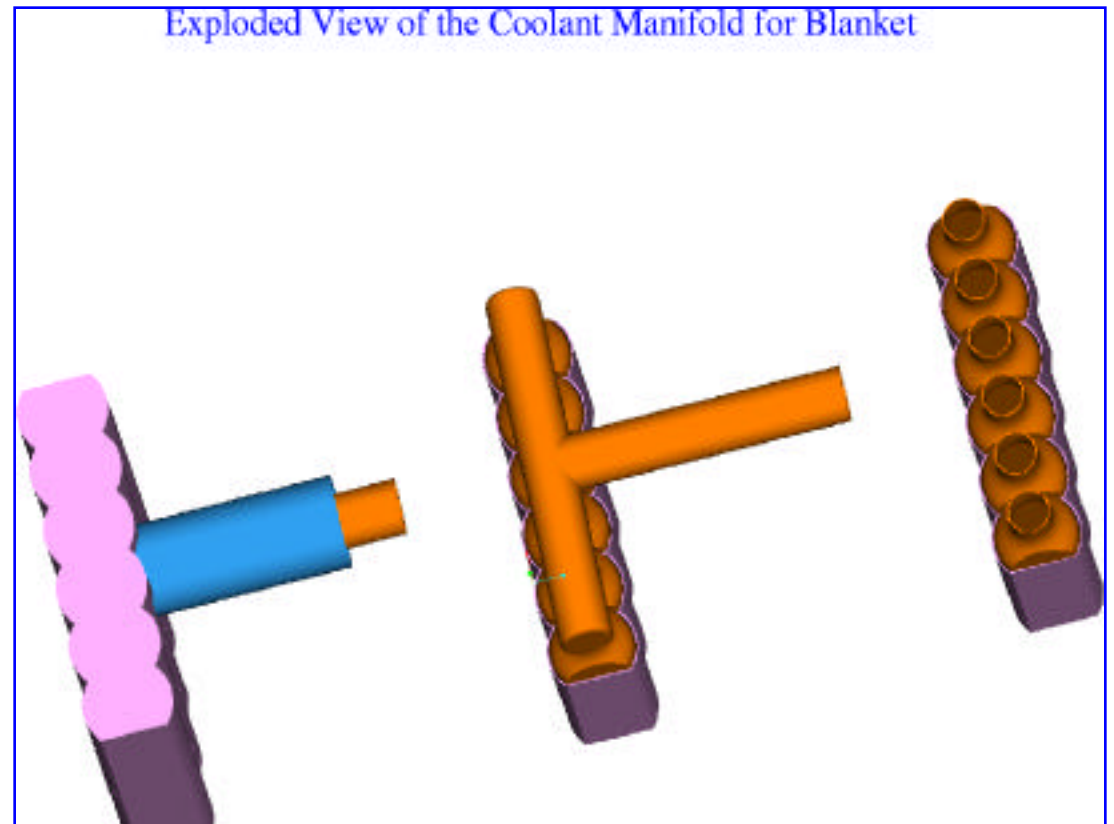
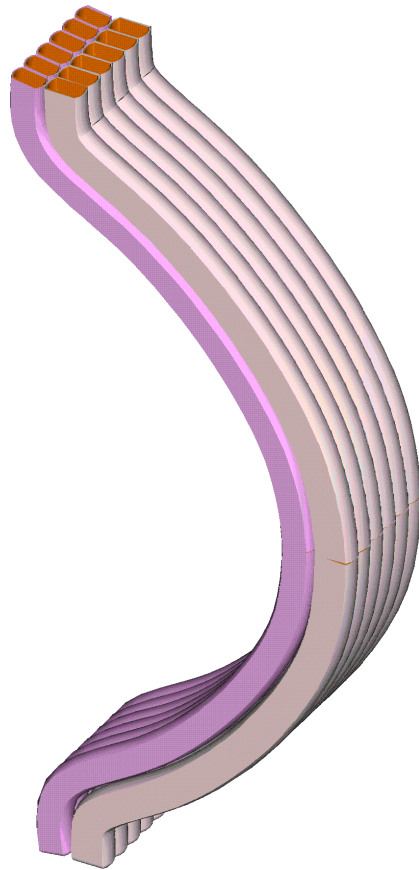
Layout of Coolant Manifold for ARIES-AT Power Core



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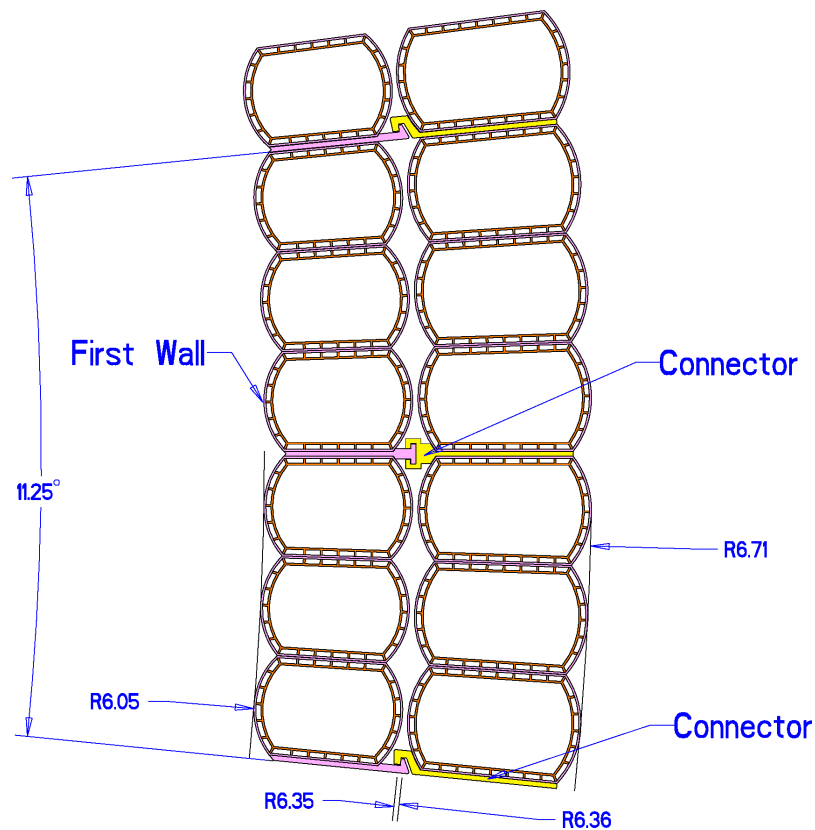
ARIES-AT Outboard Blanket Segment Configuration



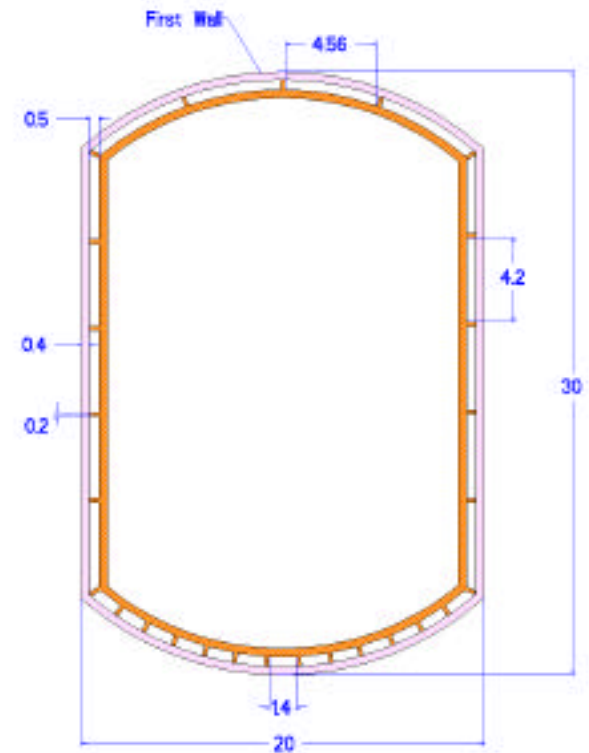
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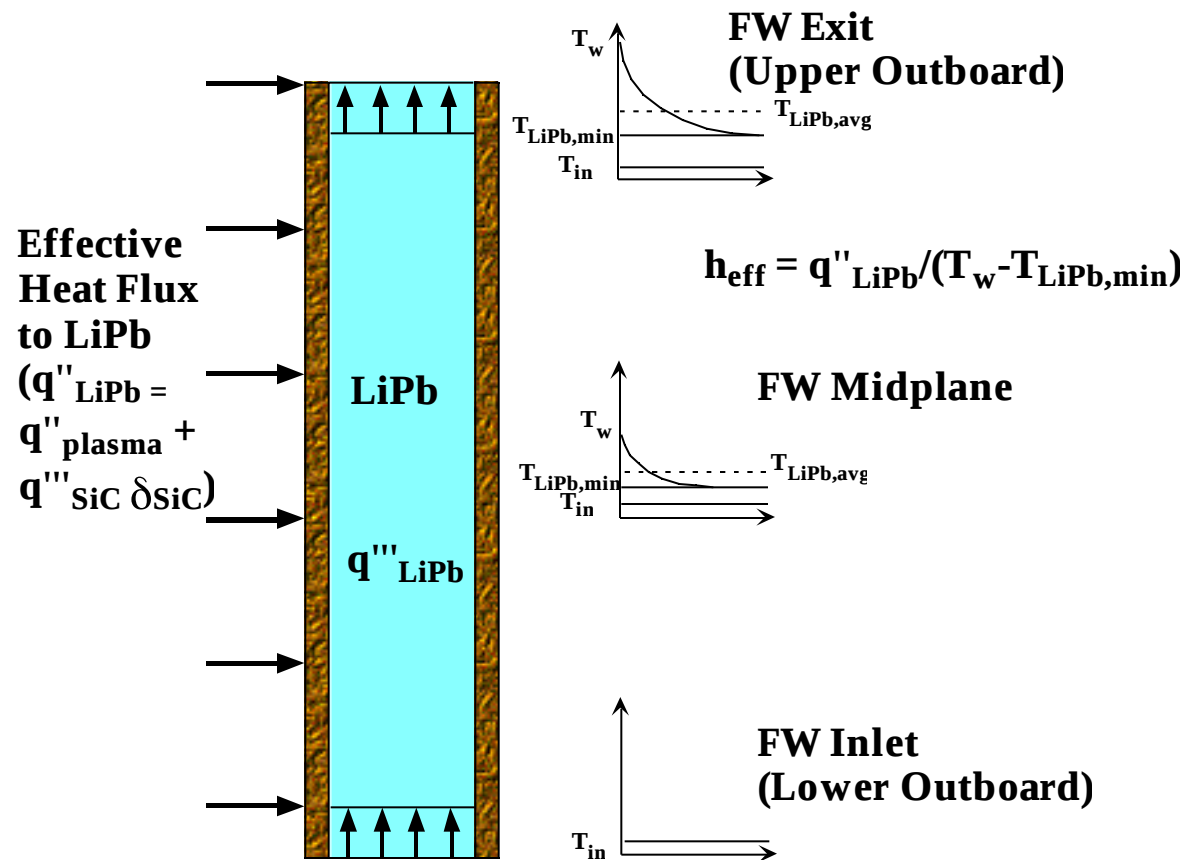
Cross-Section of ARIES-AT Outboard Blanket



Cross-Section of ARIES-AT Outboard FW/Blanket
(Unit in cm)

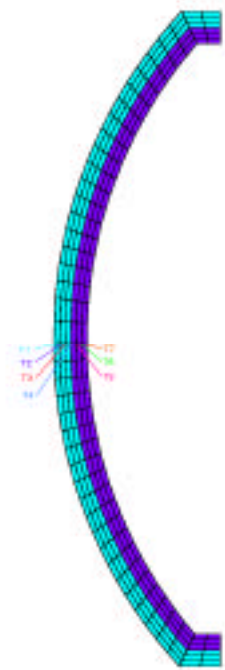


LiPb Temperature Distribution in FW Poloidal Channel under MHD-Laminarization Effect



2-D Moving Coordinate Analysis of FW

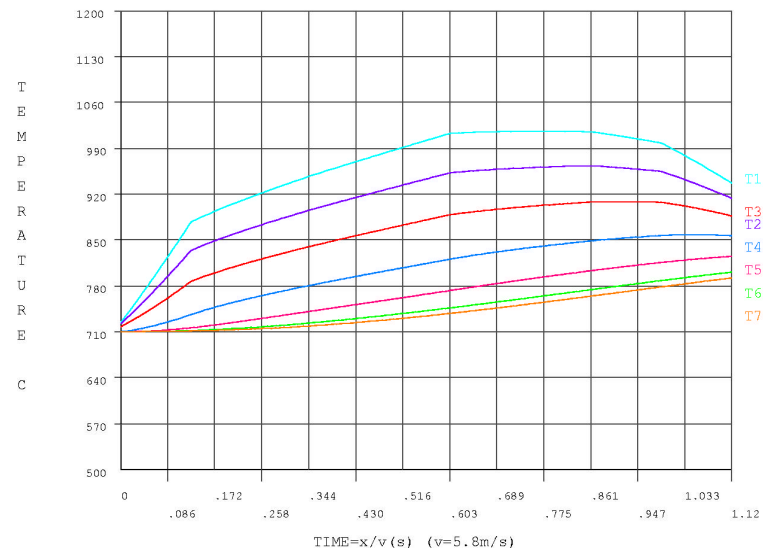
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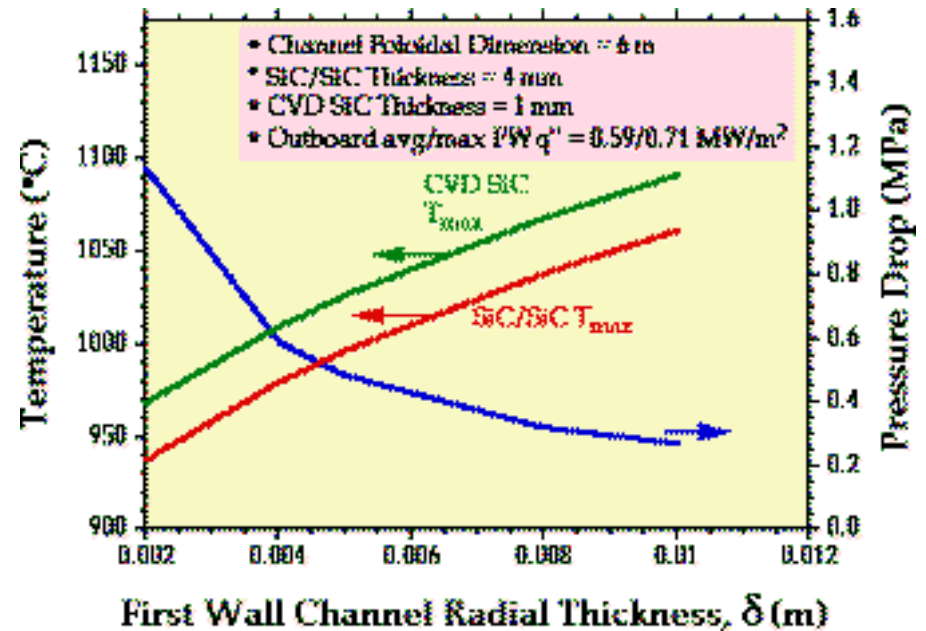
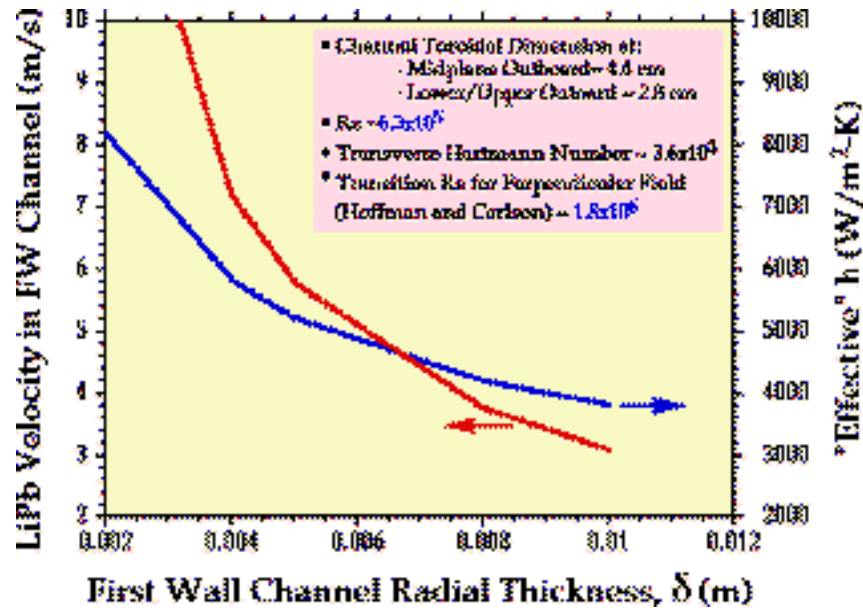
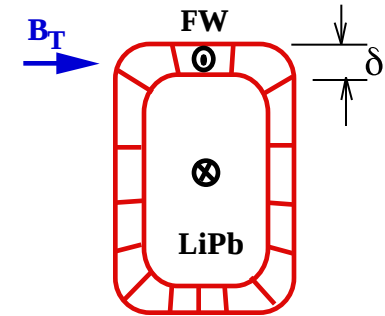
**Toroidal-Radial Plan View of Blanket
Outboard Region 1**

- Transient analysis of 2-D FW geometry over LiPb residence time to simulate 3-D situation under the assumption of conduction only in LiPb
- Heat flux and heat generation varied over time to reflect poloidal variation

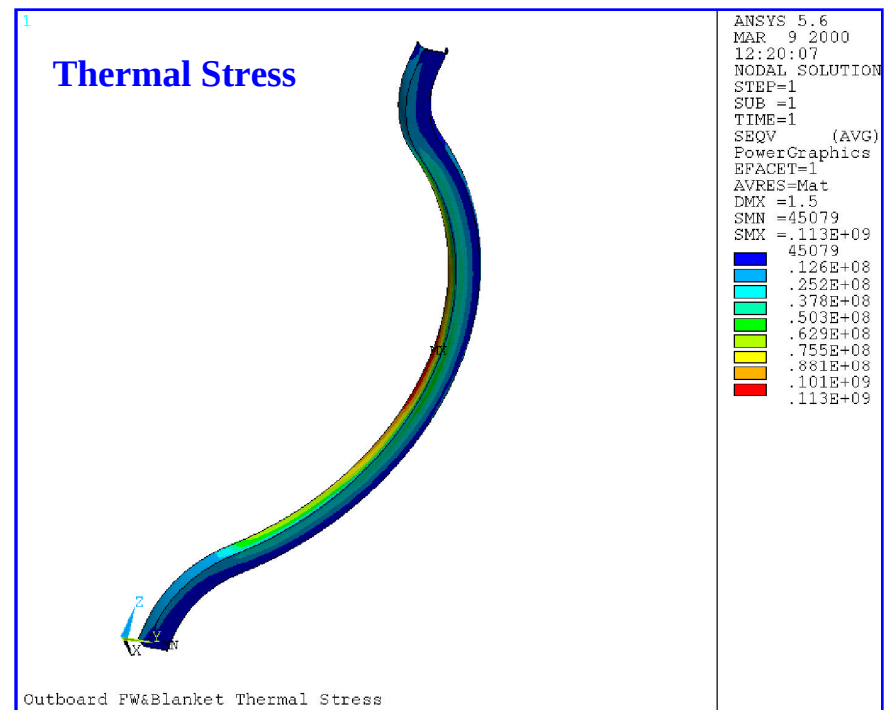
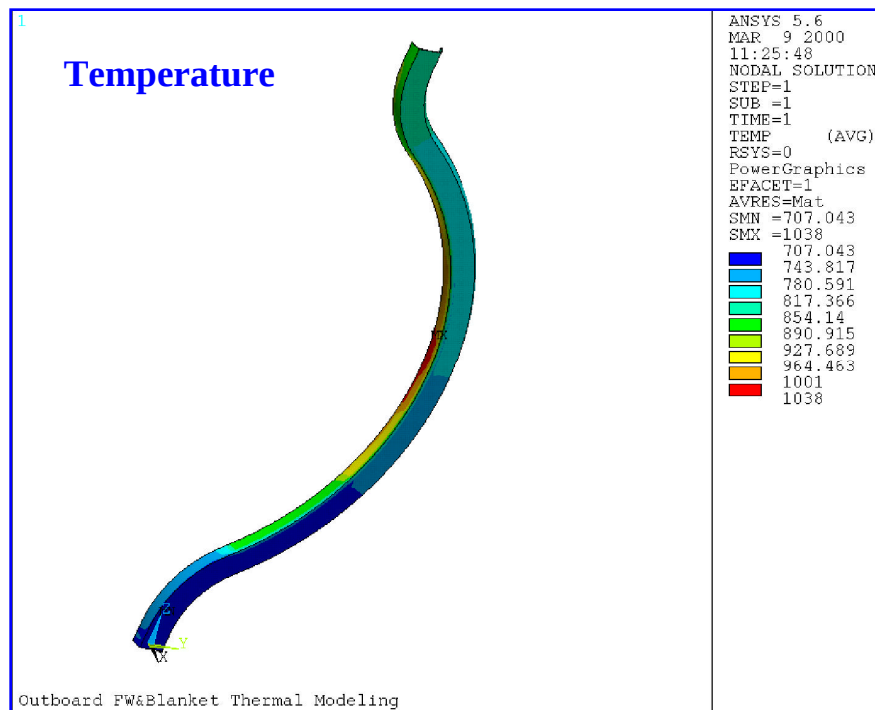
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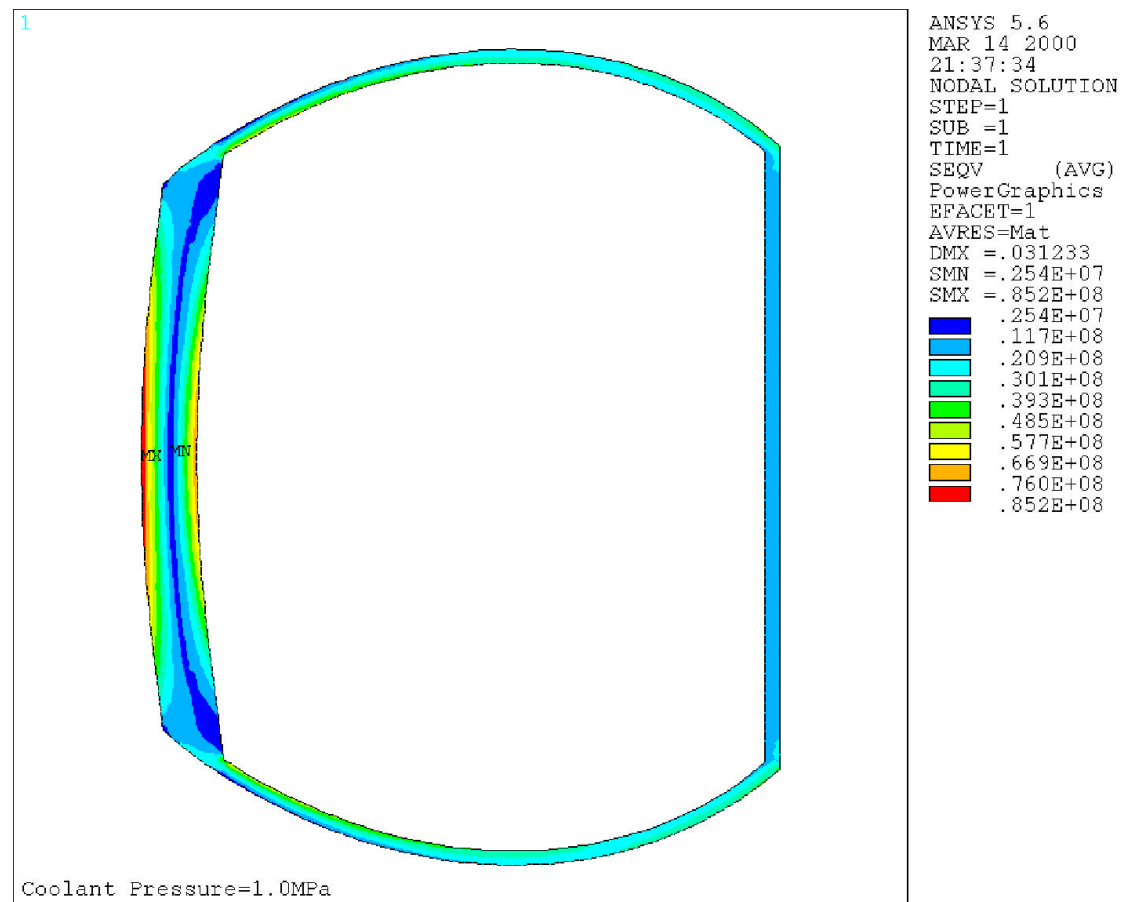
Flow and Thermal Parameters for LiPb-Cooled FW of Outboard Region 1 as a Function of FW Channel Thickness



3-D Thermal Analysis of Toroidal Half of Outboard Blanket Region 1



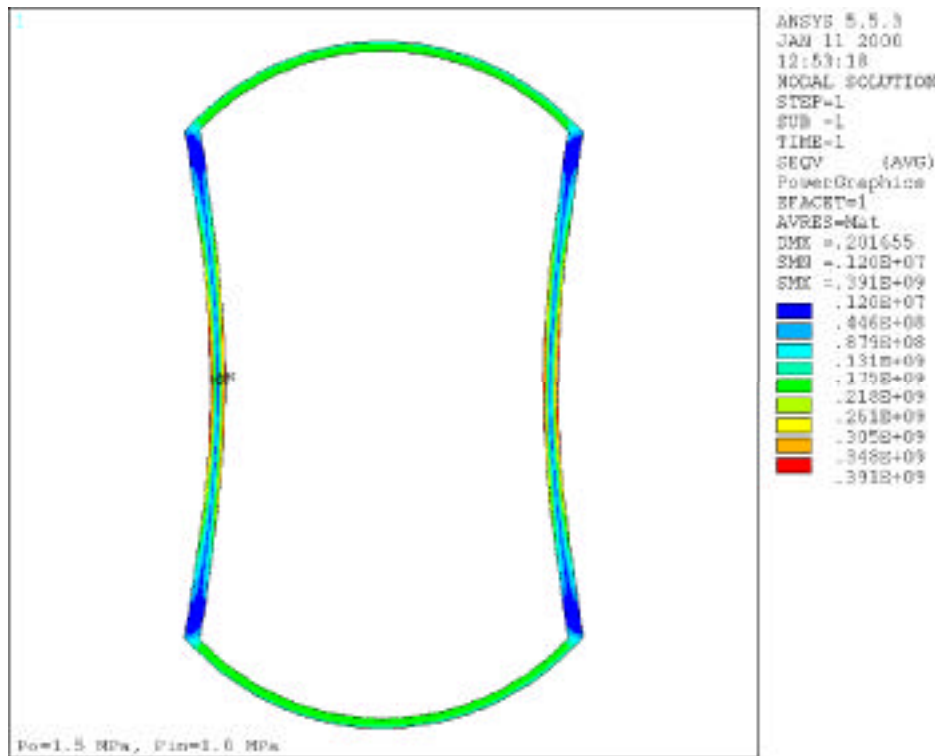
Pressure Stress Analysis of Outer Shell of Blanket Module at Segment End



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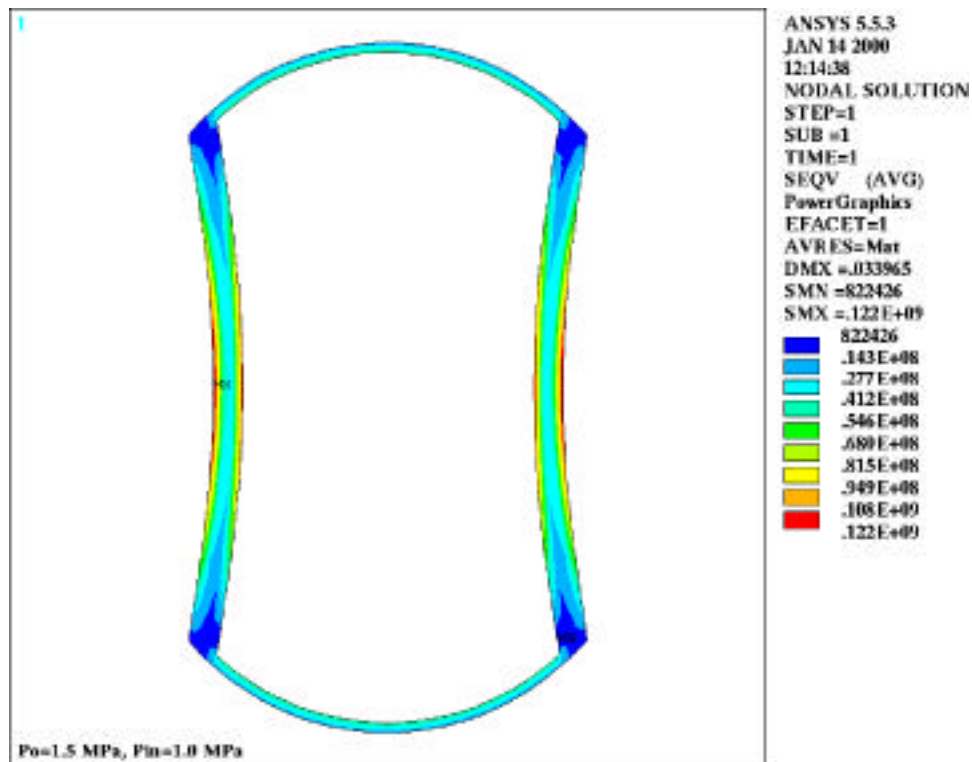
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Pressure Stress Analysis of Inner Shell of Blanket Module



- **Maximum Differential Pressure Stress on Blanket Module Inner Shell ~ 0.5 MPa**
- **Thermal stress is too high for original thickness of 5mm**
- **Solution**
 - Increase thickness
 - Add rib for same thickness

Increasing Inner Shell Thickness to Accommodate Pressure Stress

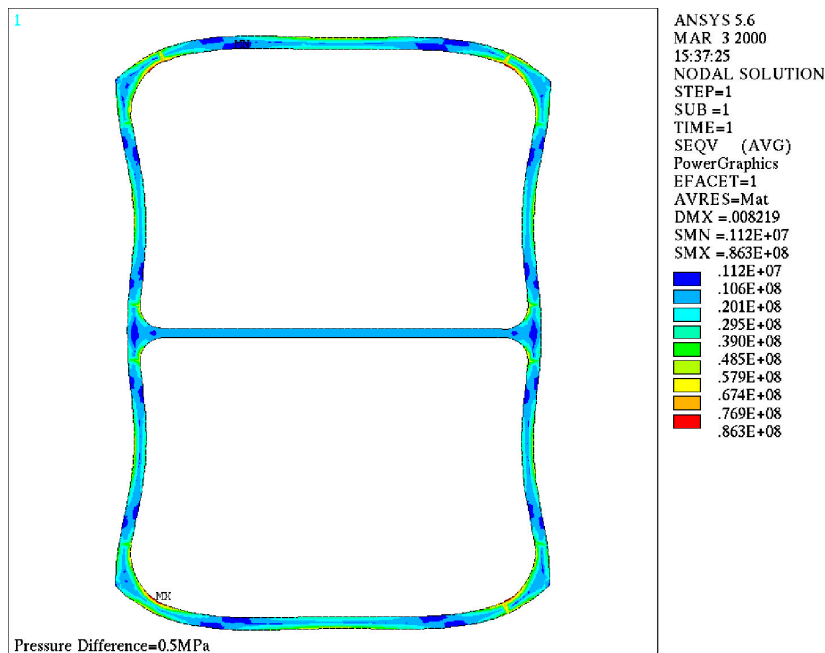


- Maximum pressure stress is 122 MPa for 1.5-cm thickness
- Thermal Stress probably small
- Effect on TBR
- Thickness can be poloidally tapered to account for local pressure differential value

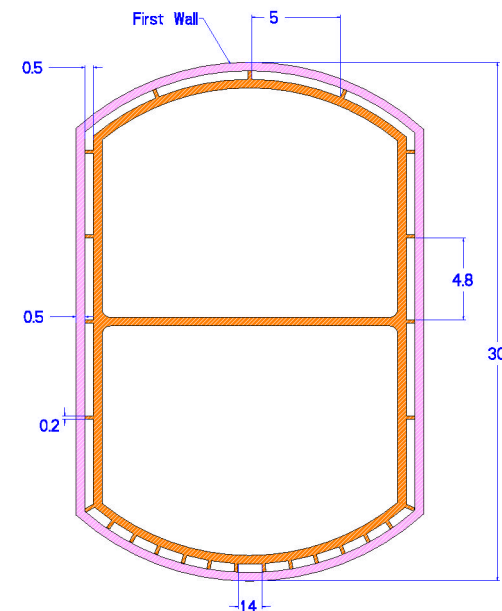
Adding Rib to Inner Shell as an Alternative Option Increasing to Accommodate Pressure Stress

- Maximum pressure stress is low, 86 MPa
- Minimal Effect on TBR

- Add complexity to manufacturing
- Rib must be cooled
- Familiar look!



Cross-Section of ARIES-AT Outboard FW/Blanket
(Unit in cm)

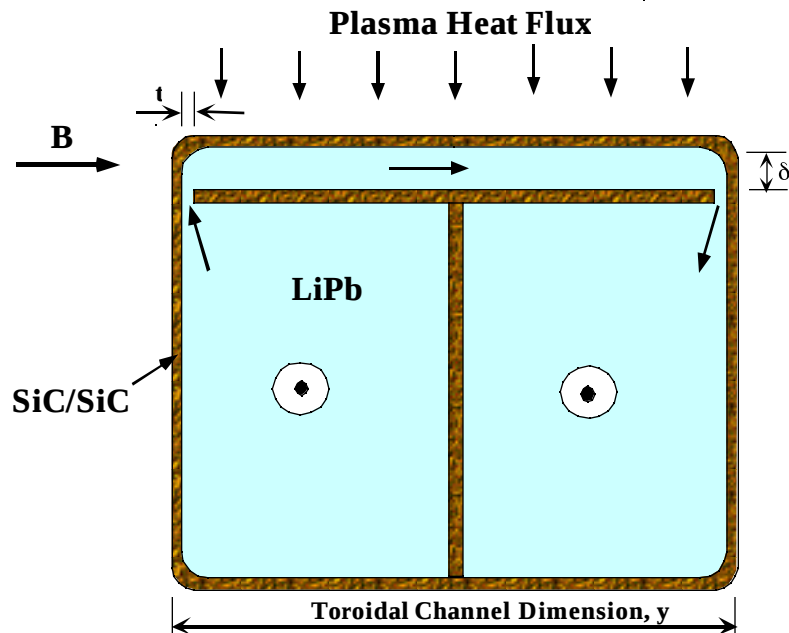


Divertor Design Considerations

- **Compatibility with Blanket Configuration and Coolant**
- **Structural Material**
 - SiC/SiC thickness $< 1\text{mm}$
($\sigma_{\text{th}} \sim 235\text{ MPa}$ and $\Delta T_{\text{SiC}} = 250^\circ\text{C}$ for $q'' = 5\text{ MW/m}^2$)
 - W with thin SiC insert with or without structural function
- **Possible Concepts**
 - Dry Wall
 - LiPb as coolant (Preferable to avoid in-reactor high pressure He but needs innovative scheme because of poor heat transfer removal capabilities)
 - Porous W HX concept with He coolant as in ARIES-ST
 - Phase-change liquid metal (Li)
 - Liquid Wall (Sn-Li)

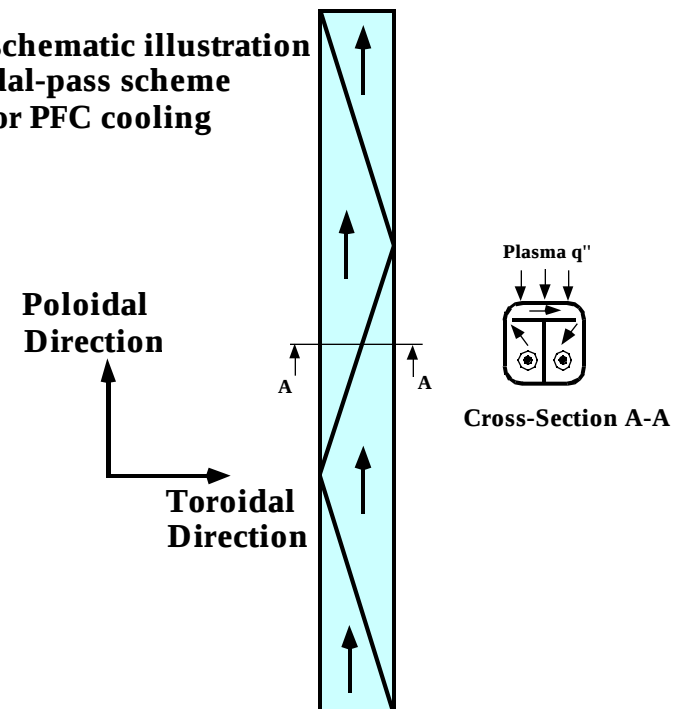
LiPb Cooling Scheme for ARIES-AT Divertor

LiPb Poloidal/Toroidal Flow for ARIES-AT Divertor

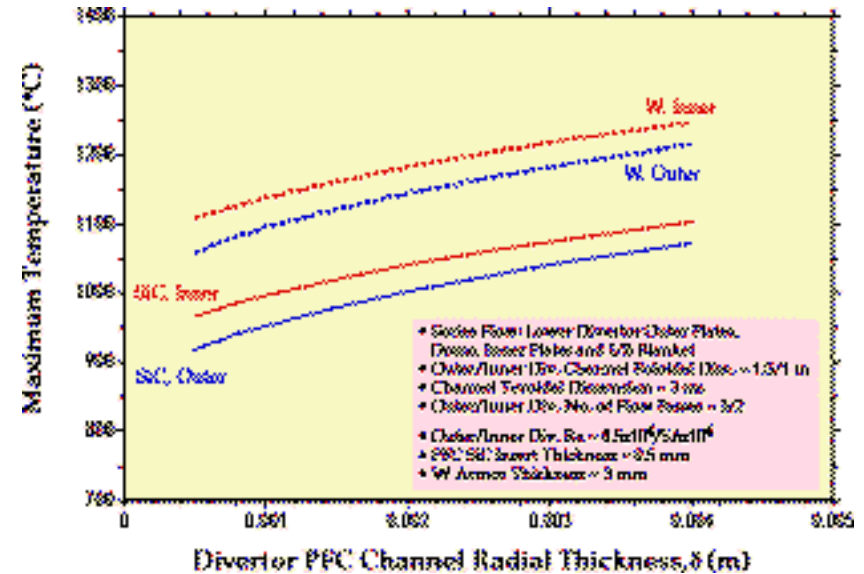
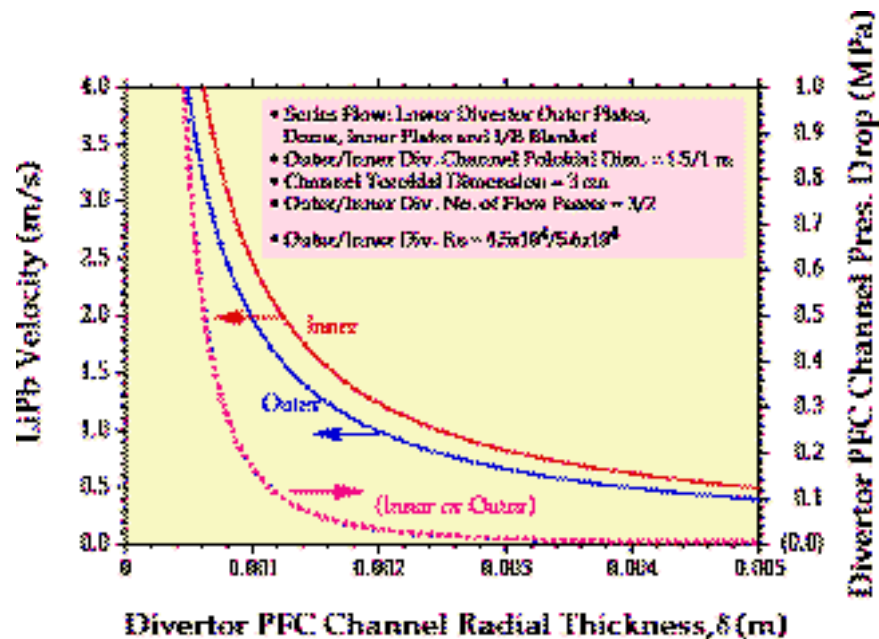
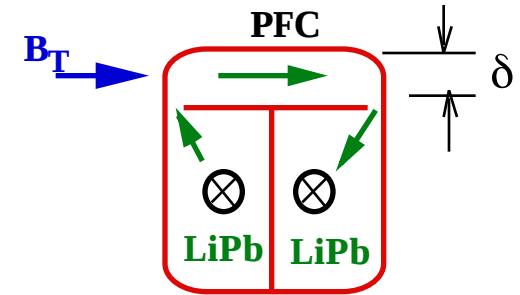


LiPb Poloidal Flow in ARIES-AT Divertor Header

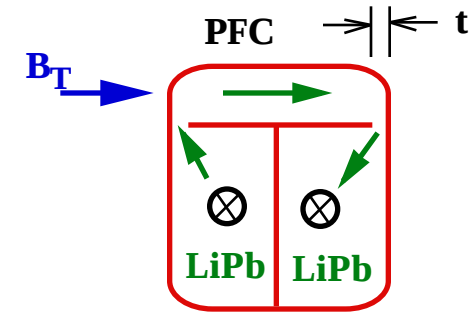
Example schematic illustration of 3-toroidal-pass scheme for divertor PFC cooling



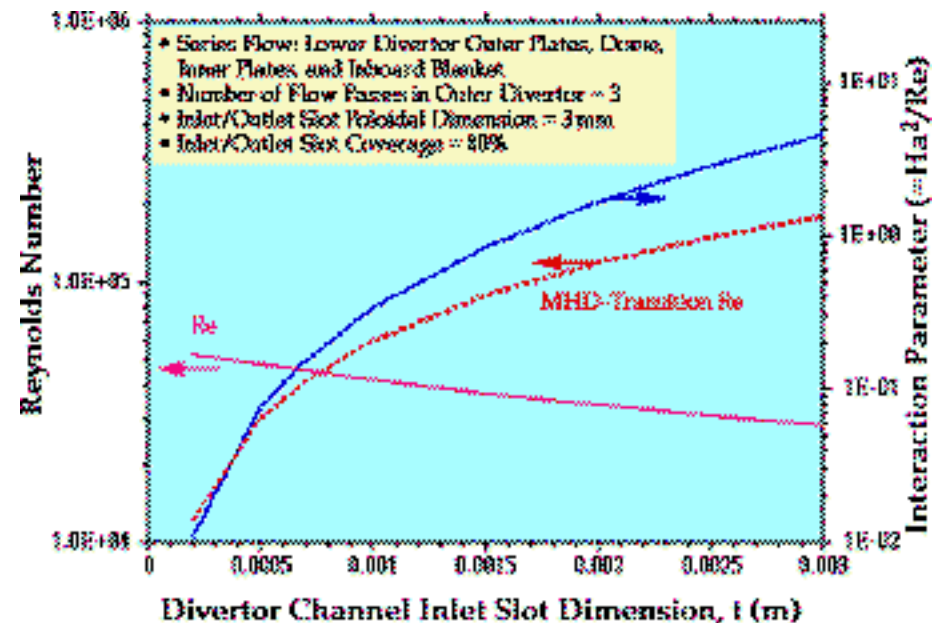
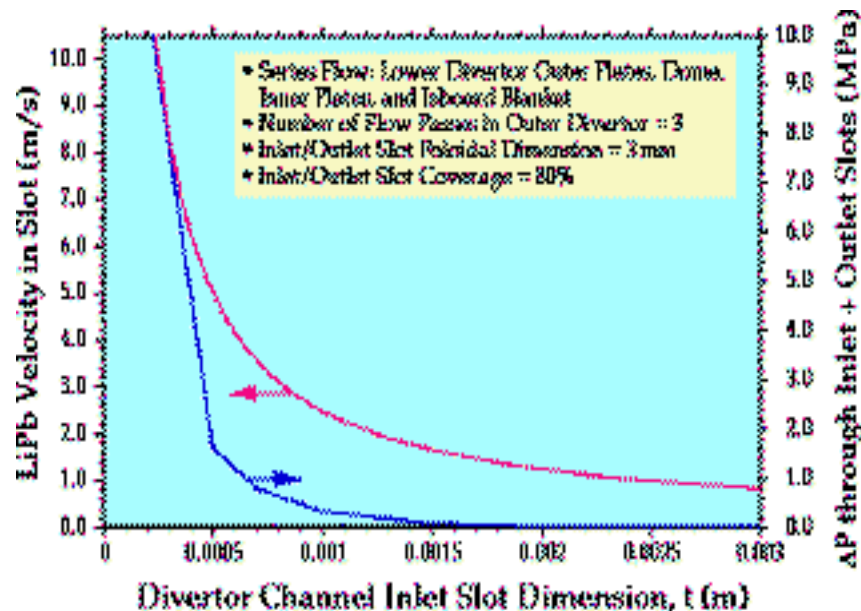
Flow and Thermal Parameters for LiPb-Cooled Divertor PFC as a Function of PFC Channel Thickness



Velocity, ΔP , Re, and Interaction Parameter as a Function of Divertor Channel Inlet/Outlet Slot Dimension



- High inertia regime (low interaction parameter) to overcome MHD-induced slanted velocity profile



Typical Blanket and Divertor Parameters for Example Design Point

Blanket Outboard Region 1

- No. of Segments 32
- No. of Modules per Segment 6
- Module Poloidal Dimension 6 m
- Avg. Module Toroidal Dimen. 0.18 m
- FW SiC/SiC Thickness 4 mm
- FW CVD SiC Thickness 1 mm
- FW Annular Channel Thickness 5 mm
- Avg. LiPb Velocity in FW 5.8 m/s
- FW Channel Re 6.2×10^5
- FW Channel Transverse Ha 3540
- MHD Turbulent Transition Re 1.8×10^6
- FW MHD Pressure Drop 0.49 MPa
- Maximum SiC/SiC Temp. 997°C
- Maximum CVD SiC Temp. (°C) 1030 °C

Lower Outer/Inner Divertor

- Poloidal Dimension 1.5/1.0 m
- Divertor Channel Toroidal Dimension 3.8 cm
- Divertor Channel Radial Dimension 3.75 cm
- Number of Divertor Channels 744/595
- SiC Insert Thickness 0.5 mm
- W Thickness 3 mm
- PFC Channel Thickness 2 mm
- Number of Toroidal Passes 3/2
- Velocity in PFC Channel 1/ 1.2 m/s
- Maximum SiC Temperature 1000/1040°C
- Maximum W Temperature 1150/1180°C
- W (1-D) Thermal Stress 162 MPa
- Toroidal Dimension of Inlet and Outlet Slot 1 mm
- Vel. in Inlet & Outlet Slot to PFC Channel 2.5/3.1 m/s
- Interaction Parameter in Inlet/Outlet Slot 0.34/0.42
- Pressure Drop 0.47/0.5 MPa

Future Work Includes:

- **Converge on coolant routing scheme**
- **Converge of maintenance scheme**
- **Tabulated list of parameters (LiPb volume and mass in different components, etc..)**
- **Blanket fabrication flow diagram**
- **Power cycle: Better characterization of heat exchanger**
- **Divertor**
 - **Recommend using LiPb as reference coolant and He as back-up option**
 - Inlet and toroidal flow in PFC channel under low interaction parameter must be verified by detailed MHD analysis and testing
 - **Detailed thermal and stress analysis**