

Conceptual design of liquid metal cooled power core components for a fusion power reactor

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and

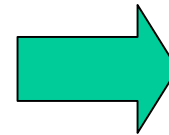
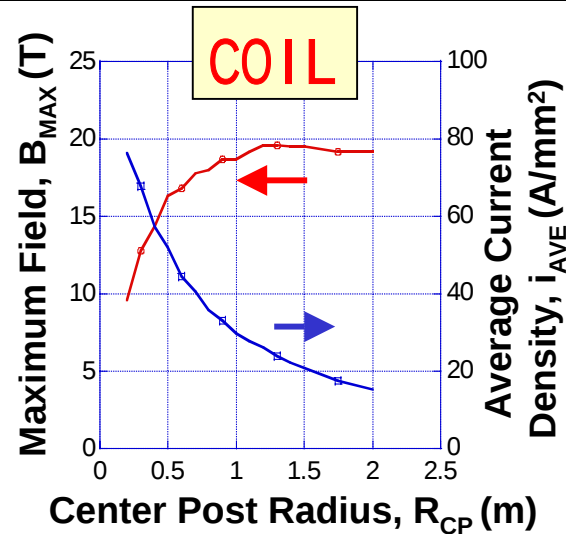
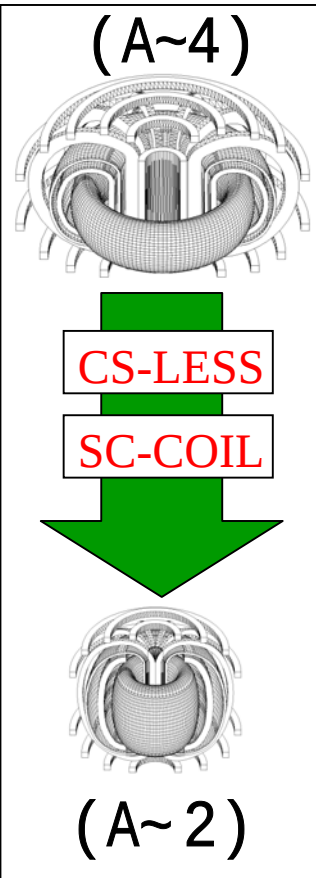
Satoshi NISHIO (西尾敏)

Japan Atomic Energy Research Institute

**Japan-US workshop on
Fusion Power Plants and Related Advanced Technologies with Participation of EU**

Jan.11-13,2005 at Tokyo,JAPAN

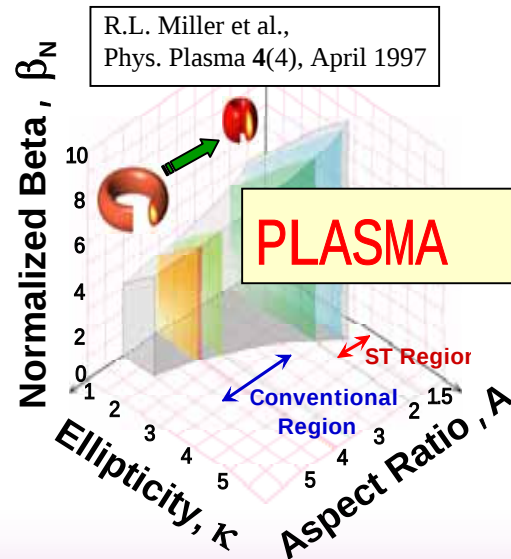
Background of Research



VECTOR
(S.Nishio 2002 IAEA)

Advantages:

- Light weight
- High β and B
- Small waste
- Economical aspect



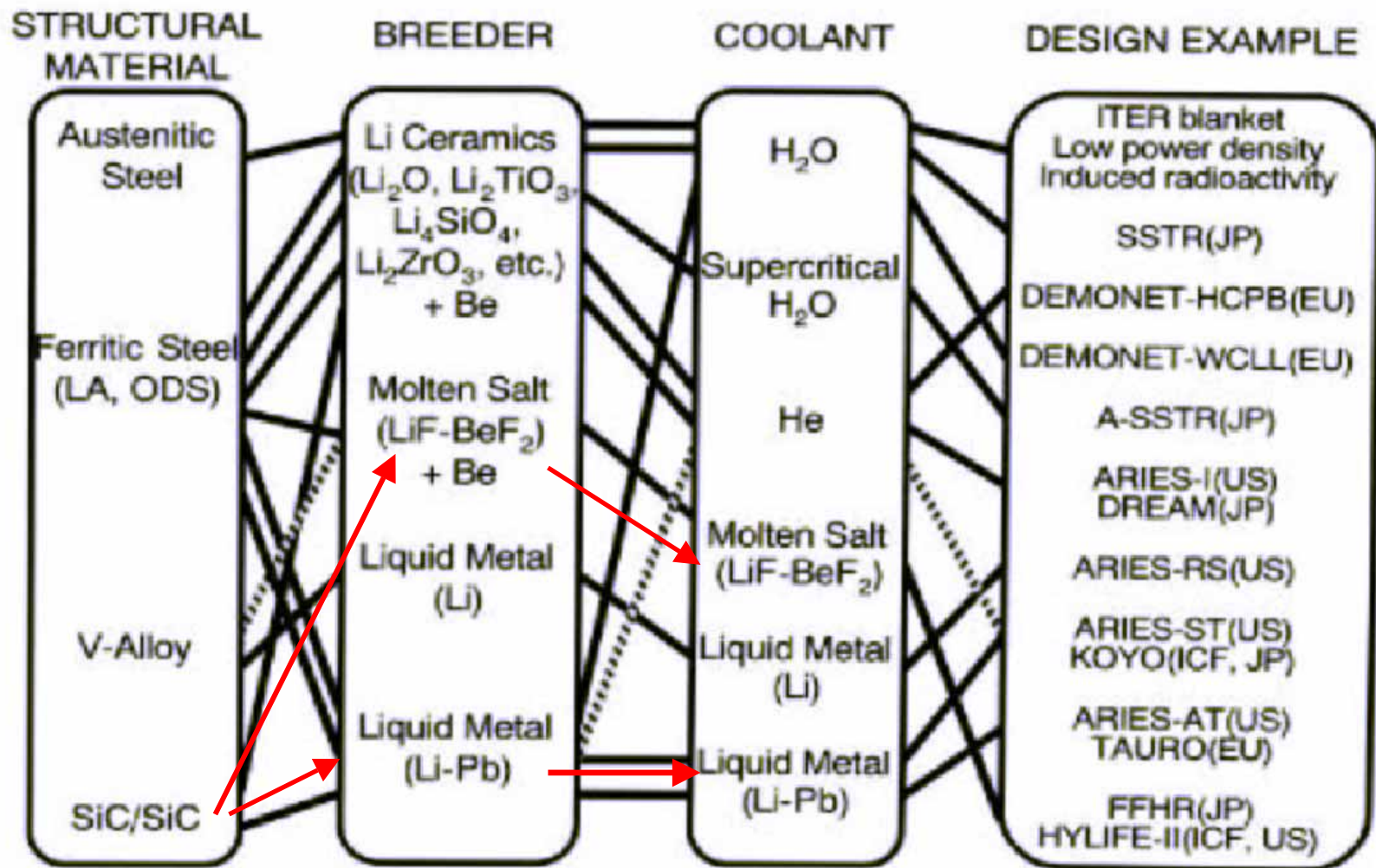
Power core components Engineering:

0. Comparison and summary of former work on Blanket

1. Design of Liquid metal self-cooled Blanket

2. Design of Plasma Facing Components

3. Power Cycle



How to choose

Structure material: **SiC/SiC**, **V-alloy** or **Fe-Steel**?

Breeder ,Coolant material: **Li**, **LiPb** or **FLiBe**?

System: **Dual coolant** or **Self-coolant**?

Compare of the three kinds structure materials

	Weight Function	Fe-Steels	V-alloy	SiC
High temperature capability	5	1	1	3
Plasma disruption effect on the structure	4	1	1	3
Low activation	4	1	2	3
High heat flux capability	3	2	3	2
Mature development of fabrication	3	3	3	1
Low Economic Cost	2	3	2	1
High radiation damage resistance	2	2	3	2
Brittle fracture and Swelling behavior	1	2	2	3
Total Score (Ideal score is 72)	Normal Distribution	40	41	57

Comparison of the three kinds Coolant materials

	Weight Function	Li	FLiBe	LiPb
Efficiency of power plant	5	2	1	3
Safety : reliability against leak	4	1	2	3
Tritium breeding and control	3	1	2	3
Material compatibility	3	1	2	3
MHD issue	2	2	3	2
Reactivity to oxygen	1	1	1	3
Total Score (Ideal score is 54)	Normal Distribution	25	32	52

LiPb :

Simple blanket structure

Easy tritium recovery

No need to exchange

MHD probably will have significant impact on pressure drop.

FliBe:

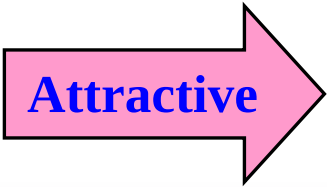
The thermal conductivity is very low, high turbulence flow is required for heat transfer

The viscosity is much high, Larger channel size are required for high turbulence flow

Tritium breeding capability is relatively limited

Compare of the Dual and self cooling blanket system

Evaluation Item	Dual	Self-cooling
Simple blanket structure	Bad	Good
Maintenance of operation	Bad	Good
Ease of fabrication	Bad	Good
Potential net efficiency	Bad	Good
Probability of LOCA	Bad	Good
Insulator requirement for MHD	Good	Bad
General Score	Terrible	Excellent

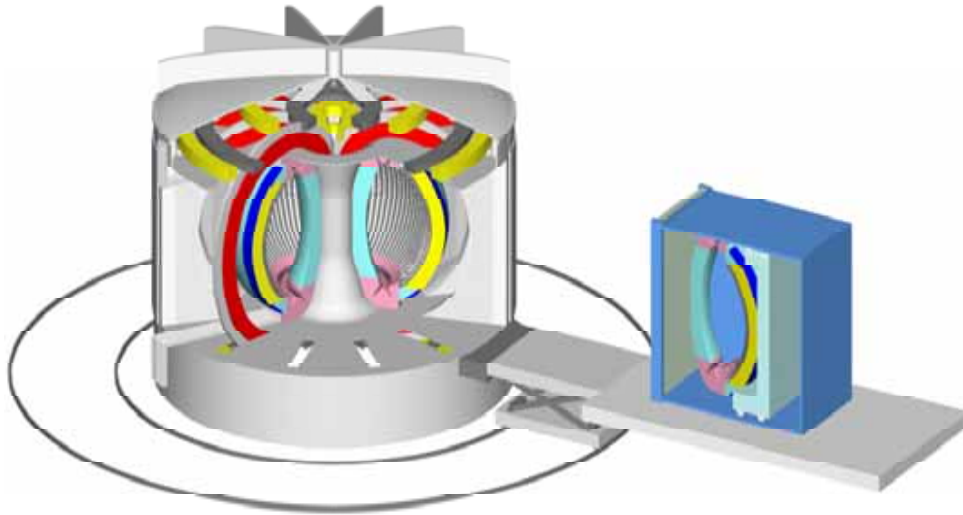


Attractive

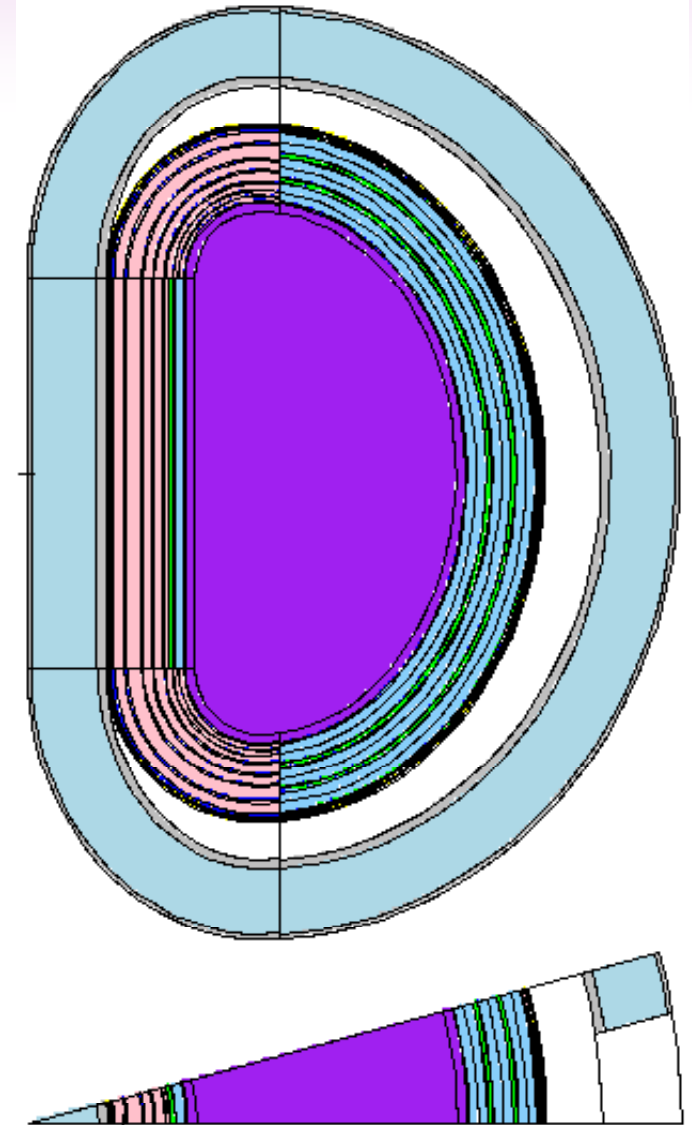
- Structure material: **SiC/SiC**
- Breeder ,Coolant material: **LiPb**
- System: **Self-cooled**

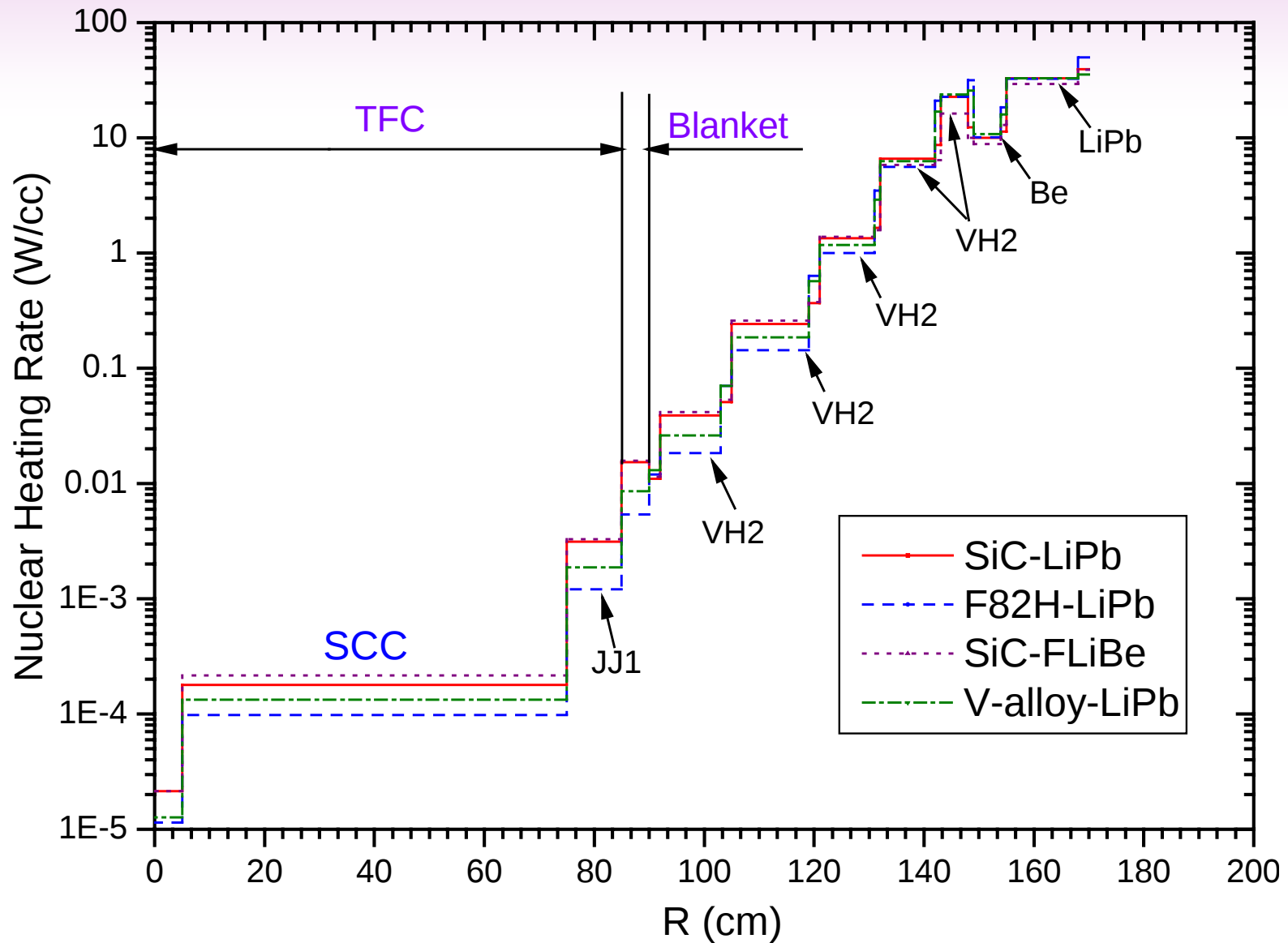
Nuclear Analysis Model

Calculated by T.Nishitani



Plasma Major Radius : $R_p = 3.2 \text{ m}$
Plasma Minor Radius : $a_p = 1.4 \text{ m}$
Number of TF coils: 12
Vacuum Vessel: SS316LN
Super conducting: Bi-HTS
Fusion Power : $P_F = 2.5 \text{ GW}$



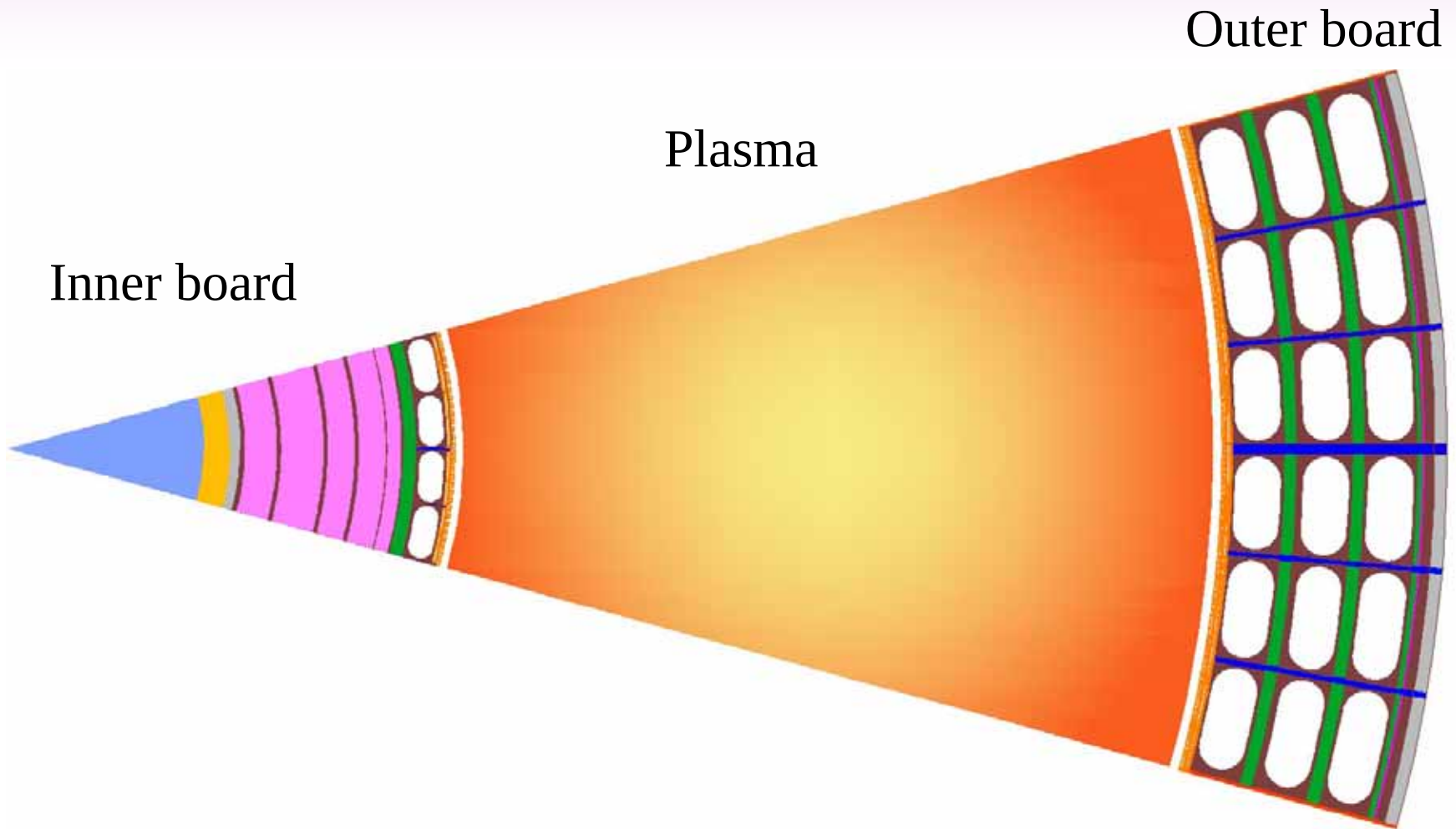


Distribution of Nuclear Heating Rate

Nuclear heating Analysis results (inner board)

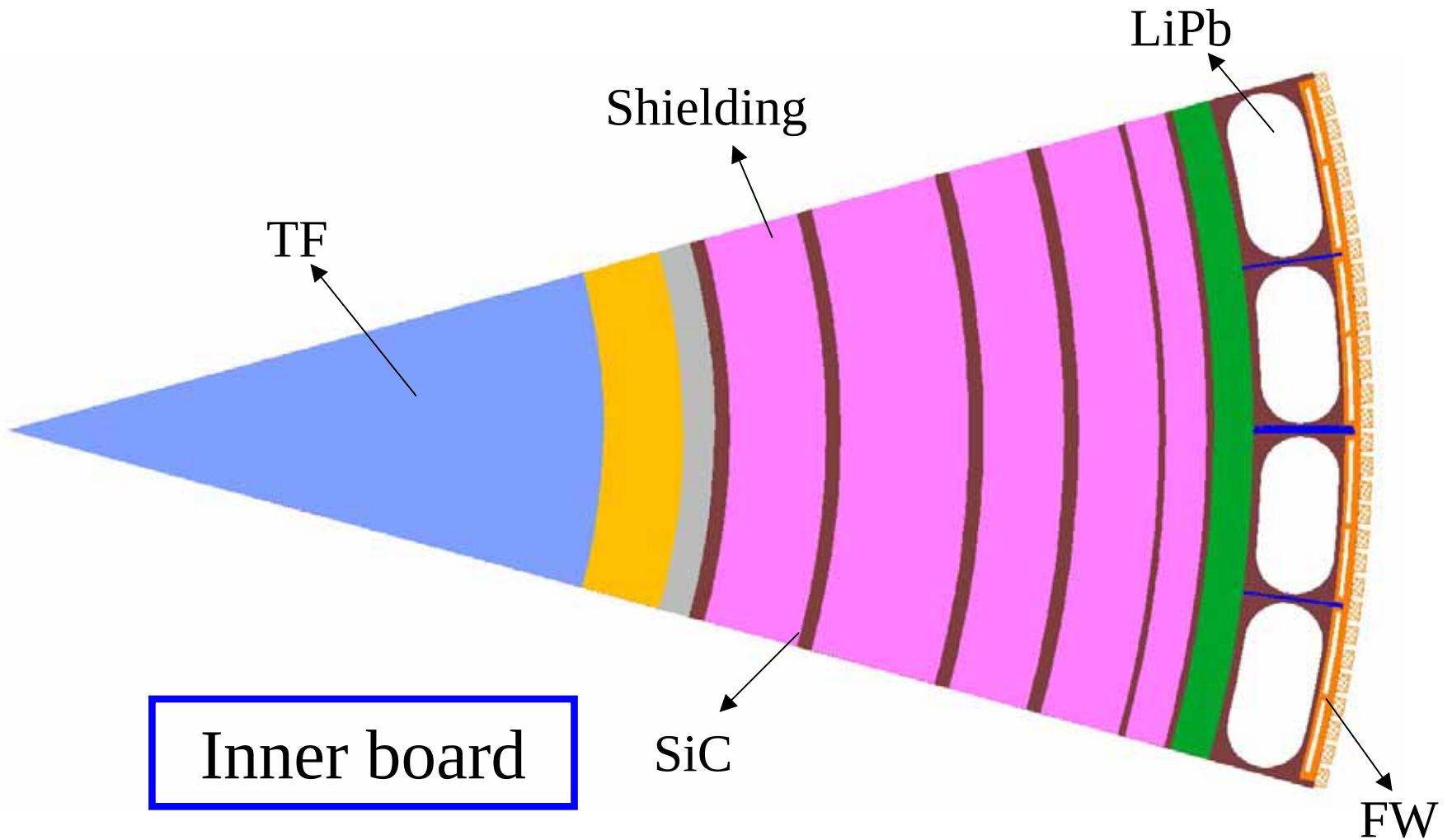
	case1	case2	case3	case4
Structure material	V-Alloy	SiC	SiC	F82H
Breeding、Multiply and Coolant	LiPb	LiPb	FLiBe	LiPb
Maximum Nuclear Heating Rate (W/cc)	35.4	39.4	38.9	49.9

1. Maximum nuclear heating on the First wall and LiPb: $> 35 \text{ W/cc}$.
2. Maximum nuclear heating on the HTS TF coils: $1\text{e-}3\text{W/cc}$.

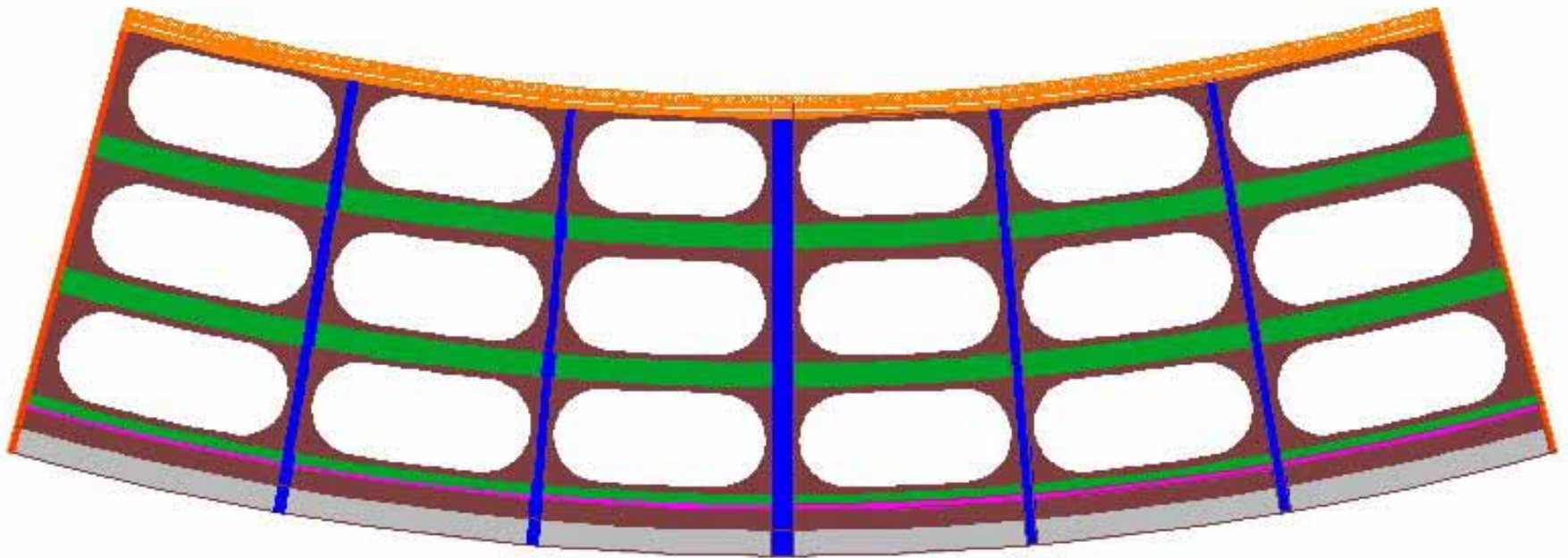


Cross section of the Low aspect ratio tokamak

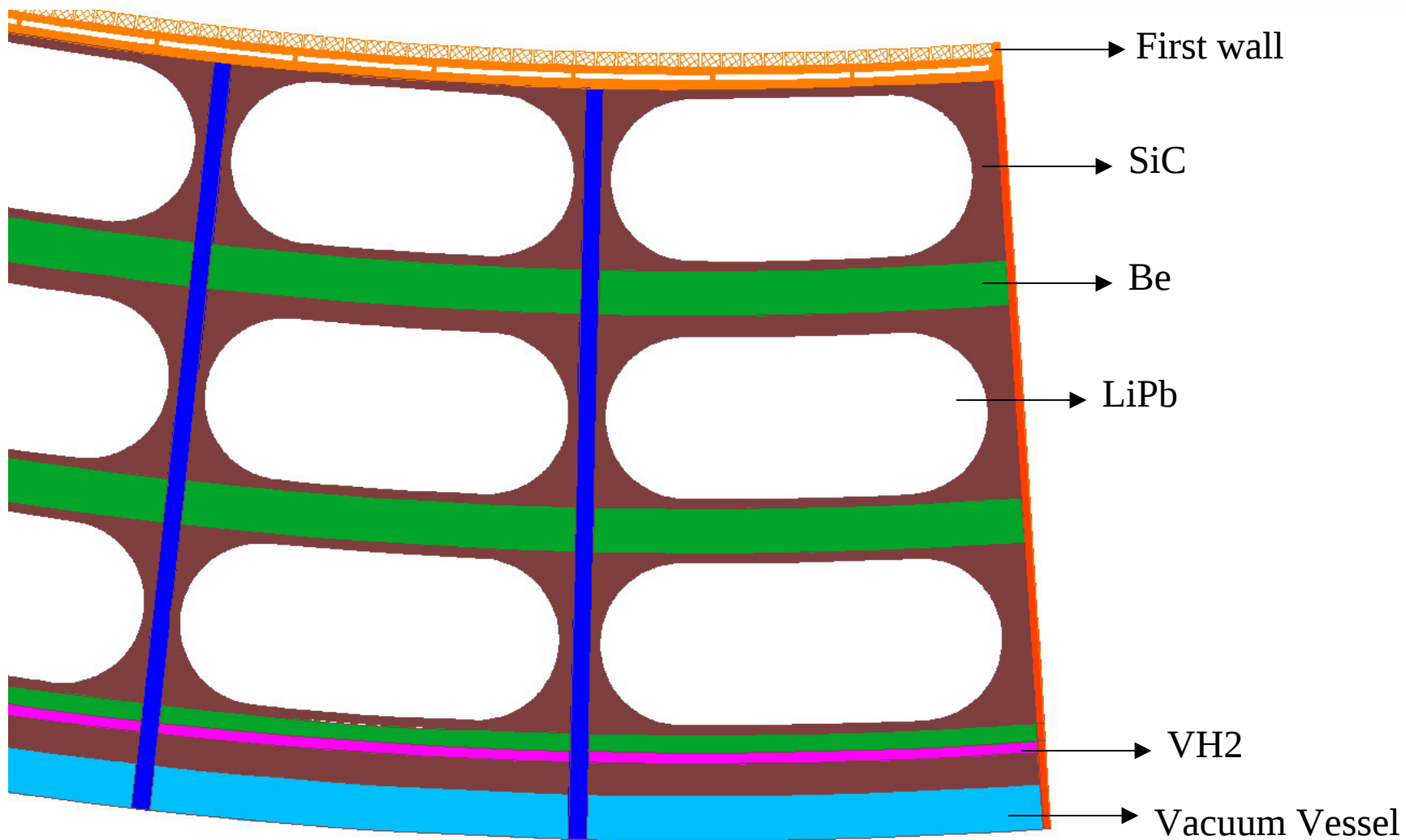
Concept Design Structure of IB for Low Aspect Ratio Tokamak



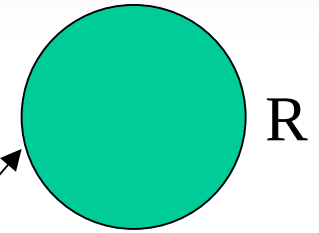
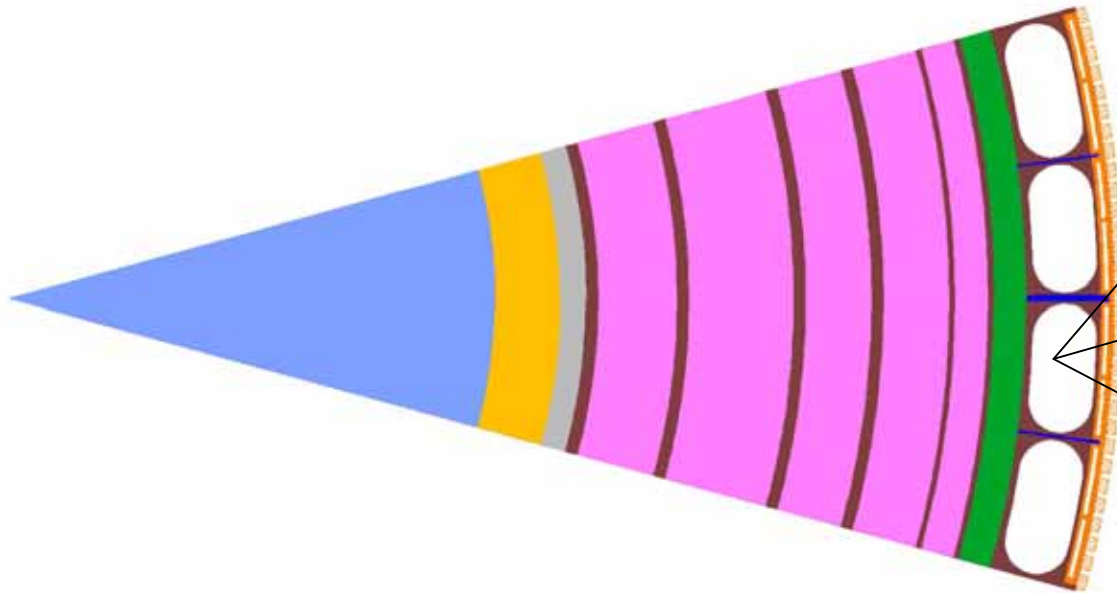
Concept Design Structure of OB for Low Aspect Ratio Tokamak



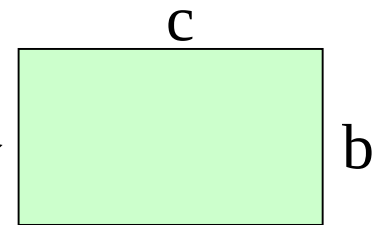
Outer board



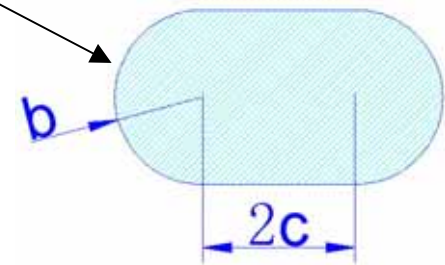
Size and shape of Cooling Channel



Circle Channel



Rectangle Channel

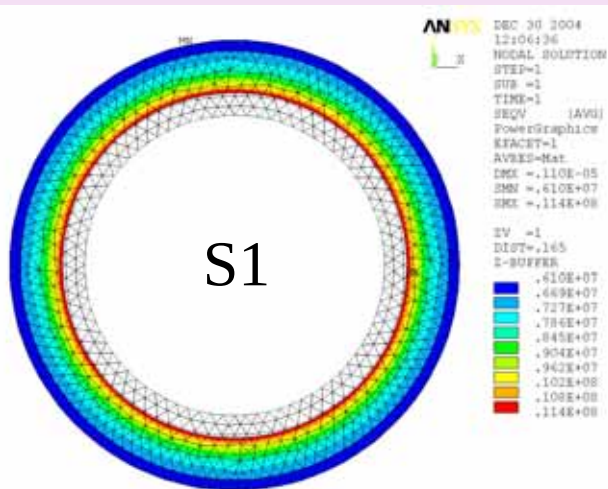


Oval Channel

Which shape structure is better for cooling channel?

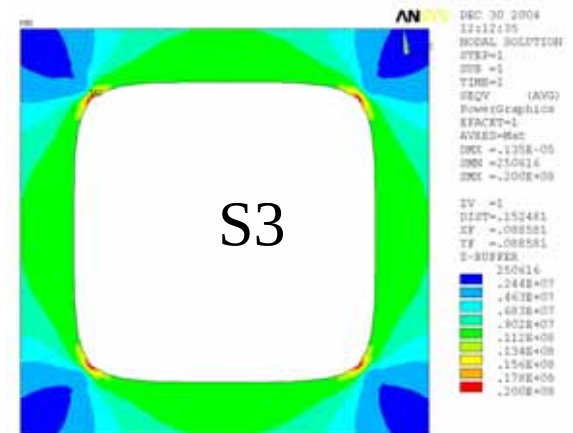
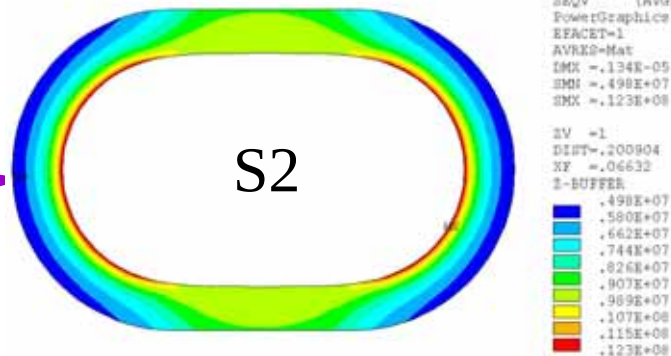
Optimization

$c/b = ?$



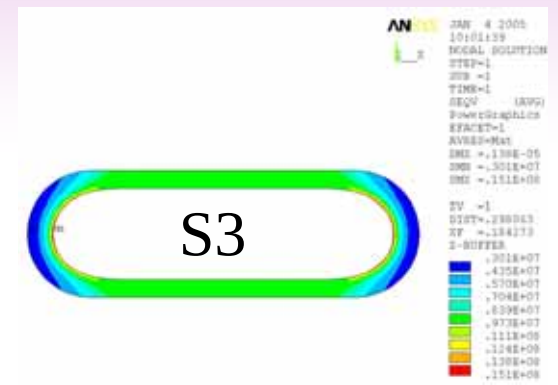
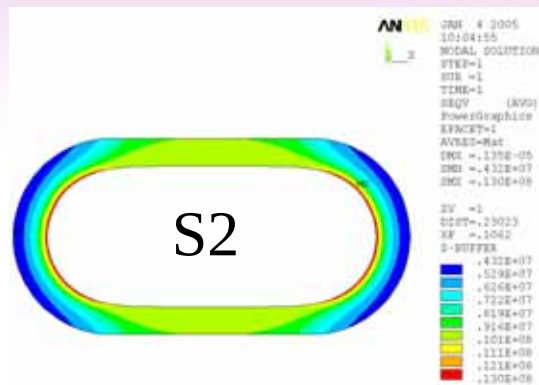
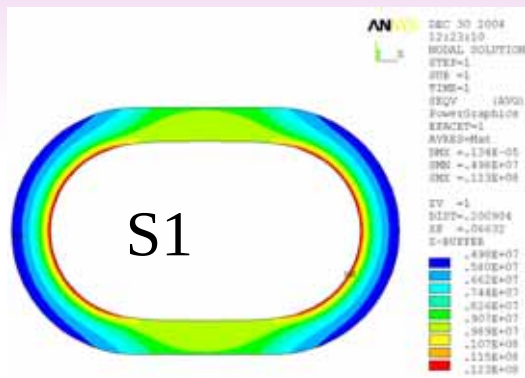
•Cooling channel area: $S1=S2=S3$

Perimeter: $L1 < L3 < L2$



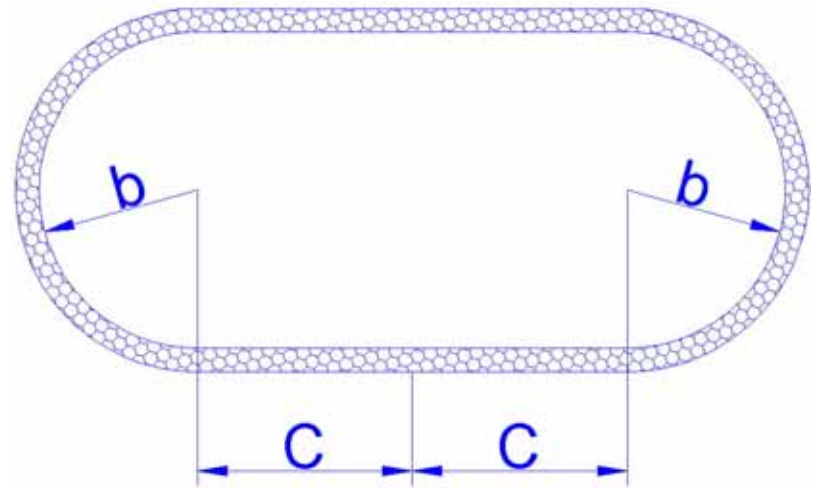
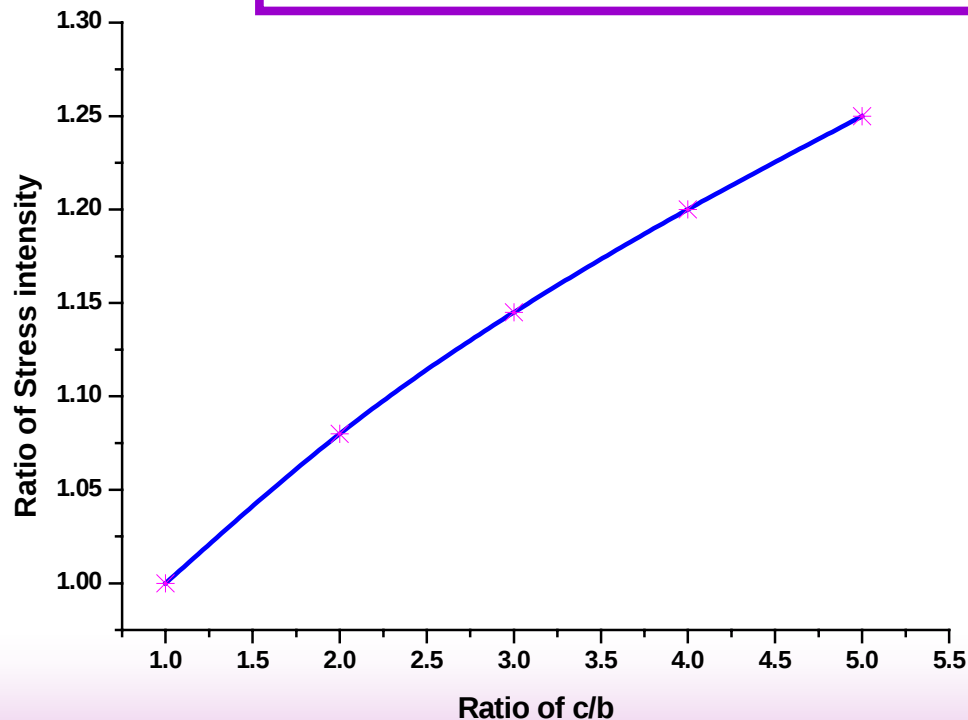
Maximum Stress Intensity

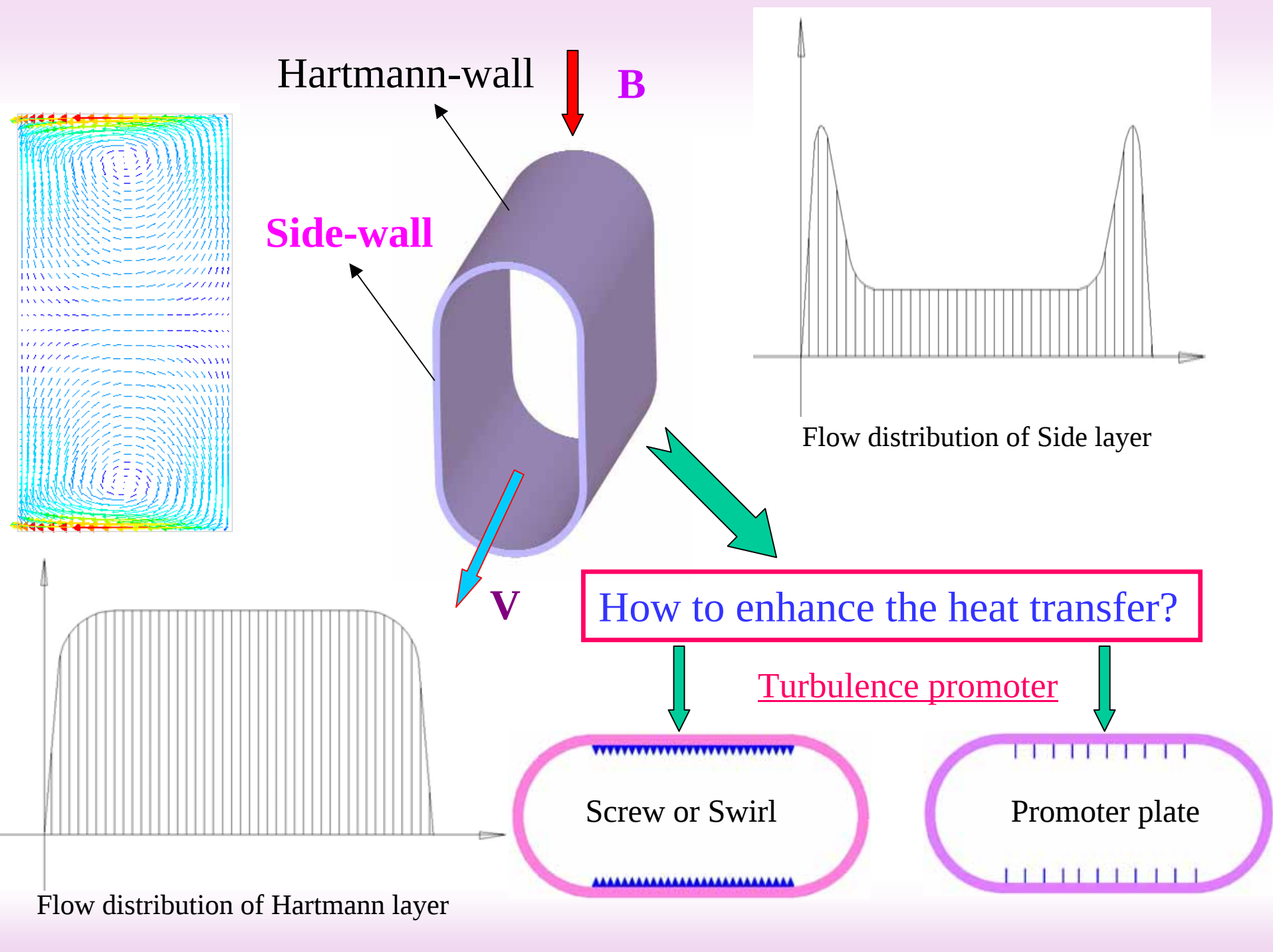
Circle:Oval:Rectangle 1 : 1.2 : 2



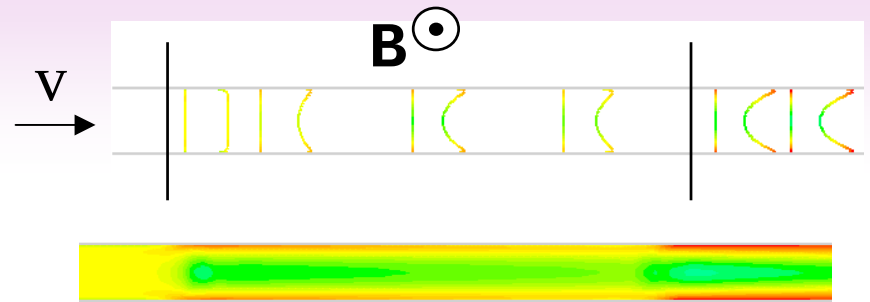
Area: $S1=S2=S3$; Inner Pressure: $P1=P2=P3$

Stress intensity 1 : 1.2 : 1.5





MHD pressure drop



1. Effect of material properties:

Conducting and Non-Conducting wall be compared

2. Effect of Channel shape:

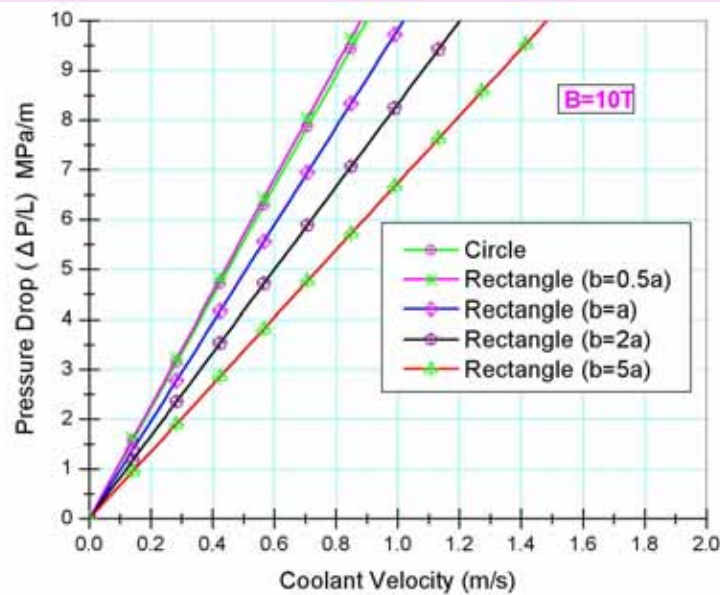
Irregular cross section, non-uniform wall thickness

3. Effect of Complex magnetic field (future work)

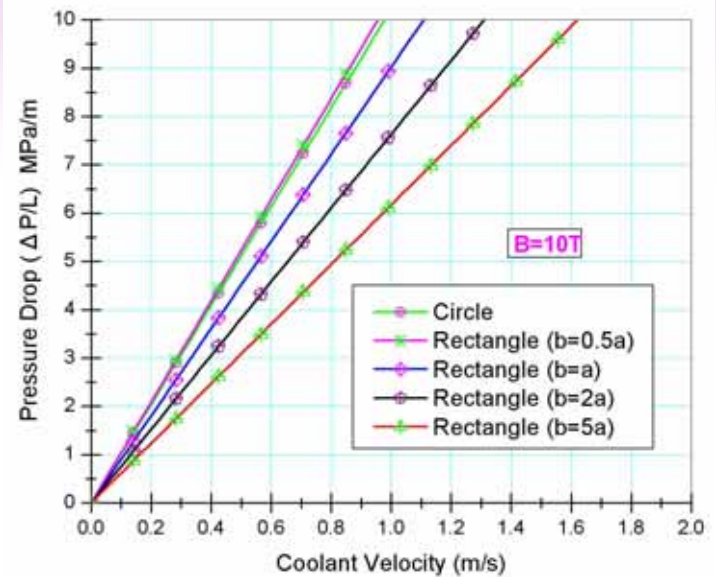
Angled field, field gradient, field ripple

4. Source of Turbulence and its effects (future work)

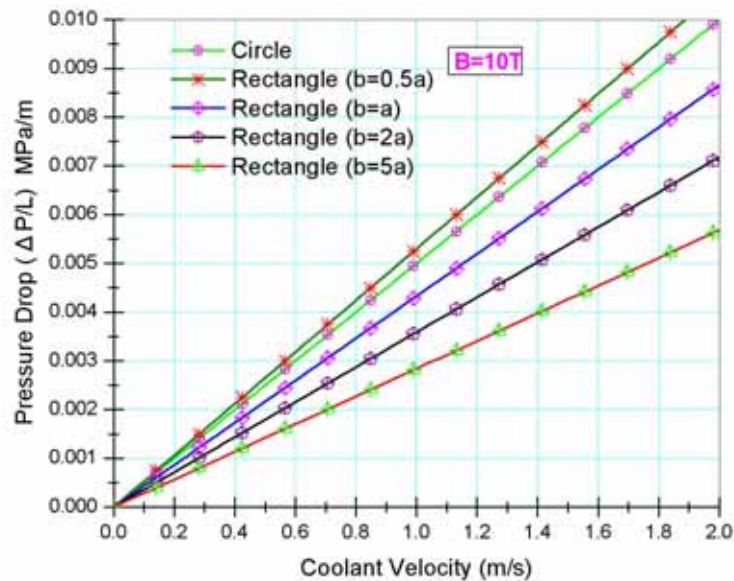
5. Effect of eddy current (future work)



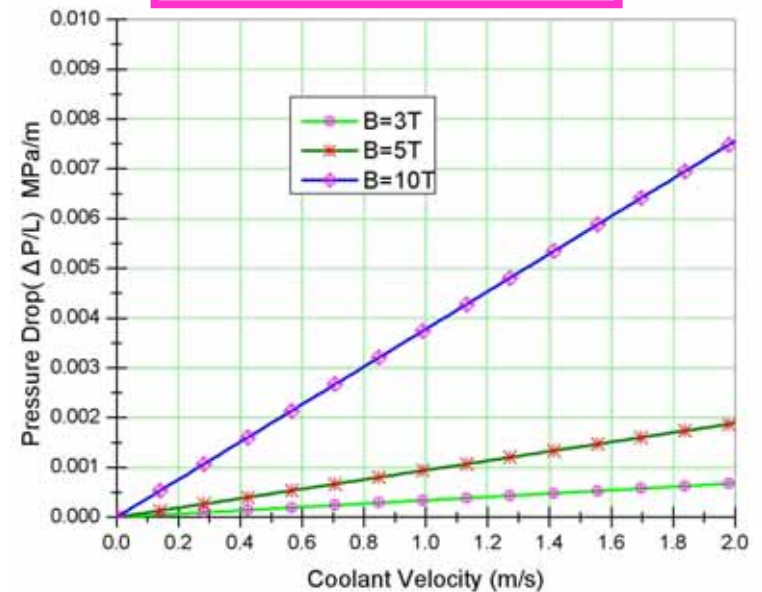
Ferritic steel-LiPb



V-alloy-LiPb

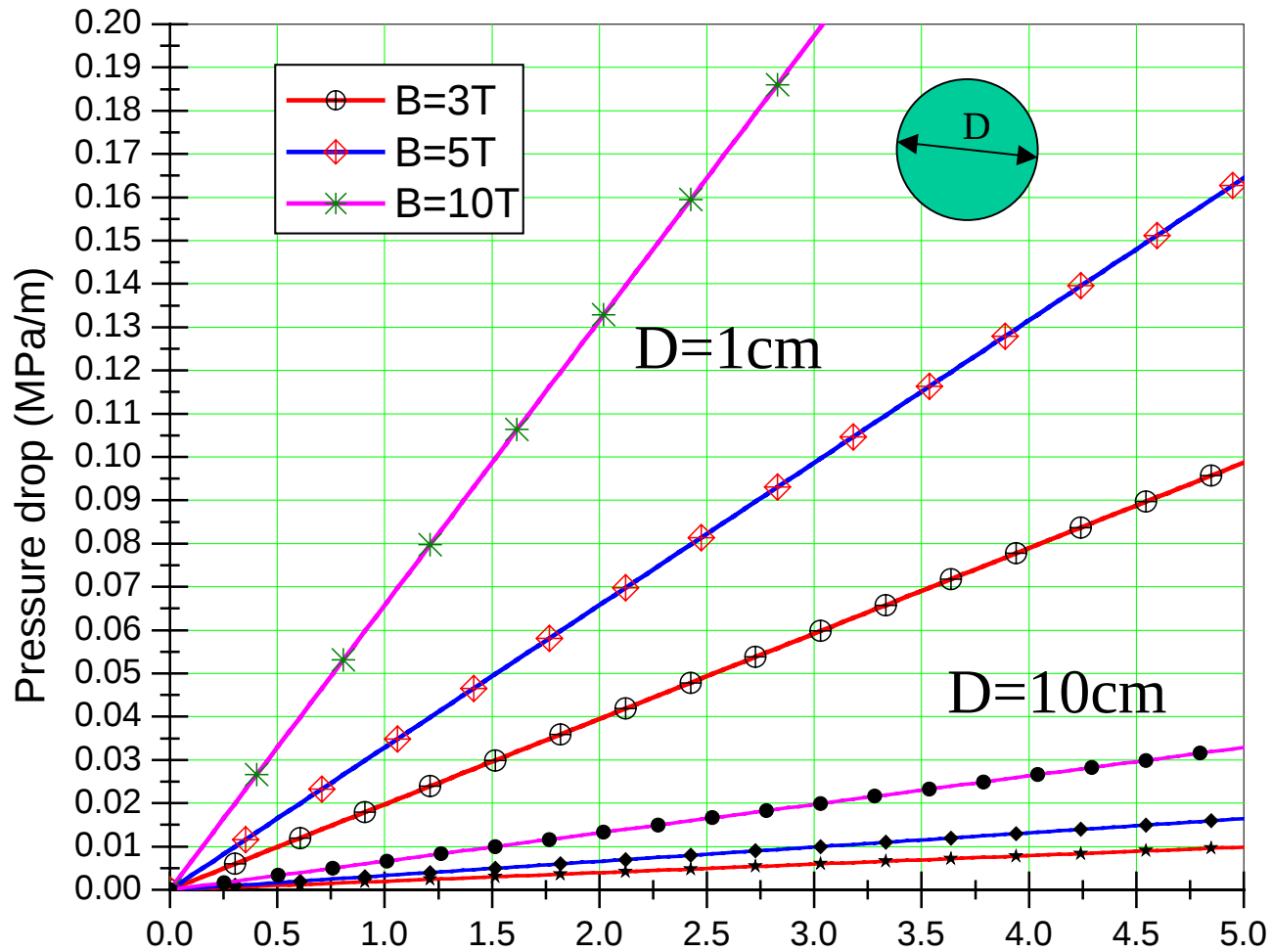


SiC-LiPb

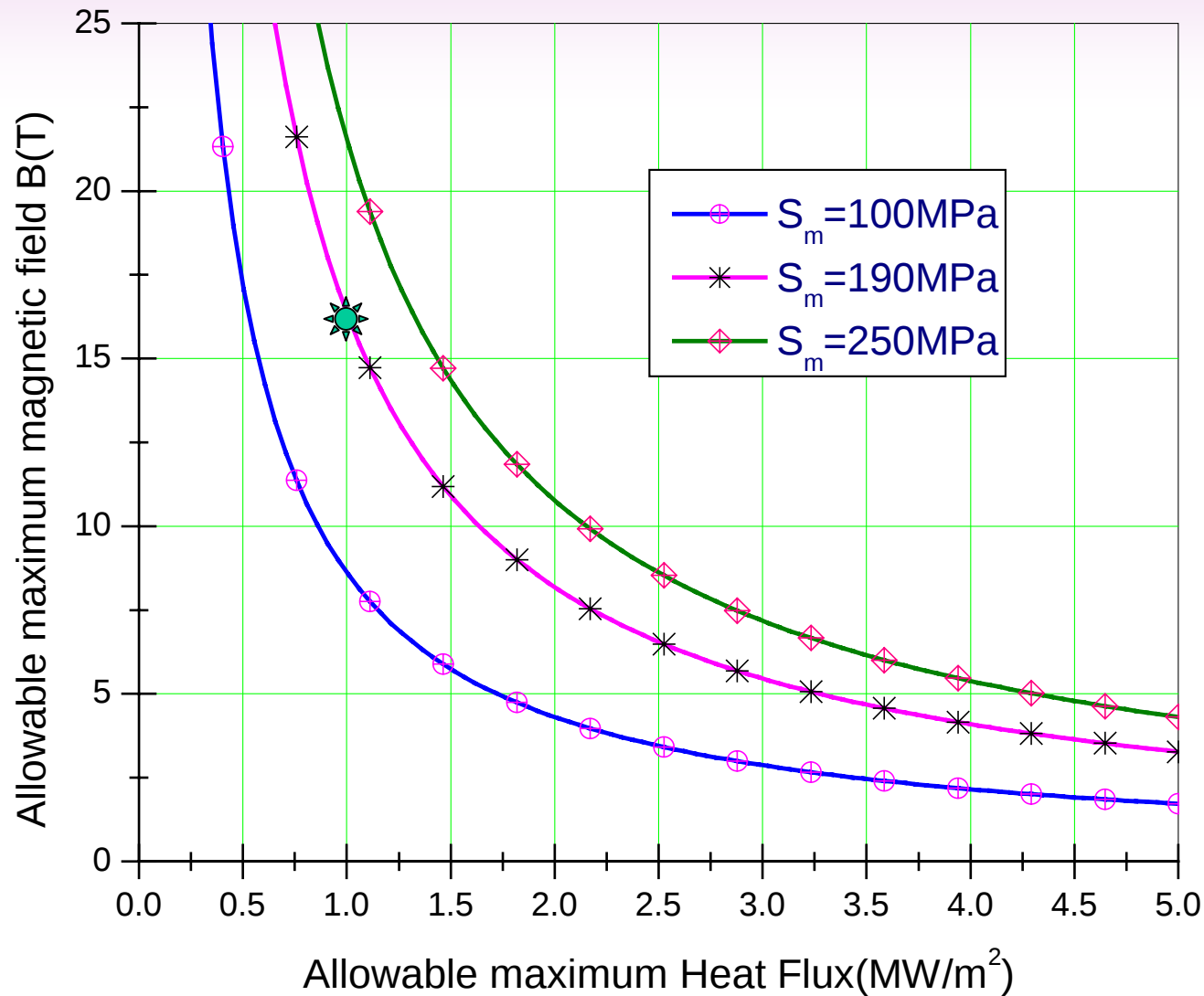


SiC-FLiBe

Non-conducting or insulated wall



Pressure drop depended on the size of cooling channel and velocity



Allowable maximum magnetic field and heat flux depended on the allowable stress of structure material

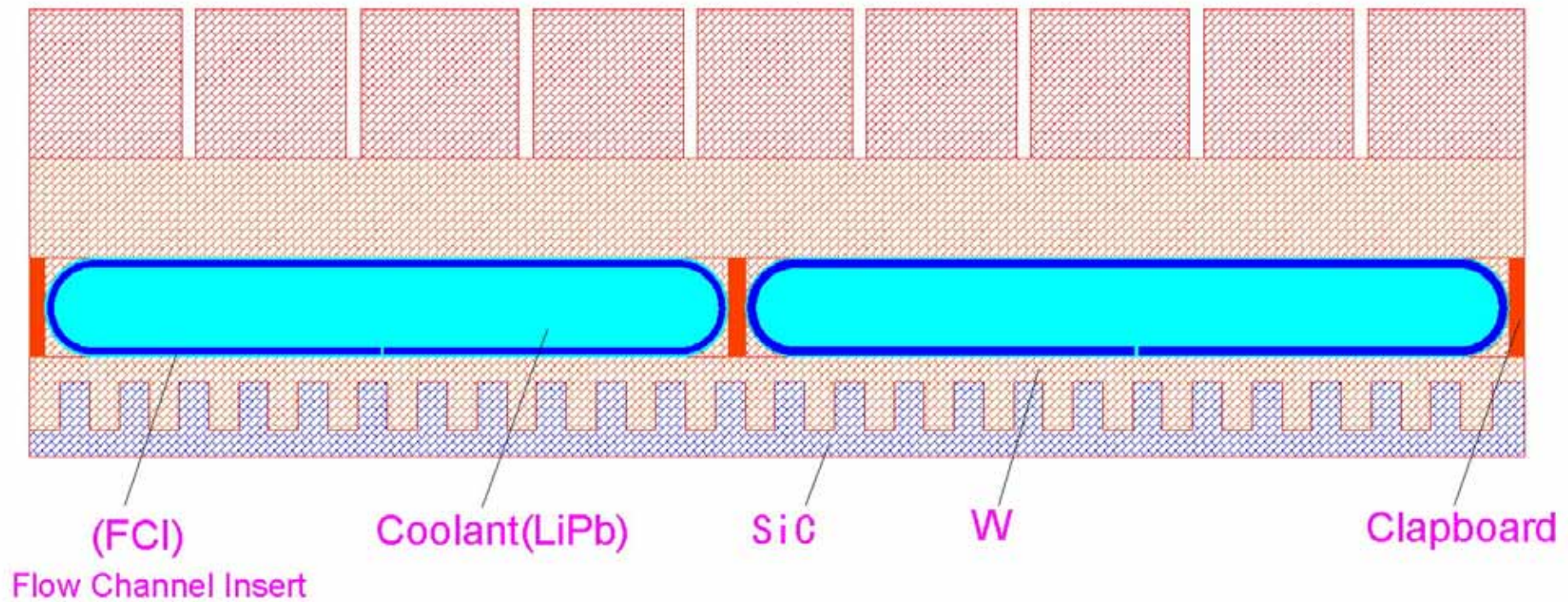
Plasma Facing Components (FW and divertor):

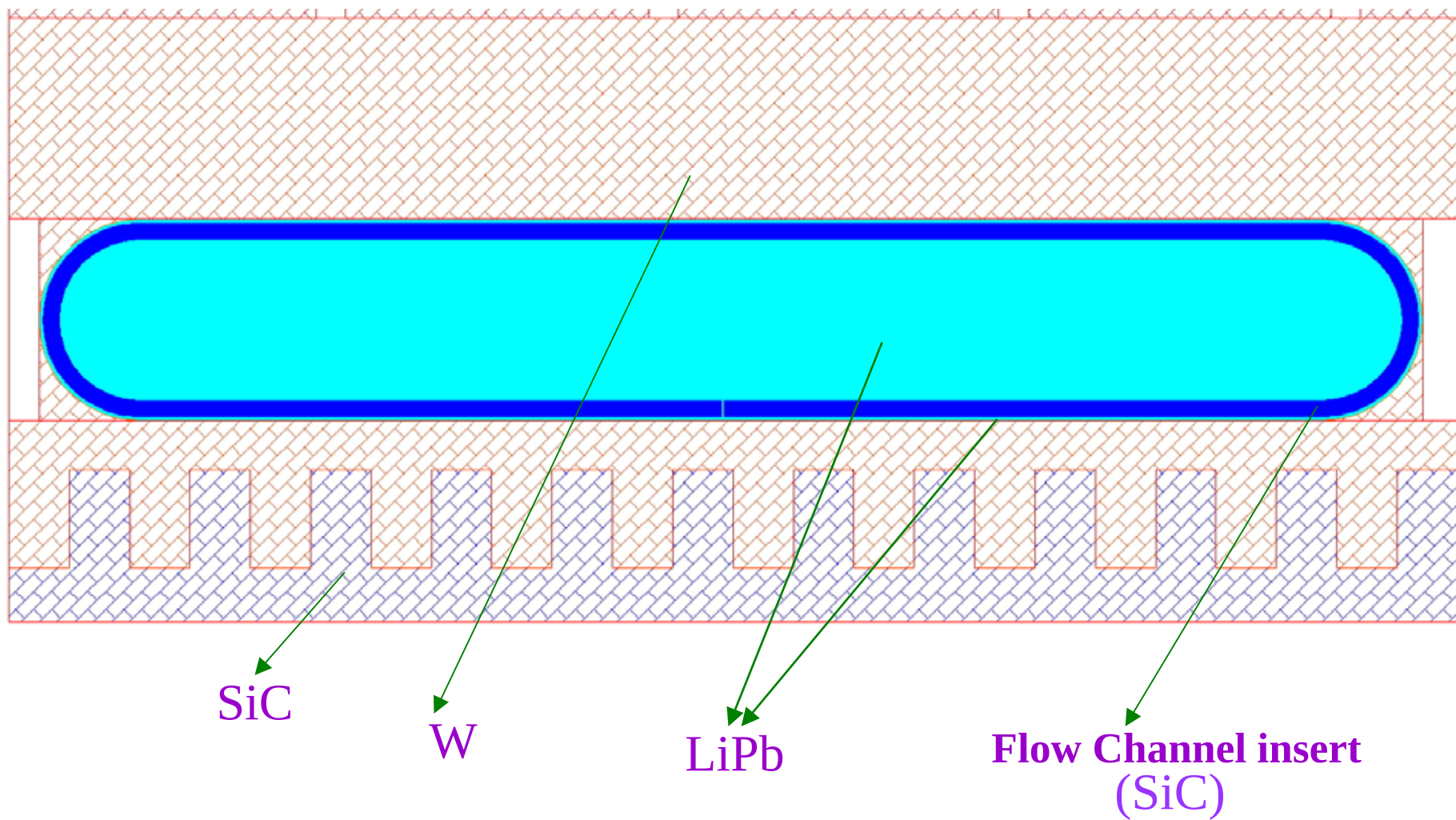
1. Material choice based on the thermal hydraulic, thermal stress, Surface erosion and other conditions
2. Safety of structure due to large EM force, especially the First wall structure due to HALO current.
3. High heat flux removal

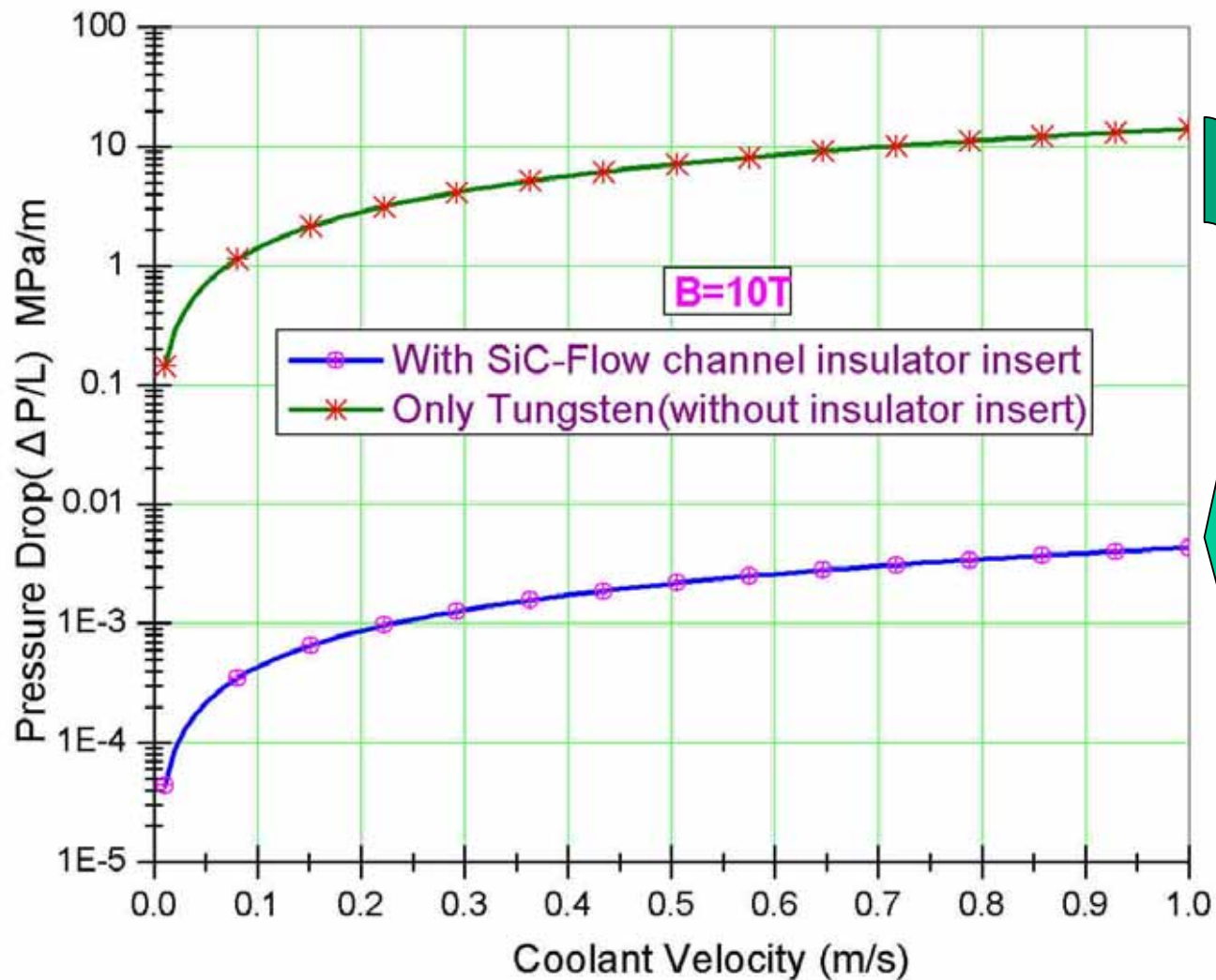
Normal design: Laminar or turbulent flow in smooth-walled channels, flow velocity, pressure drop and channel erosion and flow stability

Development of various options to increase heat transfer including swirl flow , turbulent promoters and roughened surfaces

PLASMA

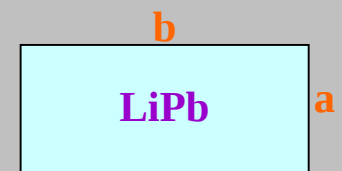






~ 3000 Times

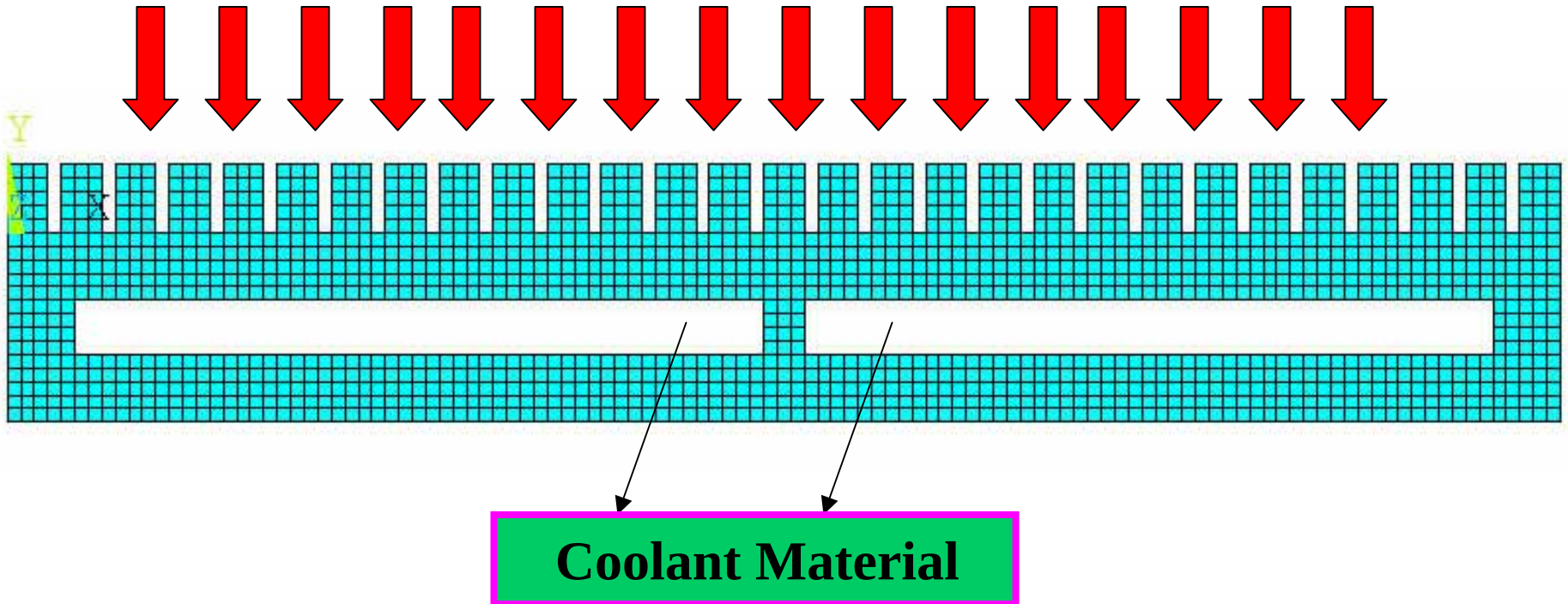
Model:



Case: $b=2a$

MHD for First Wall depended on the Conducting and Non-Conducting wall

Heat flux: 1MW/m^2



Finite Element Analysis Model

Maximum:1188K

TIME=1
TEMP (AVG)
RSYS=0
PowerGraphics
EFACET=1
AVRES=Mat
SMN =816.118
SMX =1188

ZV =1
*DIST=.116369
*XF =.114977
*YF =.847E-03
Z-BUFFER
816.118
857.388
898.659
939.93
981.201
1022
1064
1105
1146
1188

Thermal stress

Temperature

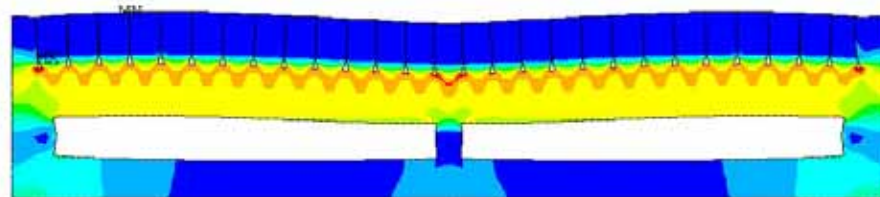


JAN 1 2005
20:45:37
NODAL SOLUTION
STEP=1
SUB =1
TIME=1
SEQV (AVG)
PowerGraphics
EFACET=1
AVRES=Mat
DMX =.443E-04
SMN =291638
SMX =.440E+09

Maximum:440MPa
< Allowable thermal stress of SiC

Note: $V=0.05\text{m/s}$ (LiPb)

Material of FW: Tungsten



ZV =1
*DIST=.116369
*XF =.114977
*YF =.847E-03
Z-BUFFER
291638
.491E+08
.979E+08
.147E+09
.196E+09
.244E+09
.293E+09
.342E+09
.391E+09
.440E+09

Maximum:2064K

ANSYS JAN 1 2005
19:57:30
NODAL SOLUTION
STEP=1
SUB =1
TIME=1
TEMP (AVG)
RSYS=0
PowerGraphics
EFACET=1
AVRES=Mat
SMN =800.507
SMX =2064

Thermal stress

Temperature

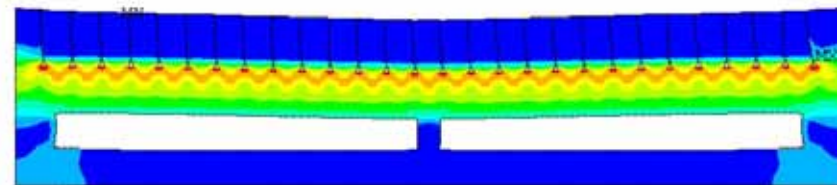
ZV =1
*DIST=.116369
*XF =.114977
*YF =.847E-03
Z-BUFFER
800.507
940.858
1081
1222
1362
1502
1643
1783
1923
2064

Maximum:1220MPa
> Allowable thermal stress of SiC

Note: $V=0.05\text{m/s}$ (LiPb)

Material of FW: SiC/SiC

ANSYS JAN 1 2005
19:59:17
NODAL SOLUTION
STEP=1
SUB =1
TIME=1
SEQV (AVG)
PowerGraphics
EFACET=1
AVRES=Mat
DMX =.949E-04
SMN =967236
SMX =.122E+10



ZV =1
*DIST=.116369
*XF =.114977
*YF =.847E-03
Z-BUFFER
967236
.137E+09
.272E+09
.408E+09
.543E+09
.679E+09
.815E+09
.950E+09
.109E+10
.122E+10

Maximum:8272K

```
ANSYS  JAN  1 2005
20:25:52
NODAL SOLUTION
STEP=1
SUB  =1
TIME=1
TEMP      (AVG)
RSYS=0
PowerGraphics
EFACET=1
AVRES=Mat
SMN  =2893
SMX  =8272
```

```
ZV  =1
*DIST=-.116369
*XF  =.114977
*YF  =.847E-03
Z-BUFFER
2893
3490
4088
4686
5283
5881
6479
7077
7674
8272
```

Thermal stress

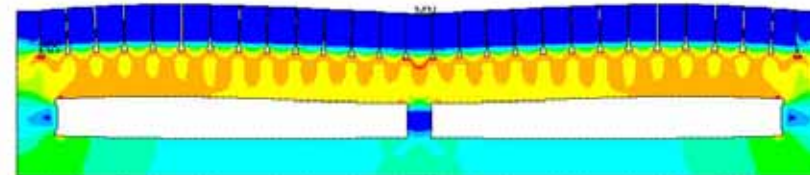
Temperature

```
ANSYS  JAN  1 2005
20:27:21
NODAL SOLUTION
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SUB  =1
TIME=1
SEQV      (AVG)
PowerGraphics
EFACET=1
AVRES=Mat
DMX  =.001185
SMN  =.117E+08
SMX  =.131E+11
```

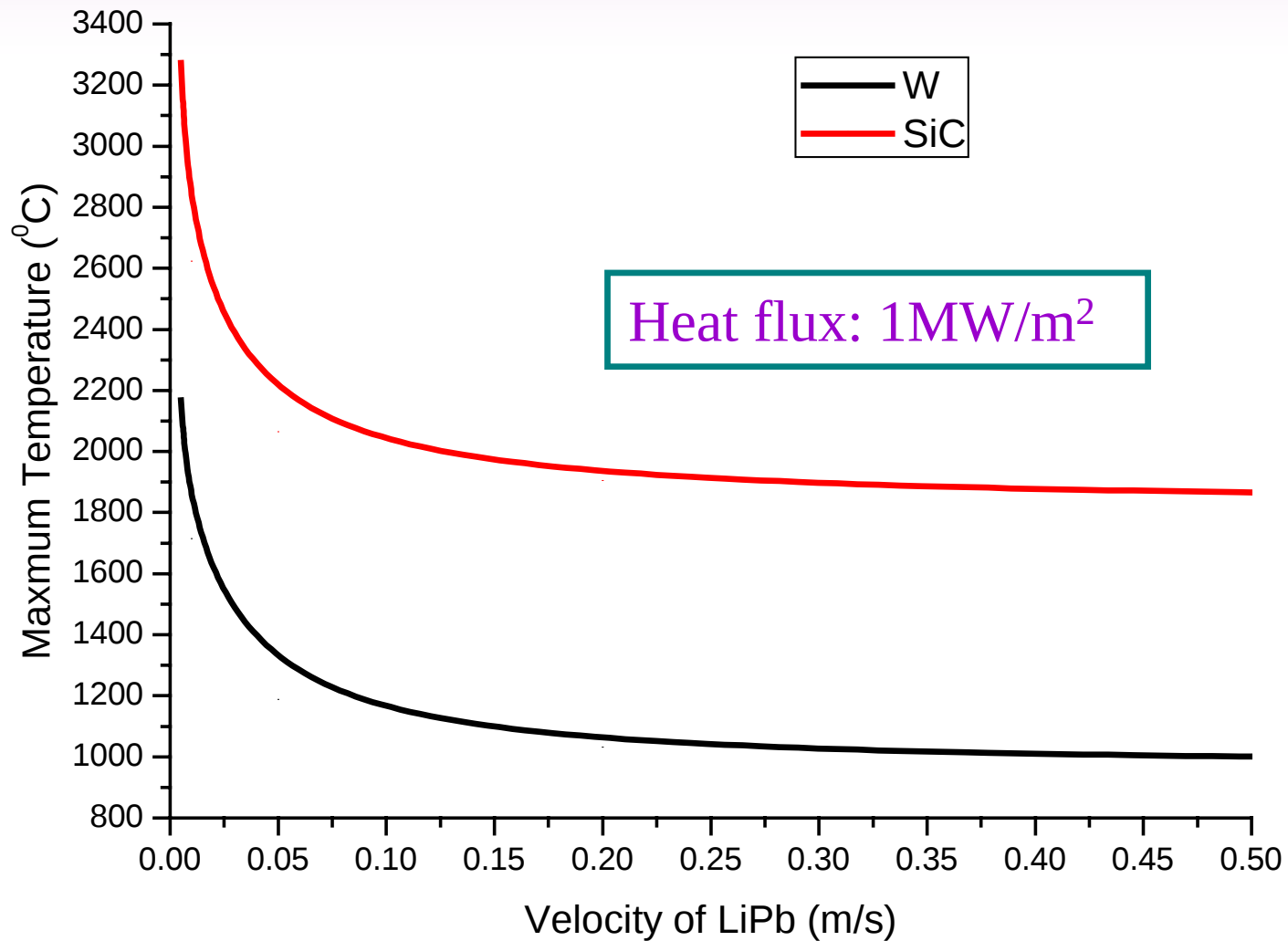
Maximum:13100MPa
>> Allowable thermal stress of SiC

Note: $V=0.05\text{m/s}$ (FLiBe)

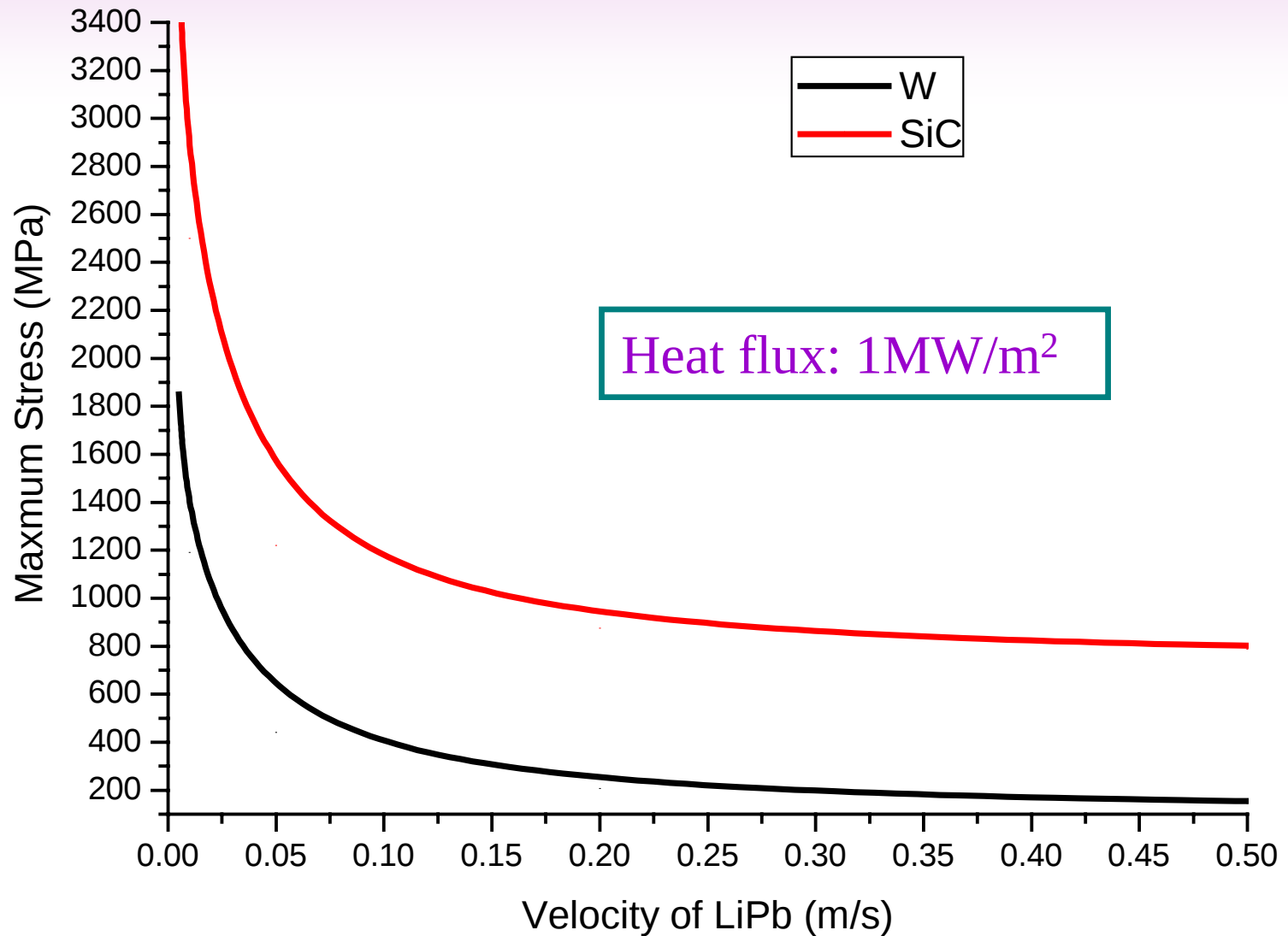
Material of FW: SiC/SiC



```
ZV  =1
*DIST=-.116369
*XF  =.114977
*YF  =.847E-03
Z-BUFFER
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.292E+10
.438E+10
.584E+10
.729E+10
.875E+10
.102E+11
.117E+11
.131E+11
```



Maximum Temperature on the First Wall with different velocity of LiPb



Maximum Stress on the First Wall with different velocity of LiPb

Summary and future work plan

- My work just begin and lots of work need to be developed. It's my honor if I can get some comments or suggestions from all of the specialists.
 - Next I will design detailed structure and then do some assessment for each structure and choose a better structure based on the results of MHD,Heat transfer and mechanical analysis.
 - Finally I will considered all of the effect factors and then give some detailed **design windows** for LAR Tokamak Reactor engineering design.
-

Plasma disruption and Electromagnetic issues:

1. Effects on Liquid Metal Flow and its heat transfer

2. Time constants for control Field penetration due to LM blanket:

Deep blanket penetration mainly depends on the details of geometry and conducting paths available. How to connect each sector? And how to evaluate the blanket time constants?

3. Halo current due to vertical displacement events effect on the fluid flow in first wall including stress concentration on its supporting system

4. EM Force in LM due to the plasma disruption and quench of superconducting coils

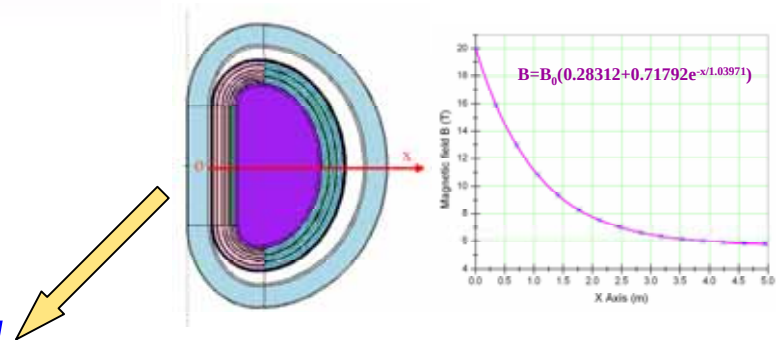
5. Additional stress on structure materials of Blanket due to EM force

6. Arcing in some small gap area, leading to insulator damage and welding of structure break

During design how to consider these factors?

Future work: Analysis, Experiment and Assessment

- *Mechanical stress analysis*
- *Thermal hydraulic analysis*
- *EM force and eddy current analysis*
- *MHD under non-uniform magnetic field*
- *Connection and Supporting system of Blanket*



Declining curve of magnetic field in Vacuum vessel

- Predict the lifetime based on the swelling limit
- Evaluate of the effects of radiation creep on the allowable design stresses
- Fracture mechanics analysis to understand the micro-crack propagation
- Fatigue analysis from the engineering design
- Assessment of **Loss of coolant accident** and **Loss of flow accident**

We also want to corporate with Kyoto University, Osaka University and other Institute for some further experiments.

Thanks!