

Overview of US Power Plant Studies:

A) Results from ARIES-IFE Study

B) Plans For Compact Stellarator

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Electronic copy: <http://aries.ucsd.edu/najmabadi/TALKS>

ARIES Web Site: <http://aries.ucsd.edu/ARIES>

ARIES Program charter was expanded in FY00 to include both IFE and MFE concepts

ARIES activities in FY03:

- **ARIES-IFE study was continued for another year (~50% of the effort):**
 - ✓ The ARIES-IFE study is now officially completed.
 - ✓ Work in FY03 was focused on thick-liquid wall concept (*i.e.*, HYLIFE)
 - ✓ Results from 2001 and 2002 research will appear in Journal of Fusion Science & Technology (pre-prints available on ARIES Web site).
- **ARIES compact stellarator (ARIES-CS) was started (~50% of effort)**
 - ✓ This is a three-years study
 - ✓ All of ARIES Team effort will be devoted to ARIES-CS in FY04.

**Selected Results from
ARIES-IFE Studies
(Laser-Driven Direct-Drive Systems)**

ARIES Integrated IFE Chamber Analysis and Assessment Research Is An Exploration Study

Objectives:

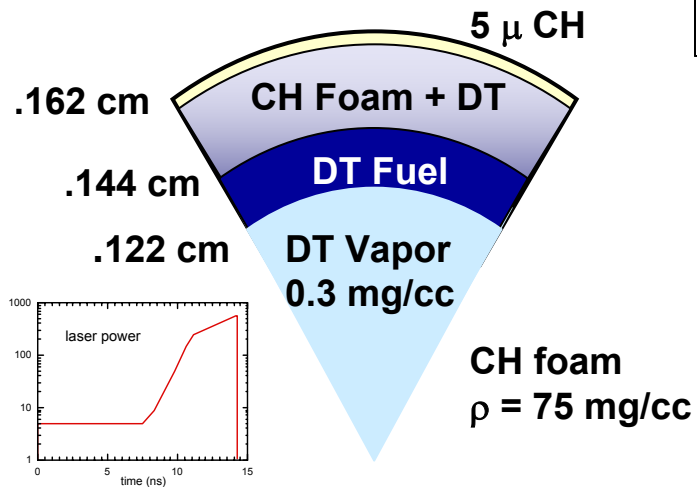
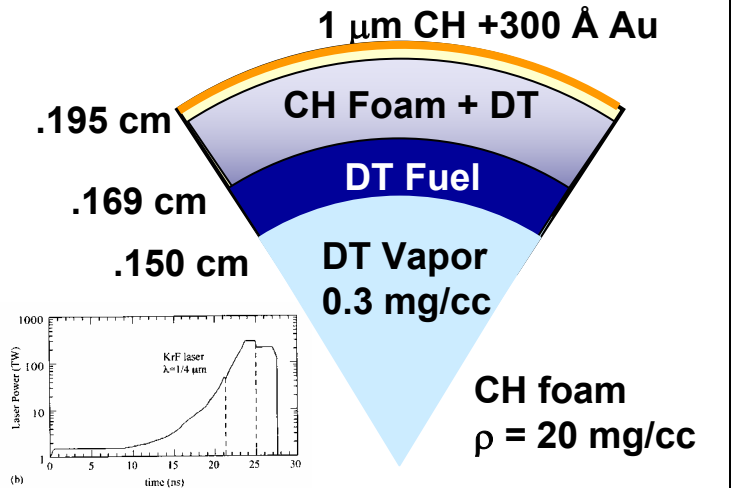
- Analyze & assess integrated and self-consistent IFE chamber concepts
- Understand trade-offs and identify design windows for promising concepts. *The research is **not** aimed at developing a point design.*

Approach:

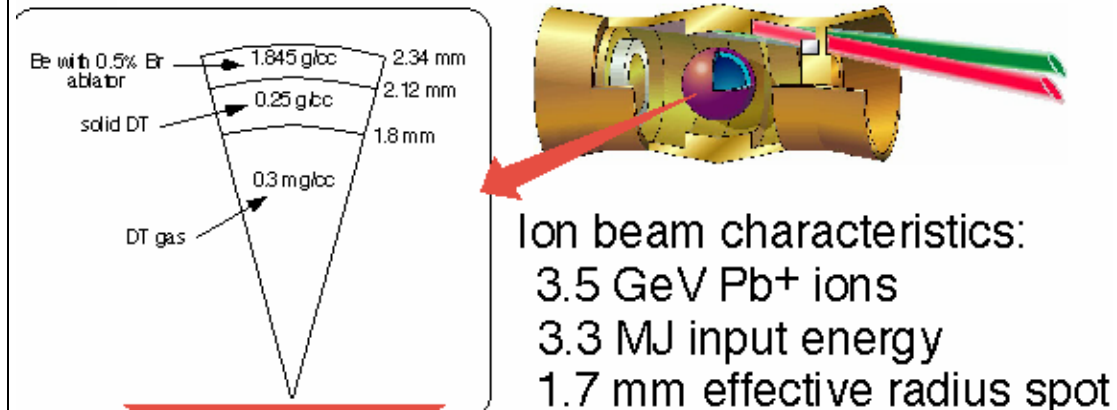
- Six classes of target were identified. Advanced target designs from NRL (laser-driven direct drive) and LLNL (Heavy-ion-driven indirect-drive) are used as references.
- To make progress, we divided the activity based on three classes of chambers:
 - Dry wall chambers;
 - Solid wall chambers protected with a “sacrificial zone” (such as liquid films);
 - Thick liquid walls.
- We research these classes of chambers in series with the entire team focusing on each.

Reference Direct and Indirect Target Designs

NRL Advanced Direct-Drive Targets



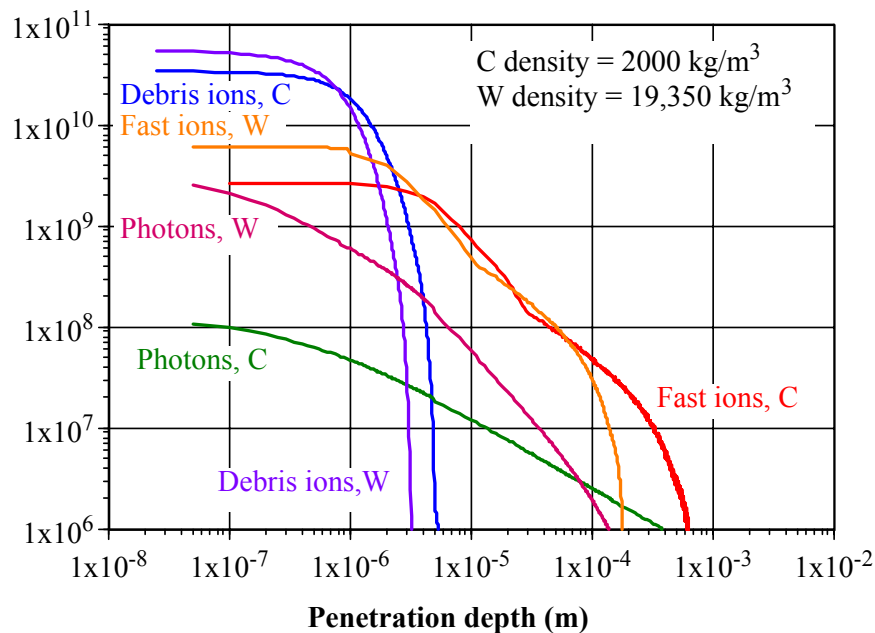
LLNL/LBNL HIF Target



- NRL Direct Drive Target Gain Calculations (1-D) have been corroborated by LLNL and UW.

Details of Target Spectra Has A Strong Impact on the Thermal Response of the Wall

Energy Deposition (J/m^2) in C and W Slabs (NRL 154MJ Direct Drive Target)



- Heat fluxes are much lower than predicted in previous studies:
- ✓ A much smaller portion of target yield is in X-rays.
- ✓ Time of flight of ions spread the temporal profile of energy flux on the wall over several μs .
- A cover gas may not be necessary for protecting the chamber wall

- Photon and ion energy deposition falls by 1-2 orders of magnitude within 0.1 mm of surface.

Dry Wall Concepts

Thermal Response of a W Flat Wall

- NRL direct-drive target in 6.5-m chamber with no gas protection:

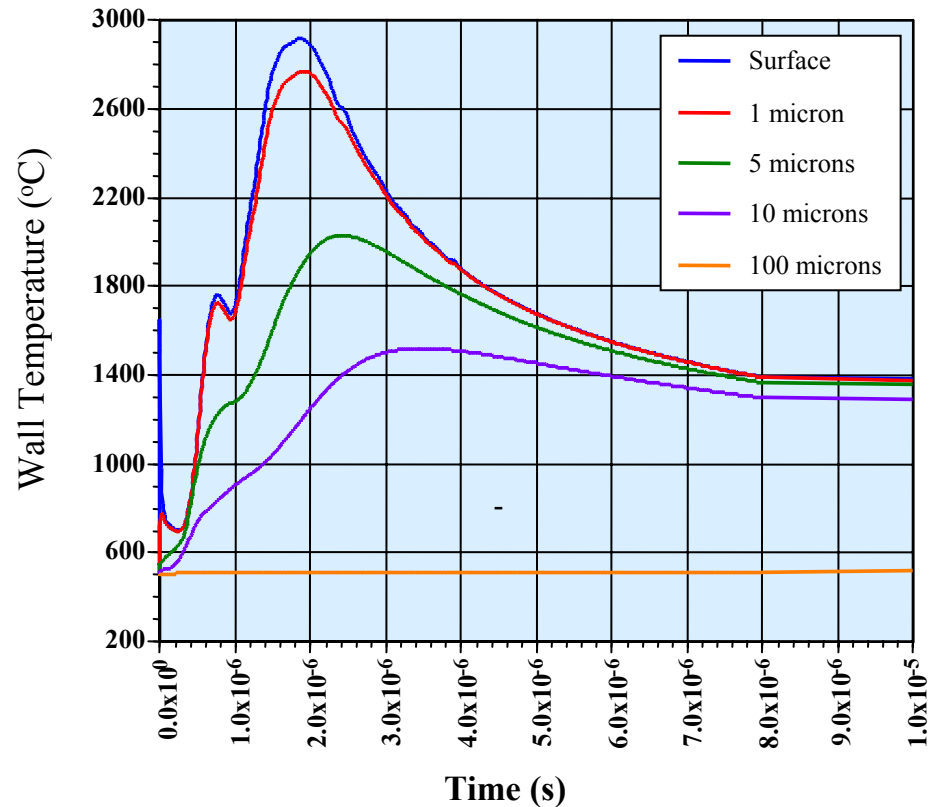
**3-mm thick W
Chamber Wall**

Coolant at 500°C

**Energy
Front**

**Evaporation heat
flux B.C. at incident
wall**

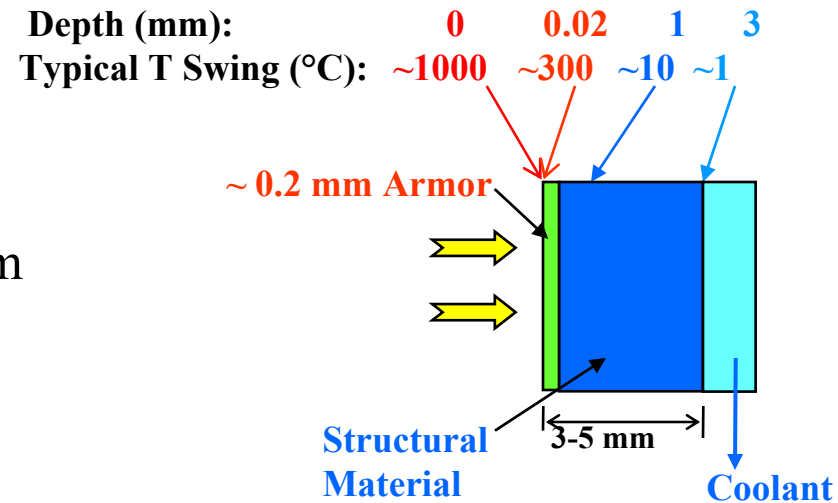
**Convection B.C. at
coolant wall:
 $h = 10 \text{ kW/m}^2\text{-K}$**



- Temperature variation mainly in thin (0.1-0.2 mm) region.
- Margin for design optimization (a conservative limit for tungsten is to avoid reaching the melting point at 3,410°C).
- Similar margin for C slab.

All the Action Takes Place within 0.1-0.2 mm of Surface -- Use an Armor

- Photon and ion energy deposition falls by 1-2 orders of magnitude within 0.1-0.2 mm of surface.
- Beyond the first 0.1-0.2 mm of the surface. First wall experiences a much more uniform q'' and quasi steady-state temperature (heat fluxes similar to MFE).
- **Use an Armor**
 - ✓ **Armor optimized to handle particle and heat flux.**
 - ✓ **First wall is optimized for efficient heat removal.**
- Most of neutrons deposited in the back where blanket and coolant temperature will be at quasi steady state due to thermal capacity effect
- **Blanket design can be adapted from MFE blankets**
- **Significant high-energy ion flux on the armor.**



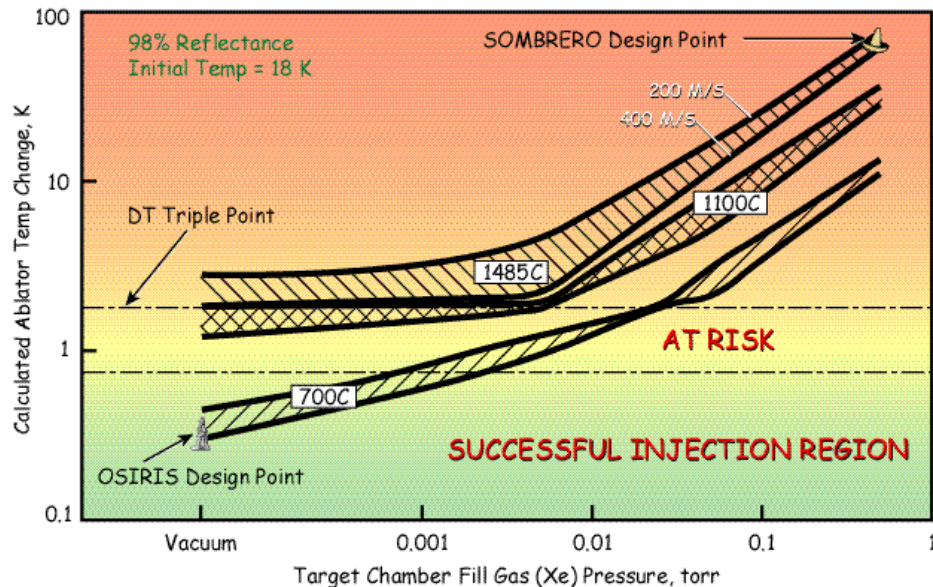
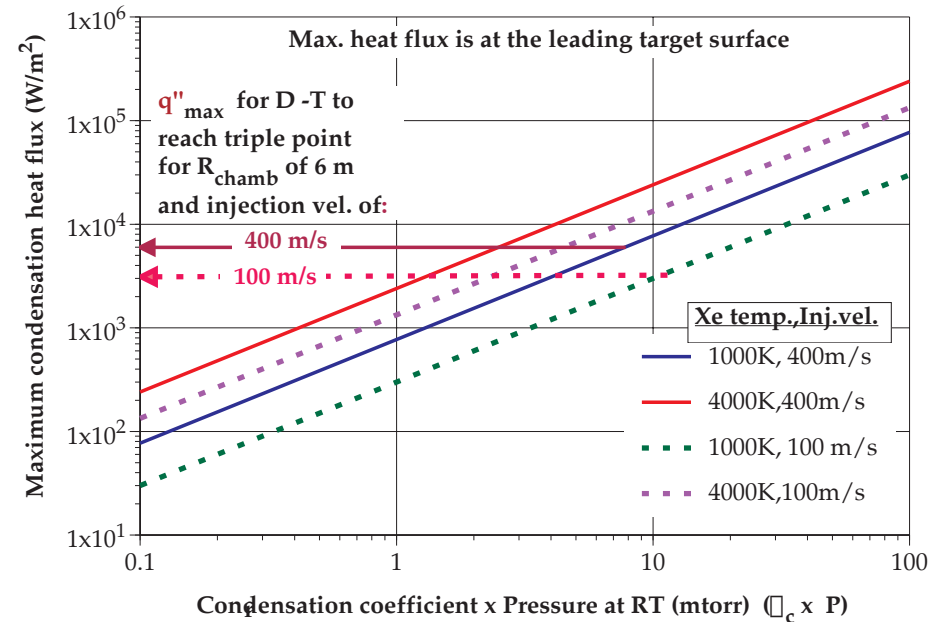
IFE Armor Conditions are similar to those for MFE PFCs (ELM, VDE, Disruption)

	ITER Type -I ELM's	ITER VDE's	ITER Disruptions	Typical IFE Operation (direct-drive NRL target)
Energy	<1 MJ/m ²	~ 50 MJ/m ²	~ 10 MJ/m ²	~ 0.1 MJ /m ²
Location	Surface near div. strike points	surface	surface	bulk (~μm's)
Time	100-1000 μs	~ 0.3 s	~ 1 ms	~ 1-3 μs
Max. Temperature	melting/ sublimation points	melting/ sublimation points	melting/ sublimation points	~ 1500-2000 °C (for dry wall)
Frequency	Few Hz	~ 1 per 100 cycles	~ 1 per 10 cycles	~ 10 Hz
Base Temperature	200-1000 °C	~ 100 °C	~ 100 °C	~ >500 °C

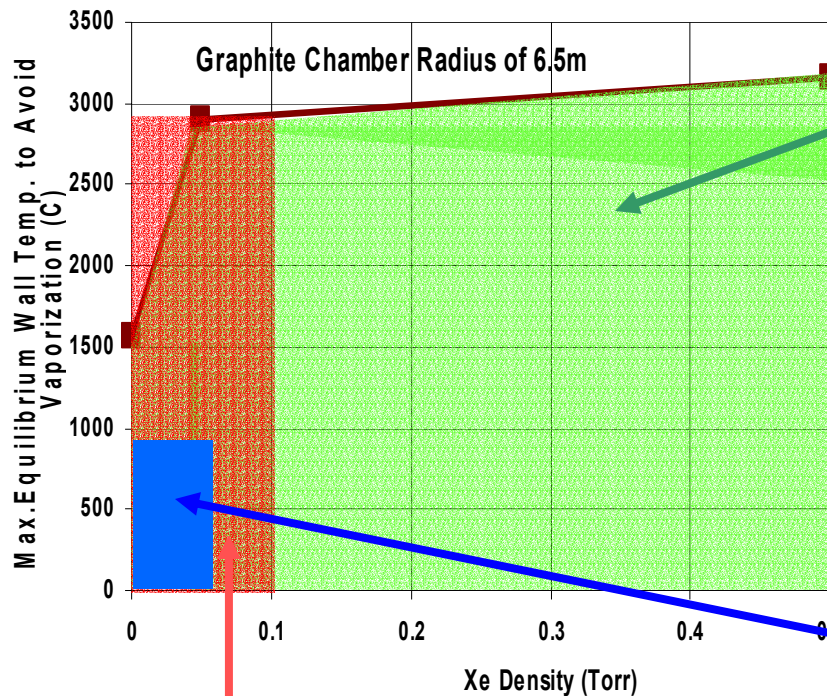
- There is a considerable synergy between MFE plasma facing components and IFE chamber armor.

Target injection Design Window Naturally Leads to Certain Research Directions

- Direct-drive targets (initial $T=18\text{K}$) are heated during their travel in the chamber by:
- Friction with the chamber gas (mainly through condensation heat flux) requiring
 - ✓ Lower gas pressure
 - ✓ Slower injection velocity
- Radiation heat flux from hot first wall, requiring
 - ✓ Lower equilibrium temperature
 - ✓ Faster injection velocity
- Addition of a thin ($\sim 70\mu\text{m}$) foam improves the thermal response considerably.



Design Windows for Direct-Drive Dry-wall Chambers



Laser propagation design window(?)

- ✓ Experiments on NIKE

Thermal design window

- ✓ Detailed target emissions
- ✓ Transport in the chamber including time-of-flight spreading
- ✓ Transient thermal analysis of chamber wall
- ✓ No gas is necessary

Target injection design window

- ✓ Heating of target by radiation and friction
- ✓ Constraints:
 - Limited rise in temperature
 - Acceptable stresses in DT ice

Wetted-Wall Concepts

Aerosol Generation and Transport is the Key Issue for Thin-Liquid Wall Concepts

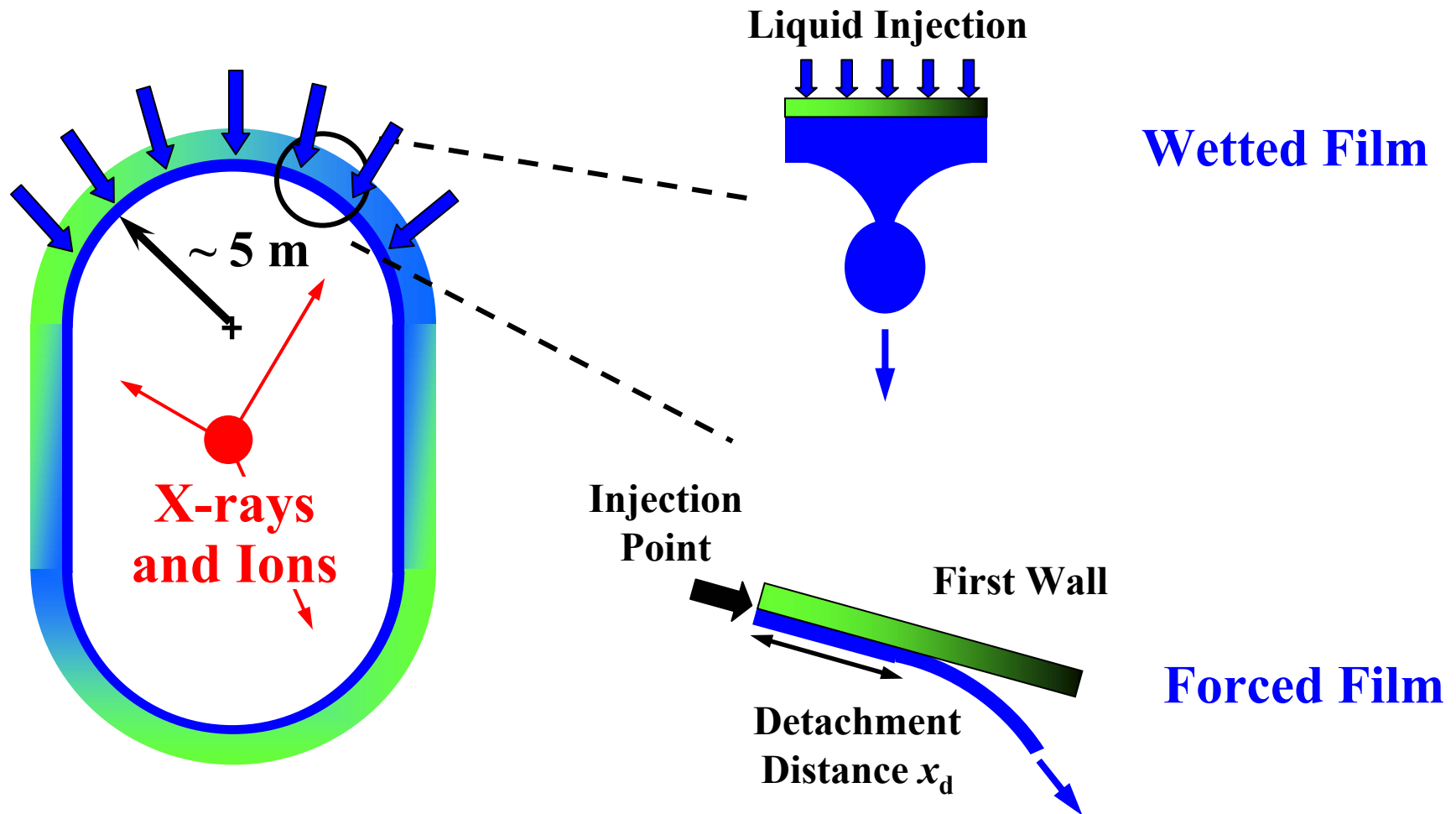
A renewable thin-liquid protection resolve several issues:

- It can handle a much higher heat fluxes compared to solid surfaces;
- It will eliminate damage to the armor/first wall due to high-energy ions.

A renewable thin-liquid protection, however, introduces its own critical issues:

- Fluid-dynamics aspects (establishment and maintenance of the film)
 - ✓ “Wetted wall:” Low-speed normal injection through a porous surface
 - ✓ “Forced film:” High-speed tangential injection along a solid surface
- Chamber clearing (recondensation of evaporated liquid)
 - ✓ “Source term:” both vapor and liquid (e.g., explosive boiling) are ejected
 - ✓ Super-saturated state of the chamber leads to aerosol generation
 - ✓ Target injection and laser beam propagation lead to sever constraints on the acceptable amount and size of aerosol in the chamber.

Two Methods for Establishment of Thin-Liquid Walls Have Been Proposed



We Have Developed Design Widows for Establishment and Stability of the Protective Film

“Wetted-wall” concept:

- Developed general non-dimensional charts for film stability over a wide variety of candidate coolants and operating conditions.
- Model predictions are closely matched with experimental data.
- It will eliminate damage to the armor/first wall due to high-energy ions.

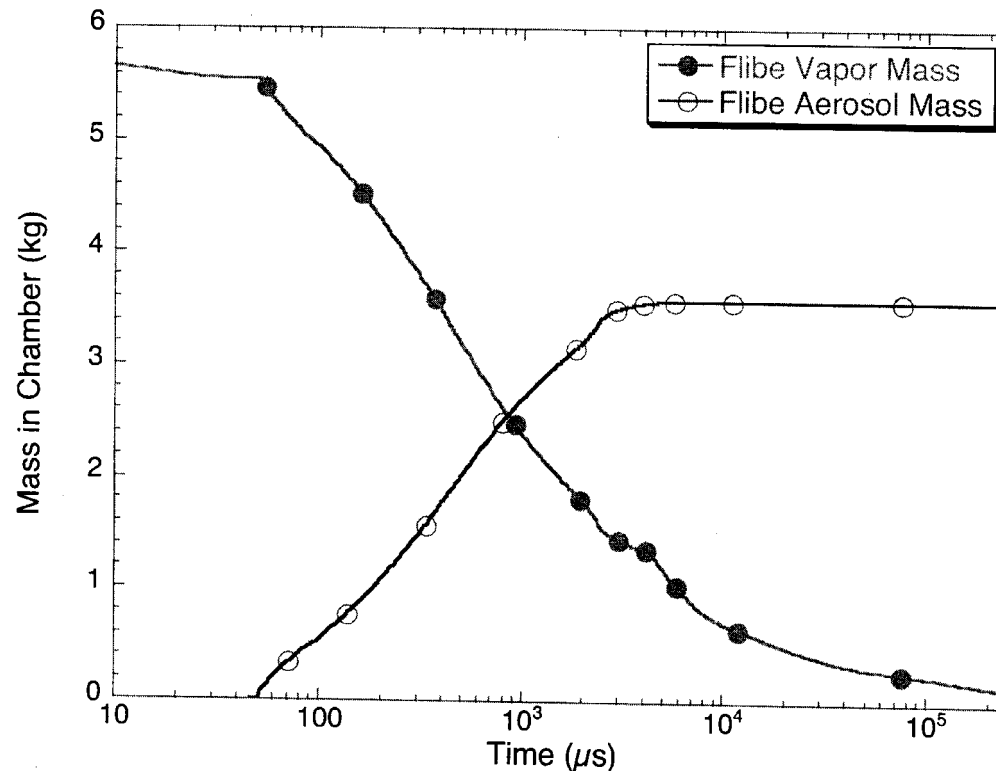
“Forced-flow” concept:

- Developed non-dimensional design widows for longitudinal spacing of injection/coolant/removal slots to maintain attached protective film;
- A wetting first wall surface requires fewer injection slots than non-wetting surface – Wetting surfaces are more desirable.

- Details are given in Prof. Abdel-Khalik’s Presentation.

Most of Ablated Material Would Be in The Form of Aerosol

- FLiBe aerosol and vapor mass history in a 6.5-m radius following a target explosion (ablated thickness of 5.5 mm)
- Most of ablated material remains in the chamber in aerosol form;
- Only homogeneous nucleation and growth from the vapor phase.



There Are Many Mechanism of Aerosol Generation in an IFE Chamber

- Homogeneous nucleation and growth from the vapor phase
 - ✓ Supersaturated vapor
 - ✓ Ion seeded vapor
- Phase decomposition from the liquid phase
 - ✓ Thermally driven phase explosion
 - ✓ Pressure driven fracture
- Hydrodynamic droplet formation (May be critical in Thick-liquid Wall Concepts’')

➤ Details are given in Dr. Tillack’s Presentation.

ARIES Research Plans for FY03-FY05

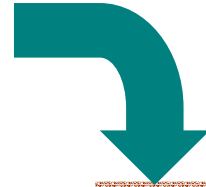
We Have Initiated a Three-Years Study of Compact Stellarators as Power Plants

- Initiation of NCSX and QSX experiments in US; Successful operation of LHD in Japan and construction of W7X in Germany;
- Review committees have asked for assessment of compact stellarator option as a power plant; Similar interest has been expressed by national stellarator program.
- Such a study will advance physics and technology of compact stellarator concept and addresses concept attractiveness issues that are best addressed in the context of power plant studies.
- NCSX and QSX plasma/coil configurations are optimized for most flexibility for scientific investigations. Optimum plasma/coil configuration for a power plant may be different. Identification of such optimum configuration will help compact stellarator research program.

ARIES-Compact Stellarator Program Was Proposed as a Three-year Study

FY03: Assessment of systems options

1. Develop physics requirements and modules (power balance, stability, α confinement, divertor, *etc.*)
2. Develop engineering requirements and constraints.
3. Explore attractive coil topologies.



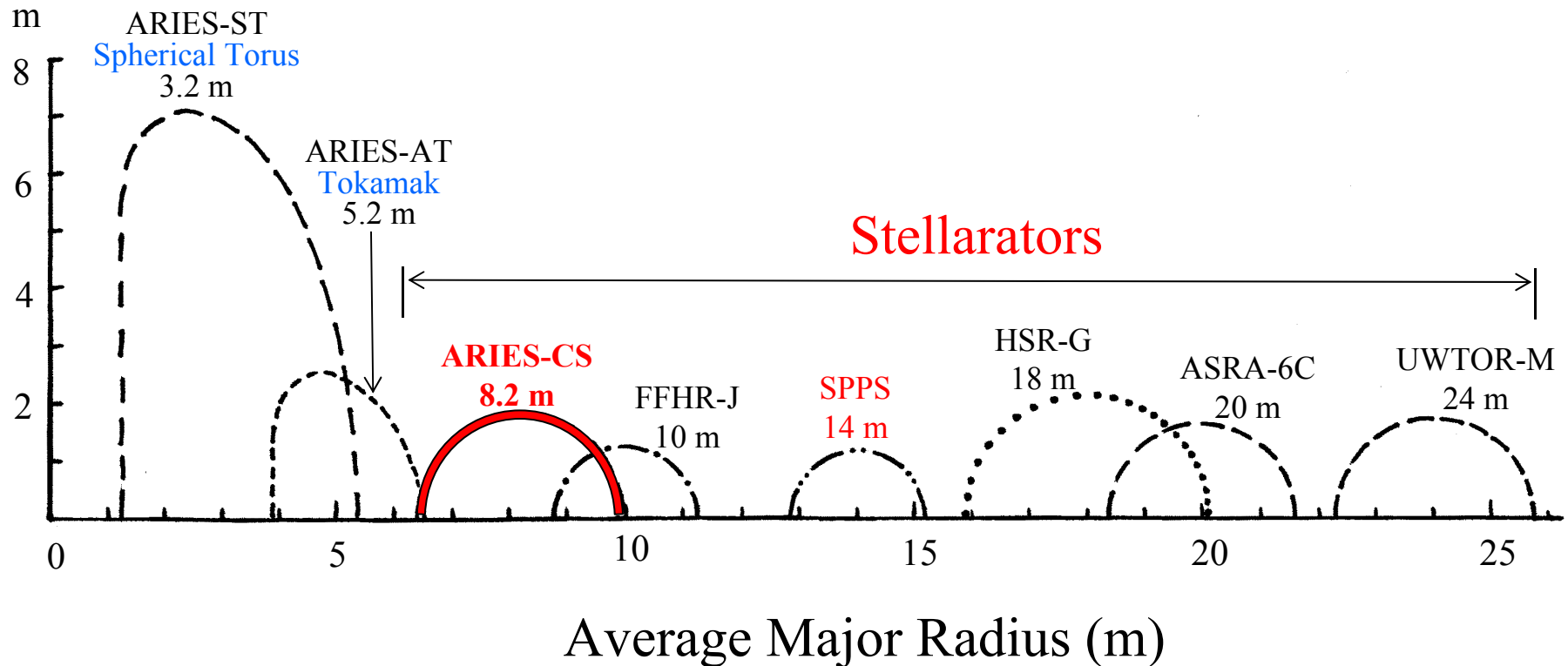
FY04: Exploration of Configuration Design Space

1. Physics: β , aspect ratio, number of periods, rotational transform, shear, *etc.*
2. Engineering: configurationally optimization, management of space between plasma and coils.
3. Choose one configuration for detailed design.



FY05: Detailed system design and optimization

Comparison of Power Plant Sizes



Status of ARIES-CS Study

- Because only half of ARIES effort was devoted to ARIES-CS in FY03 and reduction in funding in FY04, the study will probably stretch into FY 06.
- We have developed two candidate configuration for a self-consistent evaluation (Details in Dr. Mau's Presentation).
- Our initial engineering assessment has highlighted maintenance as a key driver for blanket selection. (Details in Dr. Raffray's Presentation).
- An ARIES Town-Meeting with Stellarator physicist is planned for Dec. 5-6 in PPPL.
- We should explore possibilities of collaborations in the helical systems in this workshop.