

ARIES: Fusion Power Core and Power Cycle Engineering

The ARIES Team

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Presentation Outline

Power Core and Power Cycle Engineering:

- **Power Cycle**
- **Blanket**
- **Divertor**
- **Material**



Approach Relies on:

- **Detailed Analysis**
 - Using up-to-date analysis tools
 - Developing tools for specific analytical needs
- **Application of creative solutions to extend design window**
- **Building Block**
 - build on previous ARIES design experience in bettering the end product
- **Community Interaction**
 - utilize national and international community input in evolving material properties and component parameters
 - develop clear goals for R&D program showing benefits

Power Cycle: Quest for High Efficiency

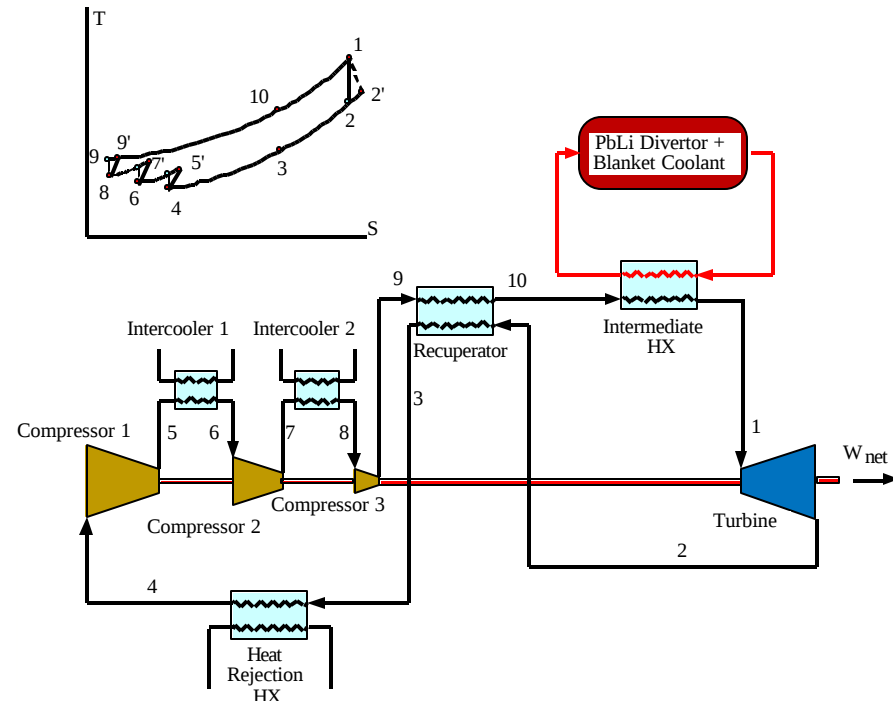
**Conventional
Steam Cycle:
Steel/Water**
 $h = 35\%$

**ARIES-RS
Li/V
Supercritical
Rankine (water):**
 $h = 45\%$

**ARIES-ST
FS/He/Pb-17Li
Brayton
(Low Temp. He):**
 $h > 45\%$

**ARIES-AT
(SiC/SiC)/Pb-17Li
Brayton
(High Temp. He):**
 $h = 59\%$

- High efficiency translates in lower COE and lower heat load
- Brayton cycle is best near-term possibility of power conversion with high efficiency
 - Maximize potential gain from high-temperature operation with SiC/SiC
 - Compatible with liquid metal blanket through use of IHX



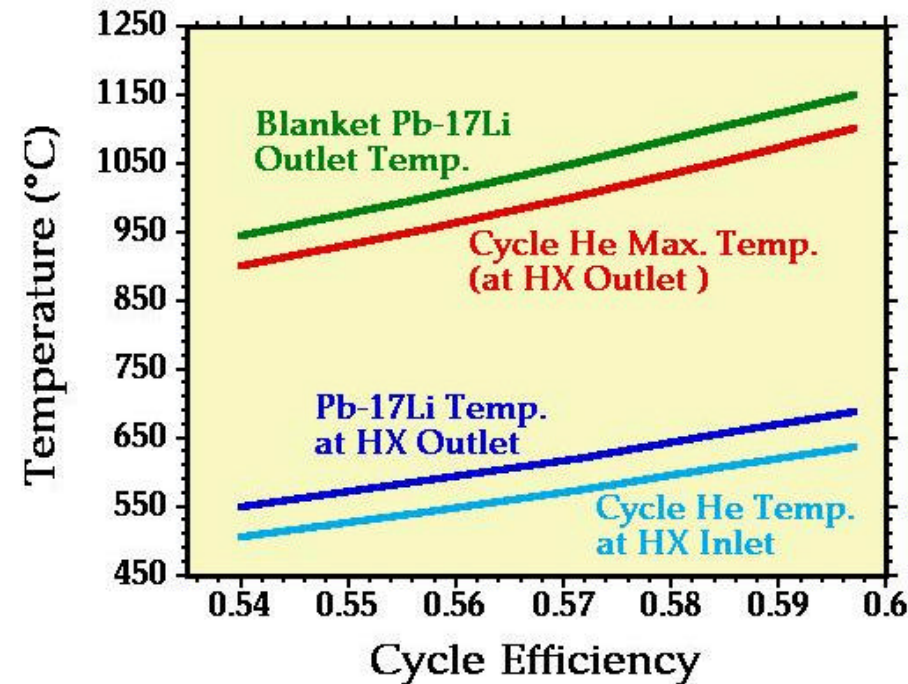
Brayton Cycle Based on Near-Term Technology and Advanced Recuperator Design Yields High Efficiency

Advanced Brayton cycle developed with expert input from GA and FZK, Karlsruhe

- FZK/UCSD ISFNT-4 paper, 1997
- GA/UCSD ANS TOFE-14 paper, 2000



- Min. He Temp. in cycle (heat sink) = 35°C
- 3-stage compression with 2 inter-coolers
- Turbine efficiency = 0.93
- Compressor efficiency = 0.88
- Recuperator effectiveness = 0.96
- Cycle He fractional DP = 0.03
- Total compression ratio set to optimize system (= 2-3)



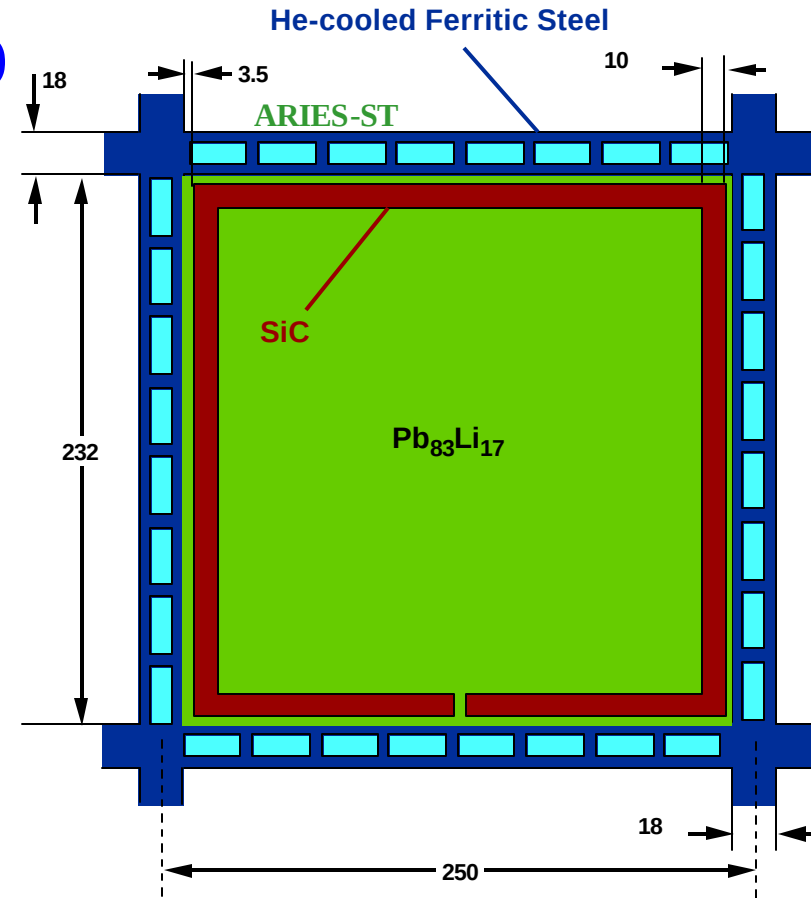
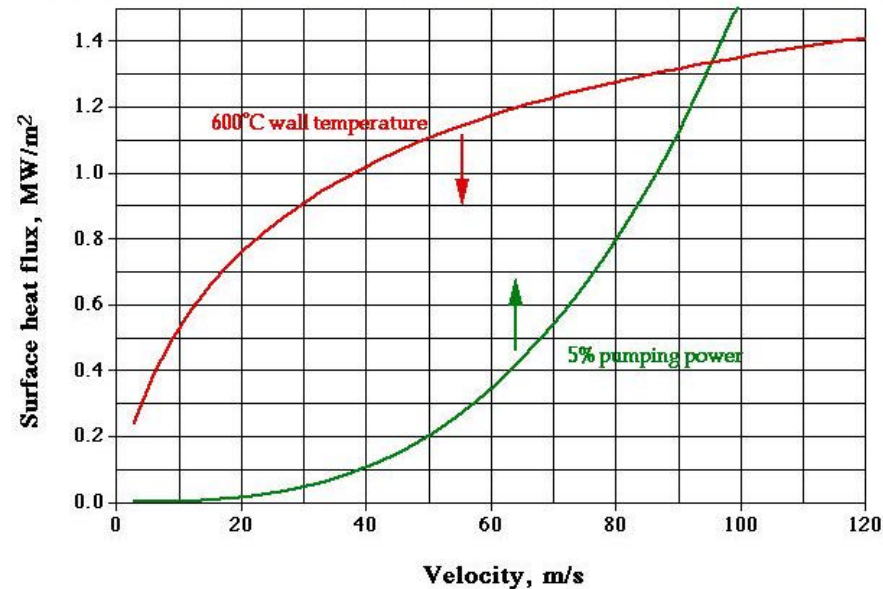
High Efficiency Requires High Temperature Operation

- **Conventionally, maximum coolant temperature is limited by structural material maximum temperature limit**
- **Innovative design solutions in ARIES-ST and ARIES-AT allow the blanket coolant exit temperature to be higher than the structure temperature**

ARIES-ST Utilizes a Dual Coolant Approach to Uncouple Structure Temperature from Main Coolant Temperature

- ARIES-ST: Ferritic steel+Pb-17Li+He
- Flow lower temperature He (350-500°C) to cool structure and higher temperature Pb-17Li (480-800°C) for flow through blanket

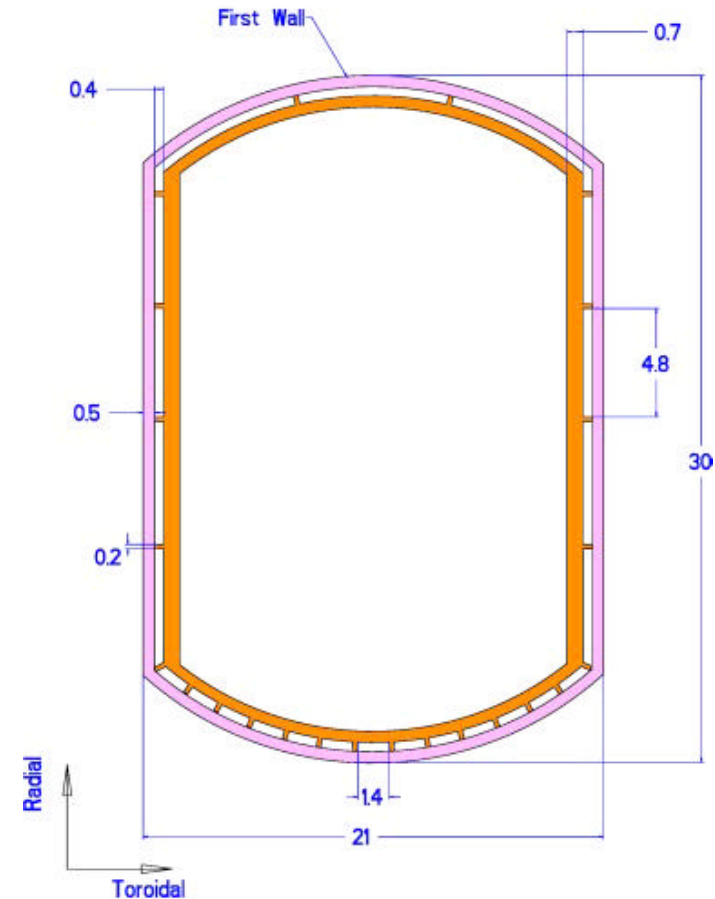
ARIES-ST First Wall Thermal-Hydraulic Design Window



ARIES-AT Utilizes a 2-Pass Coolant Approach to Uncouple Structure Temperature from Outlet Coolant Temperature

- **ARIES-AT: 2-pass Pb-17Li flow, first pass to cool SiC/SiC box and second pass to “superheat” Pb-17Li**
- **Maintain blanket SiC/SiC temperature ($\sim 1000^{\circ}\text{C}$) < Pb-17Li outlet temperature ($\sim 1100^{\circ}\text{C}$)**

Cross-Section of ARIES-AT Outboard FW/Blanket
(Unit in cm)

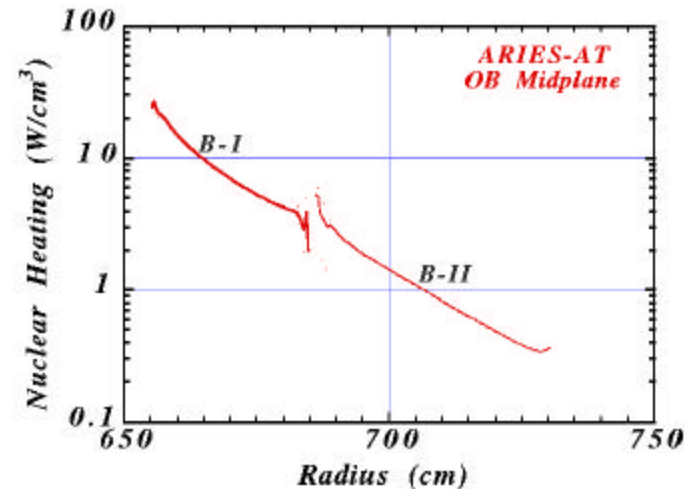
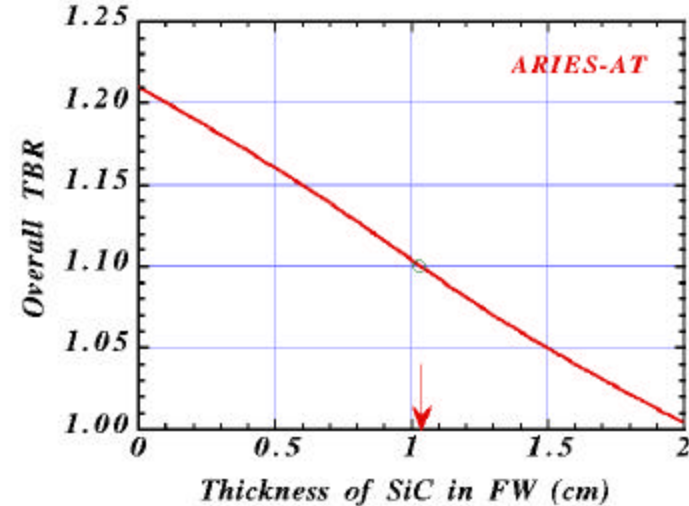


UCSD
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Detailed Modeling and Analysis Required to Demonstrate Blanket Performance

Multi-dimensional neutronics analysis

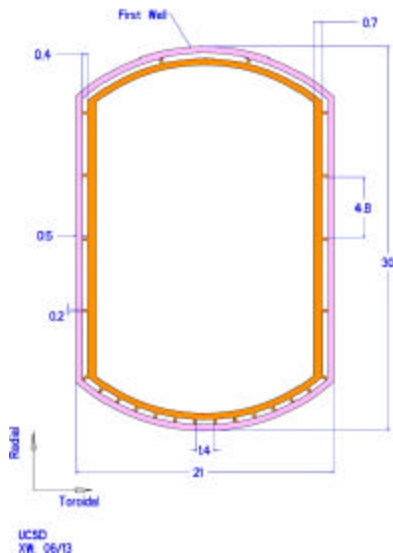
- Latest data and code
- Tritium breeding requirement influences blanket material and configuration choices
- Blanket volumetric heat generation profiles used for thermal-hydraulic analyses



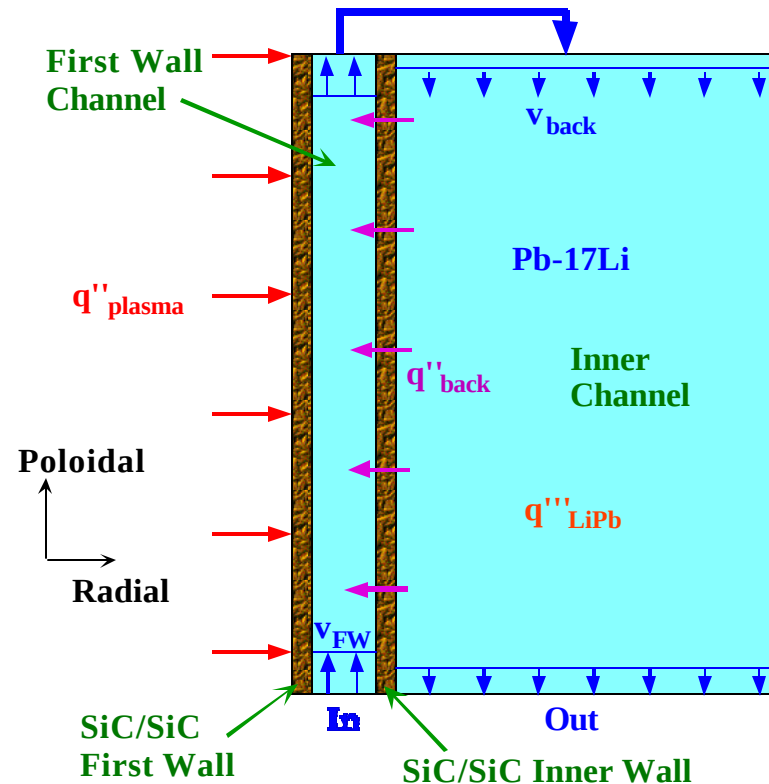
Accommodation of Material Temperature Limits Verified by Detailed Modeling

Moving Coordinate Analysis to Obtain Pb-17Li Temperature Distribution in ARIES-AT First Wall Channel and Inner Channel under MHD-Laminarization Effect

Cross-Section of ARIES-AT Outboard FW/Blanket
(Unit in cm)

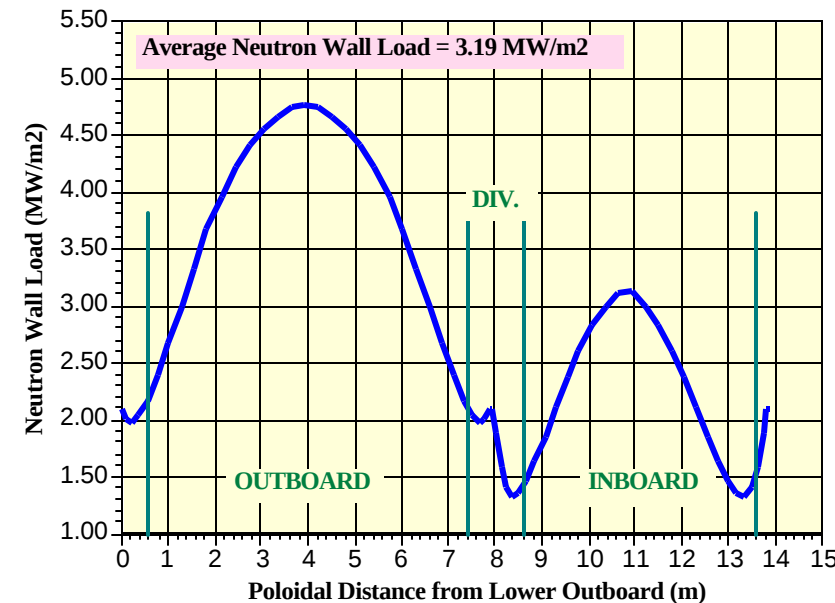
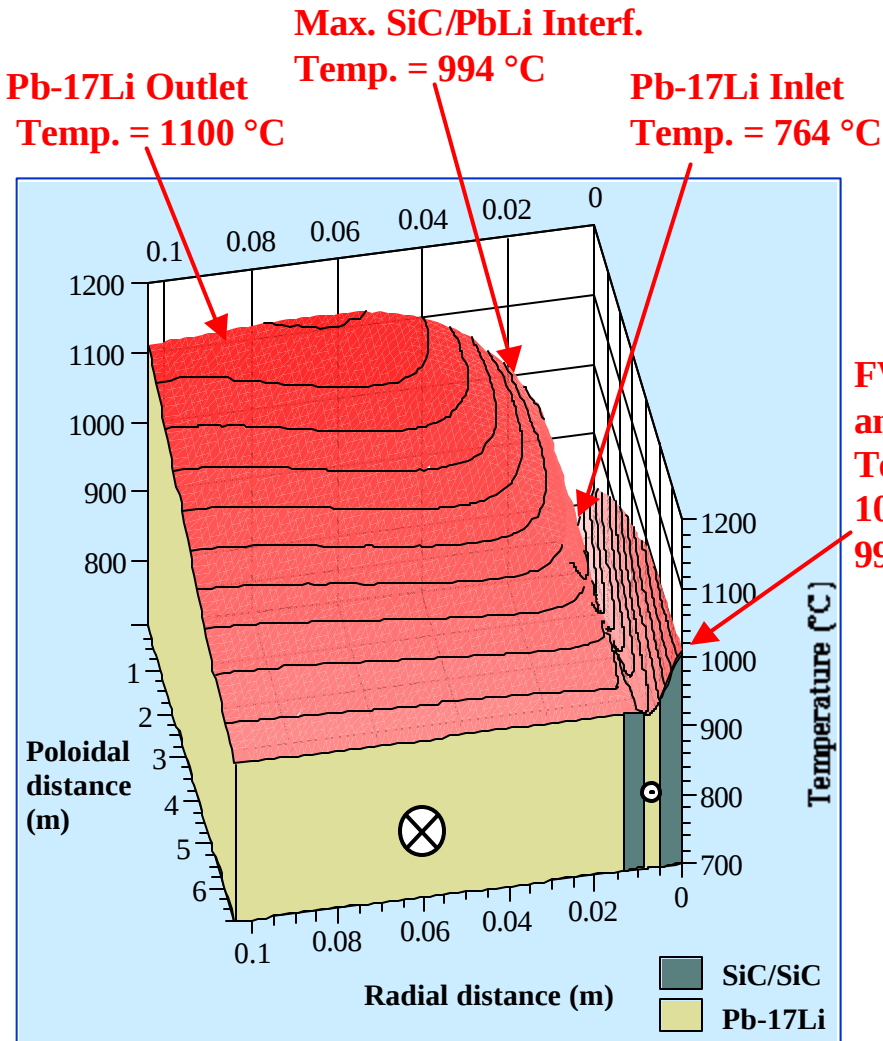


ARIES-AT Outboard
Blanket Segment



Temperature Distribution in ARIES-AT Blanket Based on Moving Coordinate Analysis

- Use plasma heat flux poloidal profile
- Use volumetric heat generation poloidal and radial profiles
- Iterate for consistent boundary conditions for heat flux between Pb-17Li inner channel zone and first wall zone
- Calibration with ANSYS 2-D results

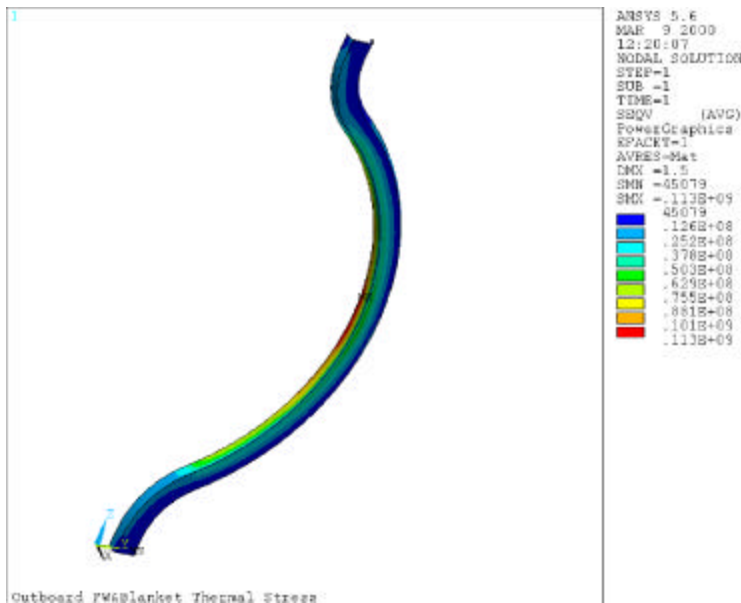


Detailed Stress Analysis Using Latest Tool for Maintaining Conservative Design Margins

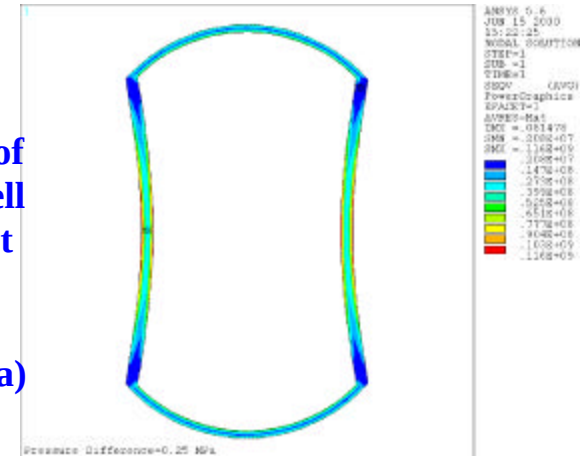
Example of 2-D and 3-D Thermal and Stress Analysis of ARIES-AT Blanket Using ANSYS

Conservative SiC/SiC stress limit from Town Meeting:
Max. allowable thermal + pressure $\sigma = 190$ MPa

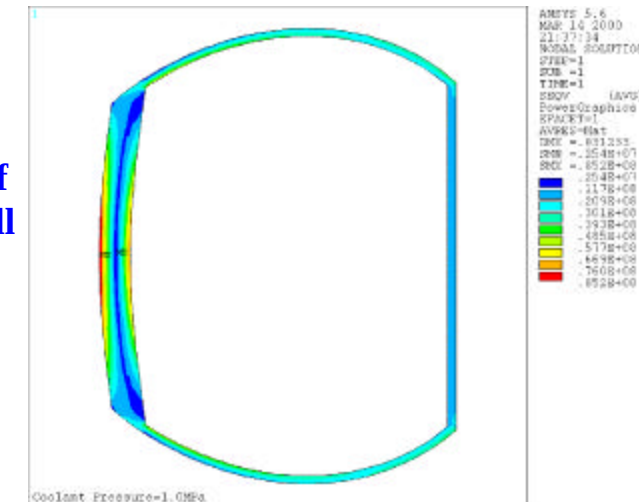
Thermal Stress Distribution in Toroidal Half of Outboard Blanket Module (Max. $\sigma = 113$ MPa)



Pressure Stress Analysis of Inner Shell of Blanket Module (Max. $\sigma = 116$ MPa)



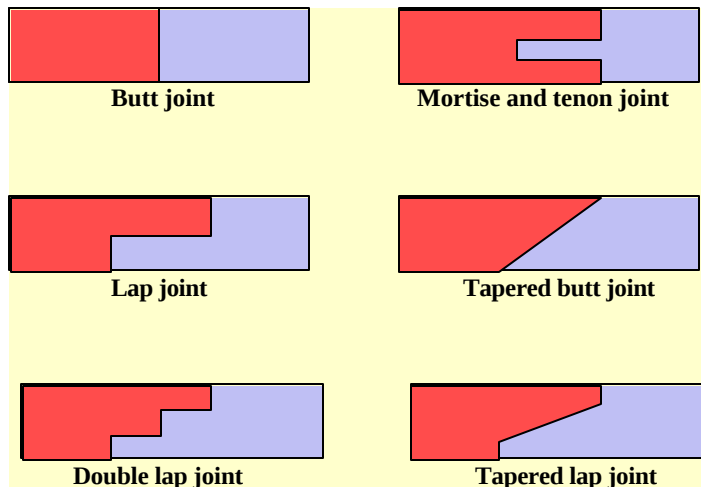
Pressure Stress Analysis of Outer Shell of Blanket Module (Max. $\sigma = 85$ MPa)



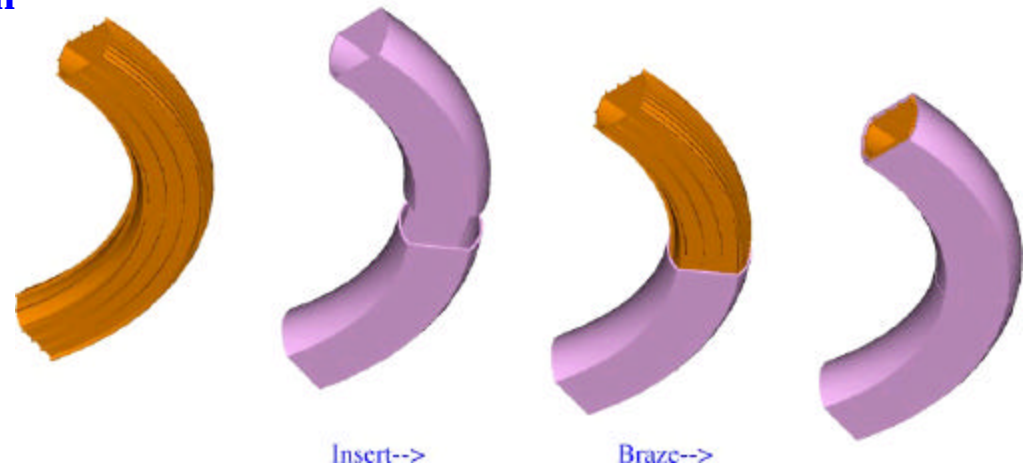
Develop Plausible Fabrication Procedure and Minimize Joints in High Irradiation Region

Example Procedure for ARIES-AT Blanket

1. Manufacture separate halves of the SiC_f/SiC poloidal module by SiC_f weaving and SiC Chemical Vapor Infiltration (CVI) or polymer process;
2. Insert the free-floating inner separation wall in each half module;
3. Braze the two half modules together at the midplane;

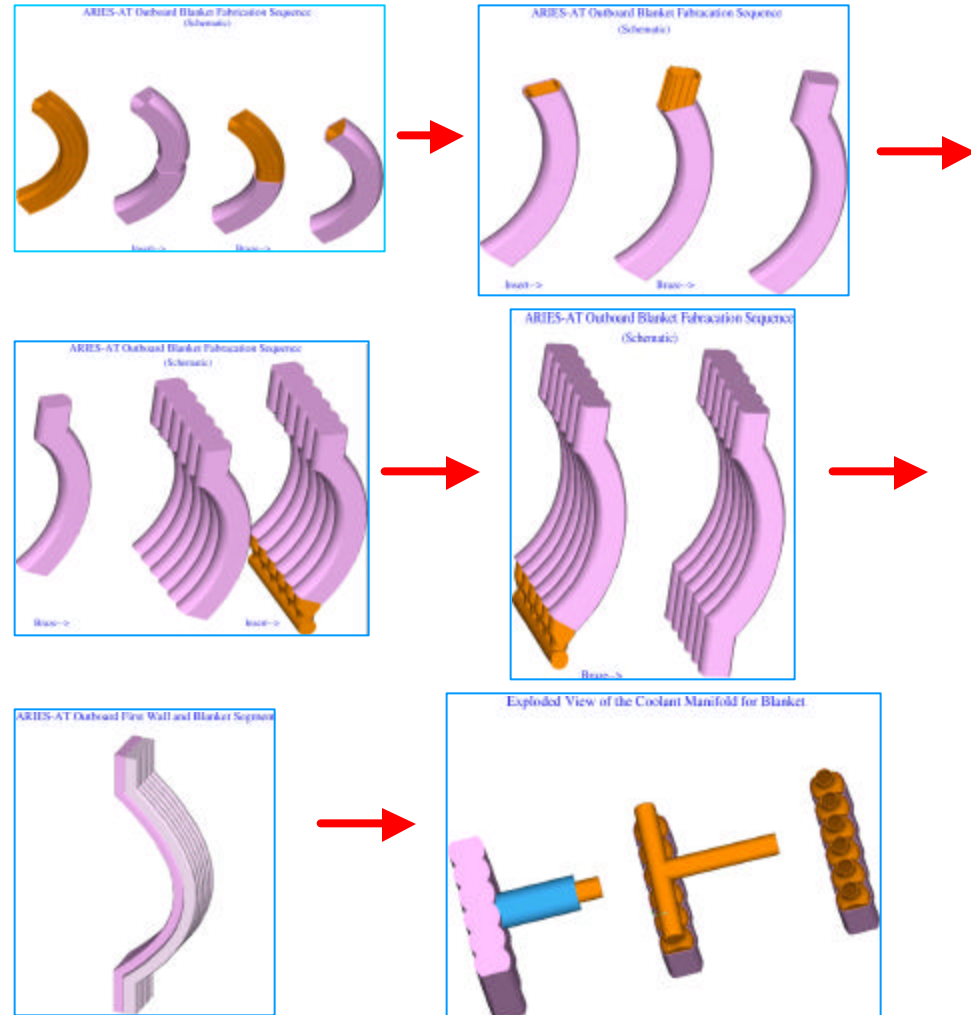


ARIES-AT Outboard Blanket Fabrication Sequence (Schematic)



ARIES-AT Blanket Fabrication Procedure Comprises:

1. Manufacturing separate halves of the SiC_f/SiC poloidal module by SiC_f weaving and SiC Chemical Vapor Infiltration (CVI) or polymer process;
2. Inserting the free-floating inner separation wall in each half module;
3. Brazing the two half modules together at the midplane;
4. Brazing the module end cap;
5. Forming a segment by brazing six modules together (this is a bond which is not in contact with the coolant); and
6. Brazing the annular manifold connections to one end of the segment.



Divertor Design Approach Relies on Community Interaction and Innovative Solution to Maximize Performance

PFC and Physics Community Interaction

- Tungsten as plasma-interactive material
- ALPS liquid divertor option collaboration
- Fully radiative divertor to maintain reasonable peak heat fluxes, $\sim 5 \text{ MW/m}^2$

Provide Guidance
for R&D

e.g. MHD Effects for Liquid Metal Cooled Divertor

- Minimize MHD effect by design choice; use of coatings, insulating inserts or SiC pipes
- However, solution must be confirmed by R&D

Divertor Coolant Compatible with Blanket Coolant and/or Power Cycle Fluid

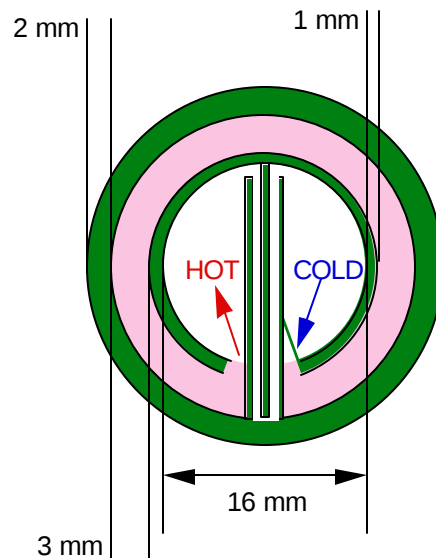
- ARIES-RS: Li in insulated channel (same coolant as blanket)
- ARIES-ST: He coolant (from power cycle)+high heat flux porous media (Pb-17Li as blanket coolant)
- ARIES-AT: Pb-17Li in SiC/SiC channel (same coolant as blanket)

- Assess Key Limiting Issue
- Detailed Analysis and Innovative Solution to Maximize Performance of Coolant/Material/Concept Combination

ARIES-ST Divertor Designed for Thermal Expansion Accommodation

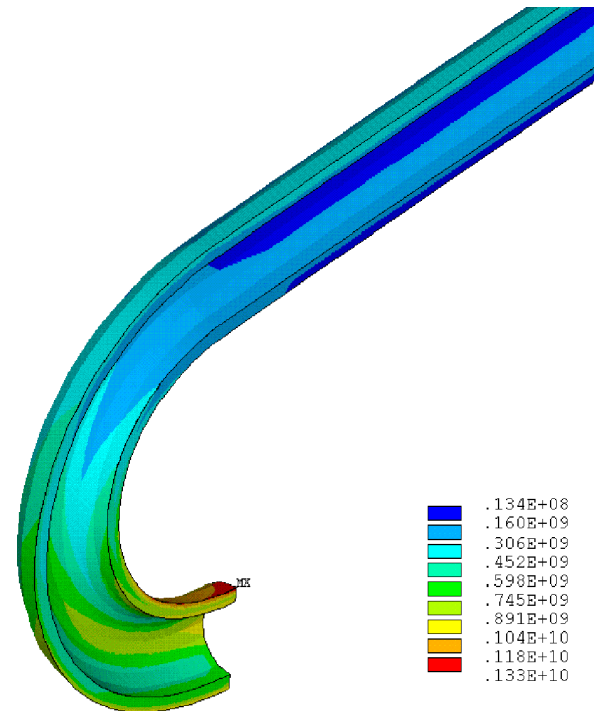
- Tungsten Armor
- High-temperature He coolant
- Advanced high heat flux porous media
- Several SBIR proposals based on similar configuration
- Initial high heat flux testing at Sandia indicate high heat flux capability for this material combination ($\sim 30 \text{ MW/m}^2$)

ARIES-ST
Divertor Tube
Cross Section



3-D stress analysis

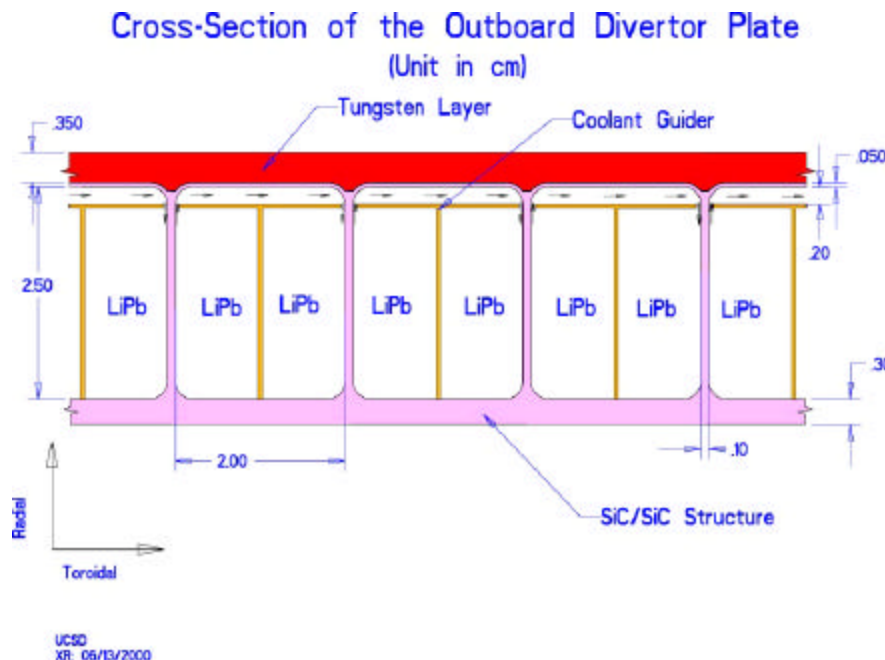
- Moderate stresses in high heat flux region
- High local stress at attachment, can be relieved by flexible joint



MHD Effects Influence Both Pressure Drop and Heat Transfer Even in Insulated Channels

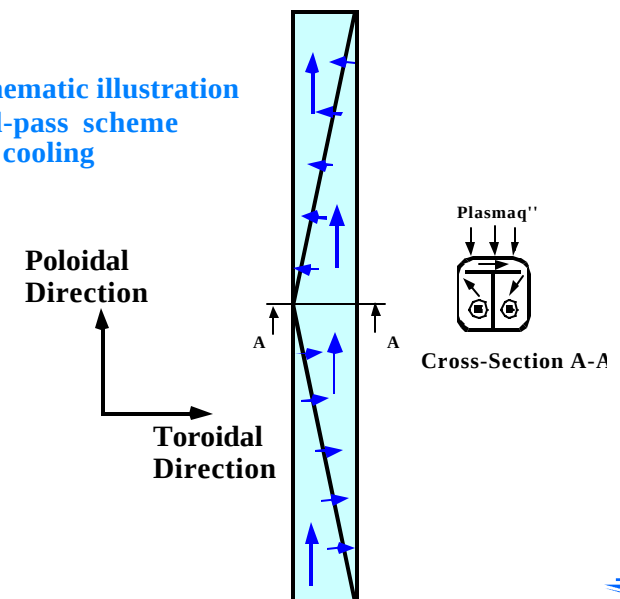
MHD Accommodation Measure for ARIES-AT Divertor Design

- Minimize Interaction Parameter (<1) (Strong Inertial Effects)
- Flow in High Heat Flux Region Parallel to Magnetic Field (Toroidal)
- Minimize Flow Length and Residence Time
- Heat Transfer Analysis Based on MHD-Laminarized Flow

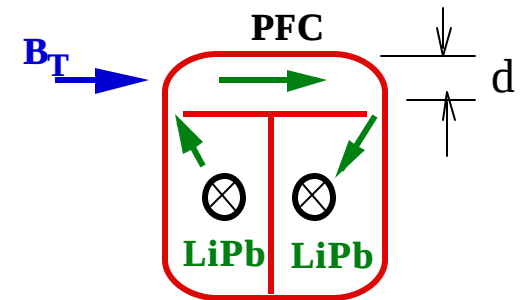
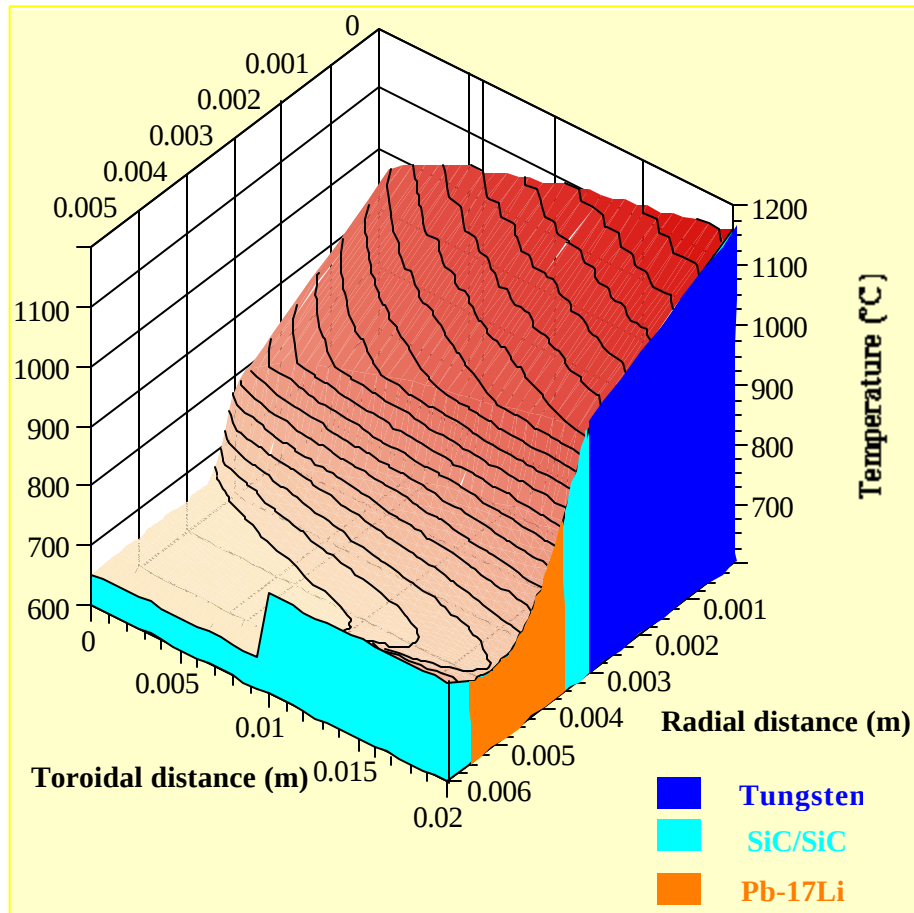


Pb-17Li Poloidal Flow in ARIES-AT Divertor Header

Example schematic illustration of 2-toroidal-pass scheme for divertor cooling



Temperature Distribution in Outer Divertor PFC Channel Assuming MHD-Laminarized Pb-17Li Flow

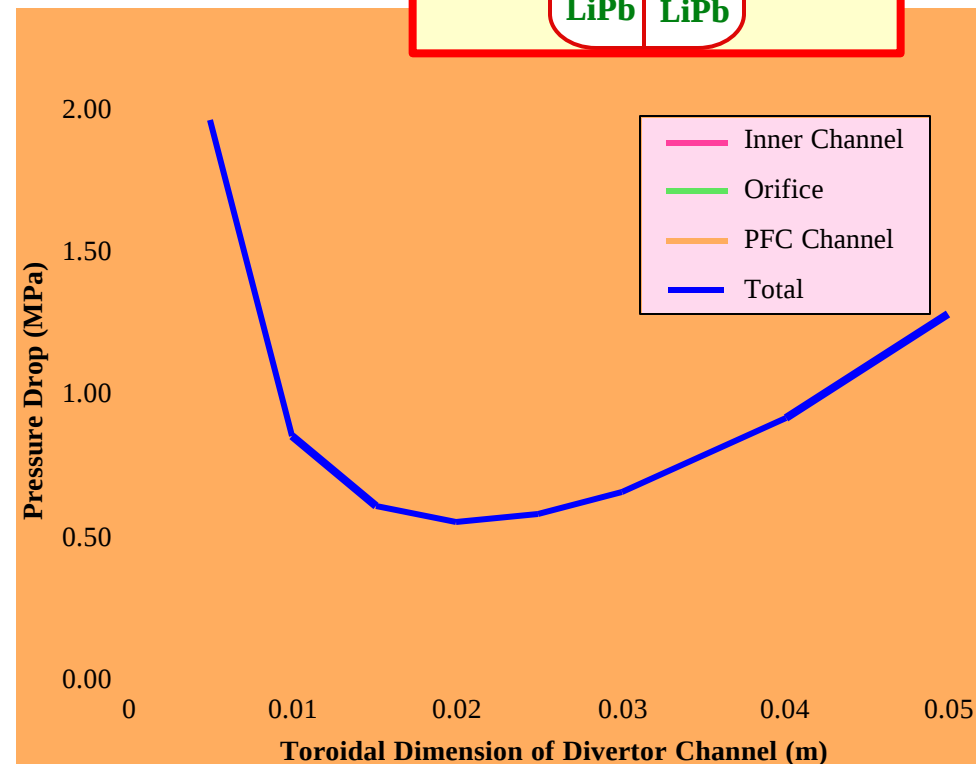
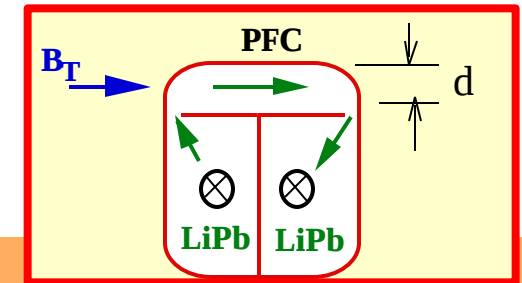
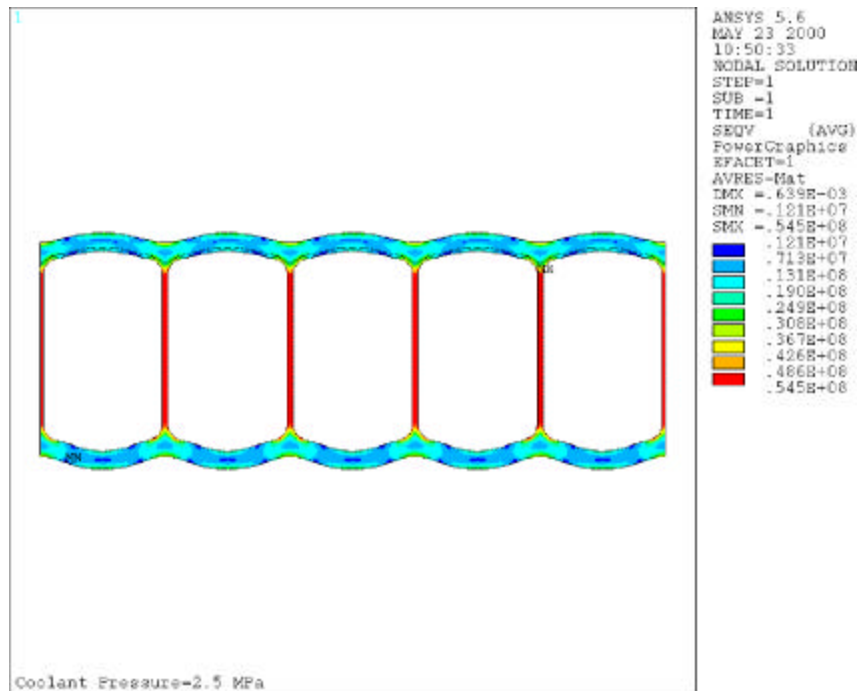


- Moving Coordinate Analysis
- Inlet Temperature = 653°C
- W Thickness = 3 mm
- SiC/SiC Thickness = 0.5 mm
- Pb-17Li Channel Thickness = 2 mm
- SiC/SiC Inner Wall Thick. = 0.5 mm
- Pb-17Li Velocity = 0.35 m/s
- Surface Heat Flux = 5 MW/m²
- Max. SiC/SiC Temp. = 1000°C

Divertor Design Optimized for Stress Limit Accommodation and Acceptable Coolant Pressure Drop

Example ARIES-AT Divertor Analysis

- For 2.5 mm tungsten, SiC/SiC pressure stress ~ 35 MPa (combined SiC/SiC pressure + thermal stress ~ 190 MPa)
- DP is minimized to ~ 0.55 MPa



Close Interaction with International Material and Blanket Design and R&D Communities

Combination of Low Activation Structural Material + Liquid Breeder Result in Attractive, High Performance Blankets

- ARIES-RS: Li + Vanadium; ARIES-ST: Pb-17Li+FS+He; ARIES-AT: Pb-17Li+SiC/SiC

Recent Example of Interaction with International Material and Design Communities

- **Organize International Town Meeting to bring together international (US, EU and Japan) material and design SiC/SiC communities (ORNL, Jan 2000)**
 - Current material development and characterization status
 - Latest SiC/SiC-based blanket design: TAURO(EU), DREAM(Japan()), ARIES-AT(US)
 - Key SiC/SiC issues affecting blanket performance
 - Detailed info on website (<http://aries.ucsd.edu/PUBLIC/SiCSiC/>)
- **Town Meeting was very successful; achievements include:**
 - Develop list of properties and parameters for design study
 - Clear R&D need for high temperature high performance blanket
 - Need better-quality material with reasonable thermal conductivity-stoichiometry goal
 - Temperature limit: Compatibility between Pb-17Li and SiC at high temperature
 - Included in US R&D plan and being carried out in Europe
 - Paper deriving from meeting submitted to FE&D