

Advanced Chamber Concept with Magnetic Intervention:

- Ion Dump Issues**
- Status of Blanket Study**

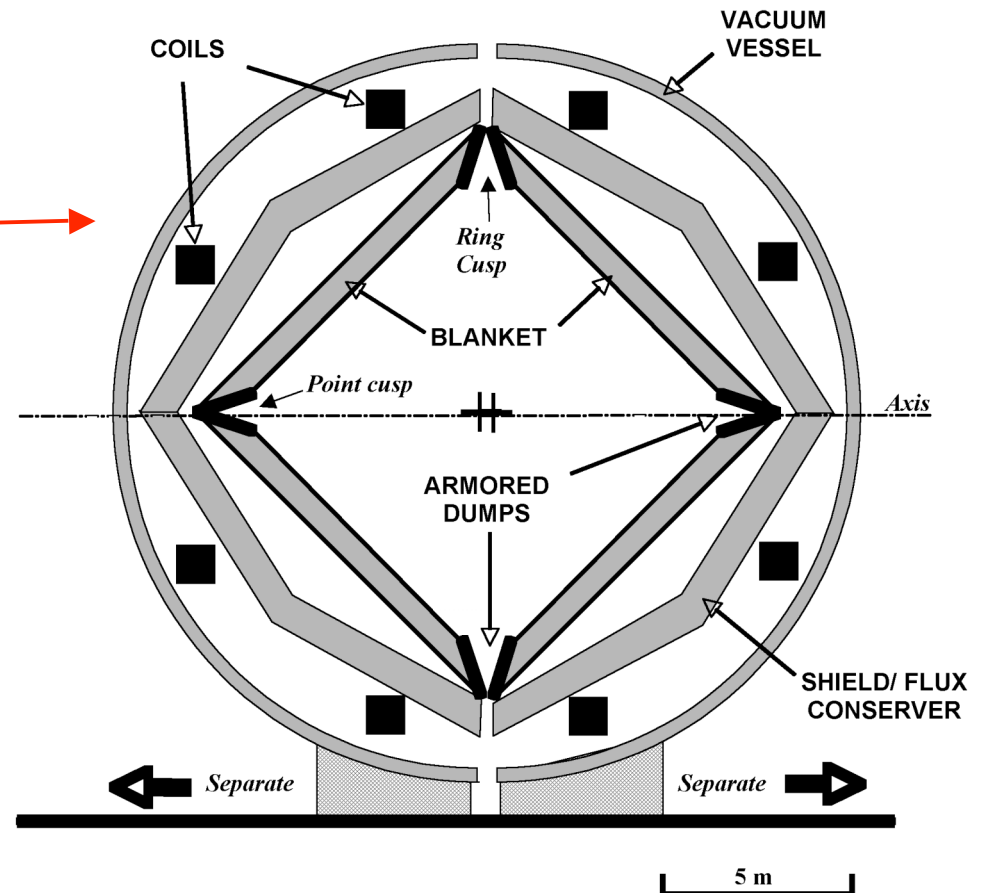
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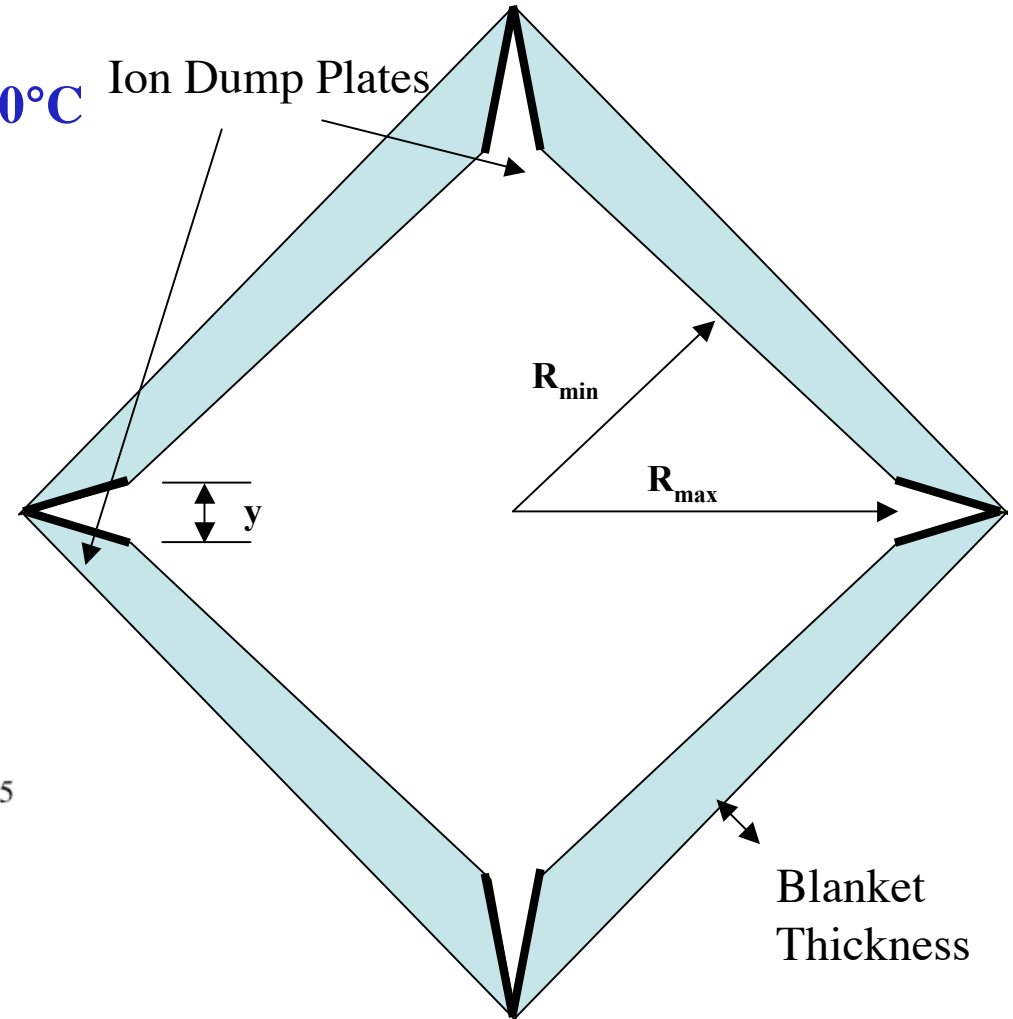
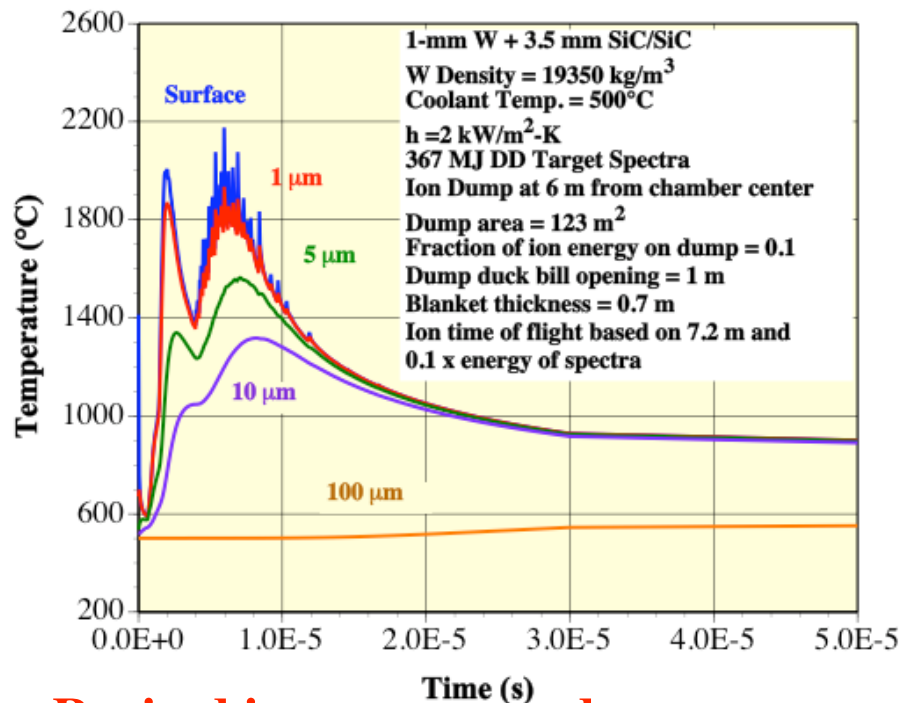
Advanced Chamber Based on Magnetic Intervention Concept Using Cusp Coils (from last time)

- Use of resistive wall (e.g SiC) in blanket to dissipate magnetic energy (*>90% of ion energy can be dissipated in the walls*).
- Initial chamber schematic from Bertie Robson (with cone-shaped chamber blanket concept).
- The initial configuration was rotated 90° for the blanket analysis as this seems to favor the maintenance scheme.
- Dump plates to accommodate all ions but at much reduced energy (*<10%*).
- Dump plates could be replaced more frequently than blanket.



Ion Energy Deposition and Thermal Response of Dump Plates Estimated for Cone-Shaped Chamber

- For example case with $\sim 10\%$ of ion energy on plate, max. W temp. $\sim 2200^\circ\text{C}$



- Revised ion energy on dumps:
 - $\sim 7.7\%$ within $0.5\ \mu\text{s}$
 - $\sim 23\%$ over $0.5\text{-}1.5\ \mu\text{s}$
- Major change, $\sim 30\%$ ion energy on dumps
- If dry wall dump within chamber, need $\sim 30\%$ of chamber area for dump
- Then, why not design whole chamber the same way?

Seems More Advantageous to Position Dump Plate In Separate Smaller Chamber

Ion Dump Ring chamber

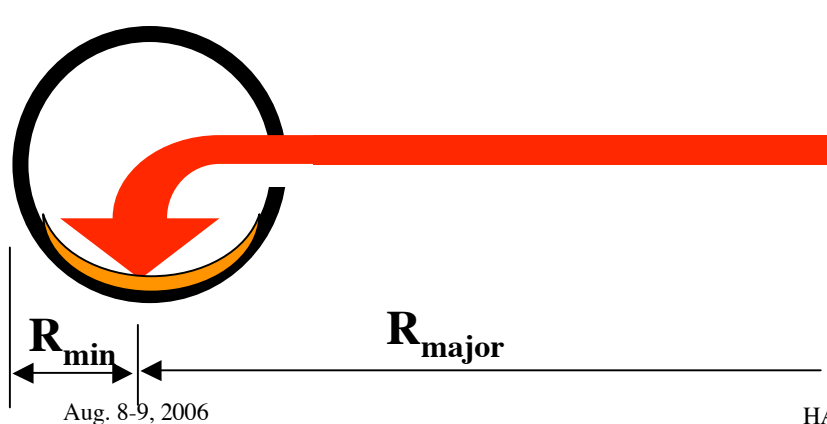
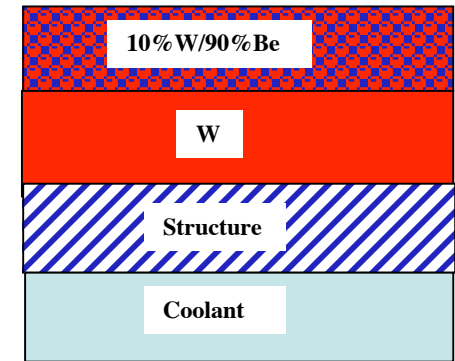


- Could use W dry wall dump, but would require large surface area and same problem with thermomechanical response and He implantation
- Could allow melting (W or low MP material in W)

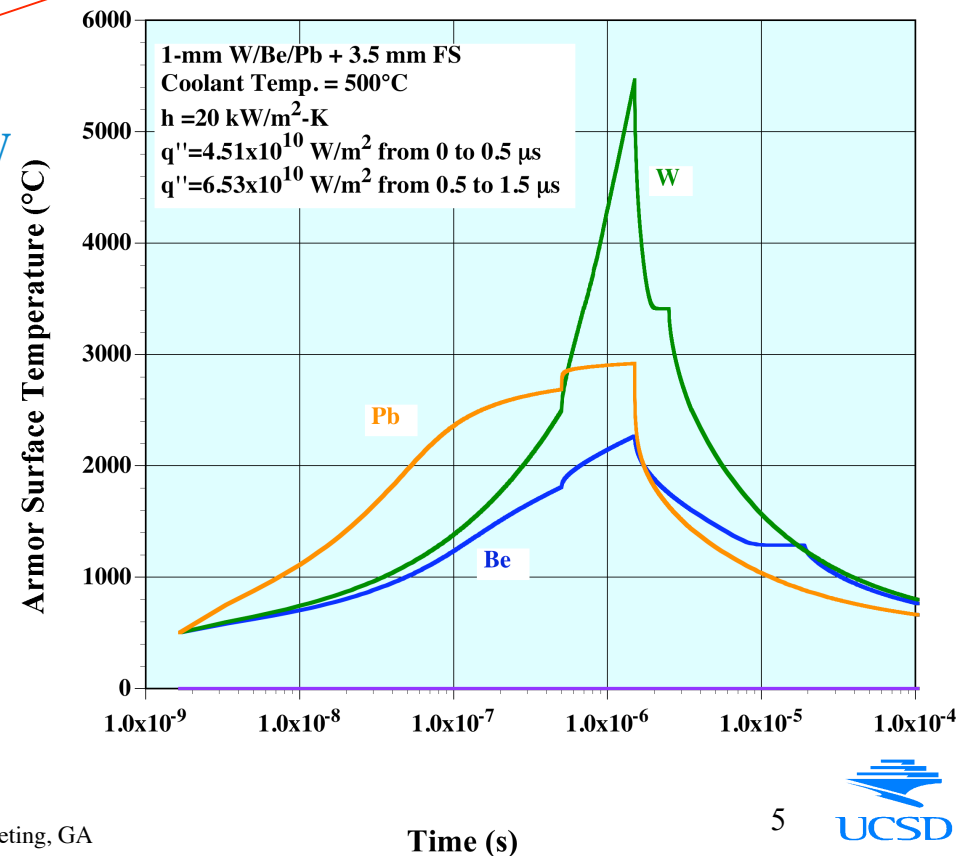
- Dry wall chamber to satisfy target and laser requirements
- Separate wetted wall chamber to accommodate ions and provide long life
- Have to make sure no unacceptable contamination of main chamber

Scoping Analysis of an Example Ring Chamber

- Some flexibility in setting chamber major and minor radii so as not to interfere with laser beams
- e.g., with $R_{\text{major}}/R_{\text{minor}} = 8/2.7$ or $9/2.4$ m, and assuming 35% of wetted wall area sees ion flux with a peaking factor of 1:
 - Ion dump area = 300 m^2
 - From 0 to $0.5 \text{ } \mu\text{s}$, $q'' = 4.53 \times 10^{10} \text{ W/m}^2$
 - From 0.5 to $1.5 \text{ } \mu\text{s}$, $q'' = 6.56 \times 10^{10} \text{ W/m}^2$
- Three cases:
 - W with phase change
 - Low MP metal (e.g. Be) in high porosity W (~80-90%) which provides integrity and could help retain Be melt layer
 - Wetted wall chamber with Pb as example material

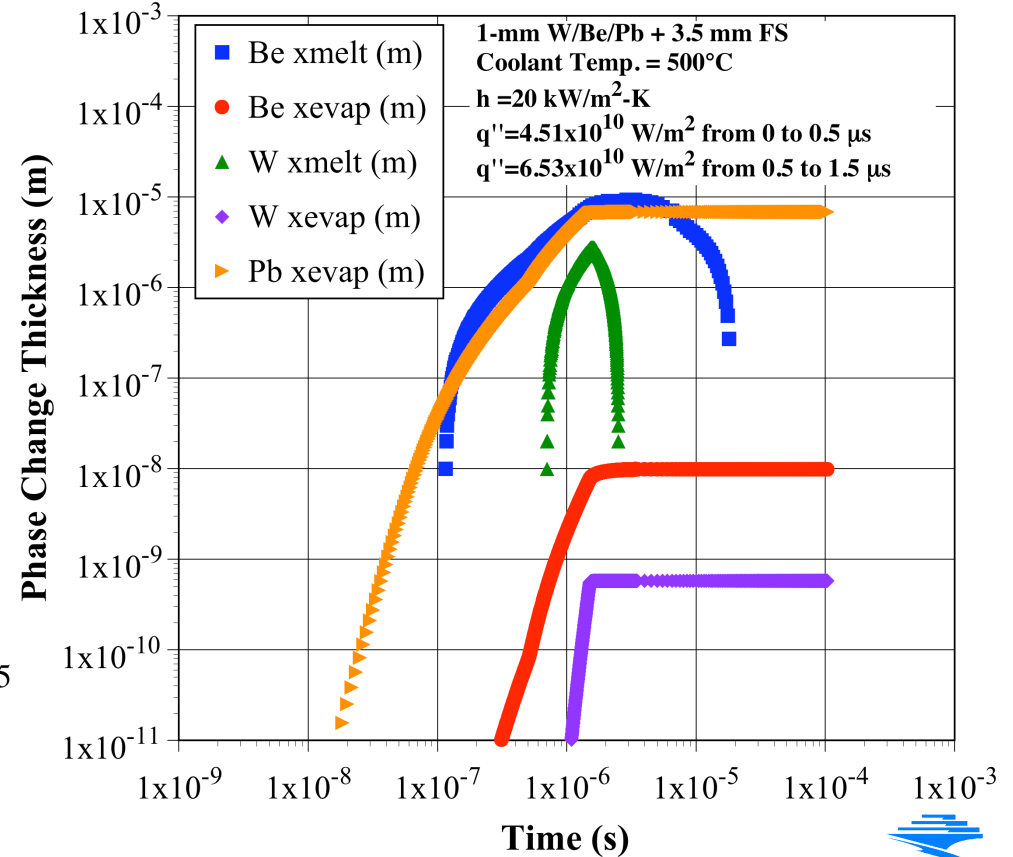
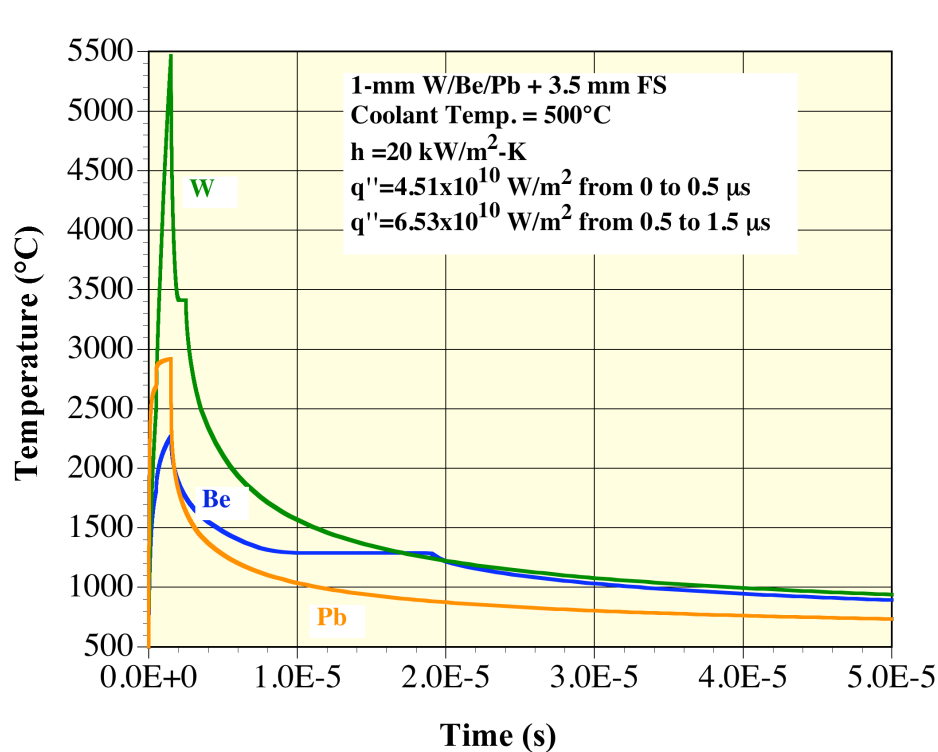


HAPL meeting, GA



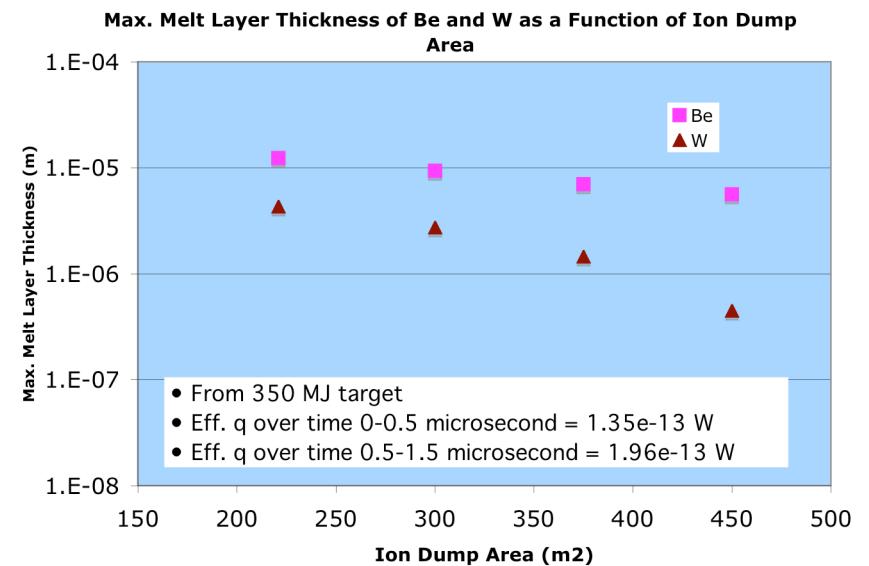
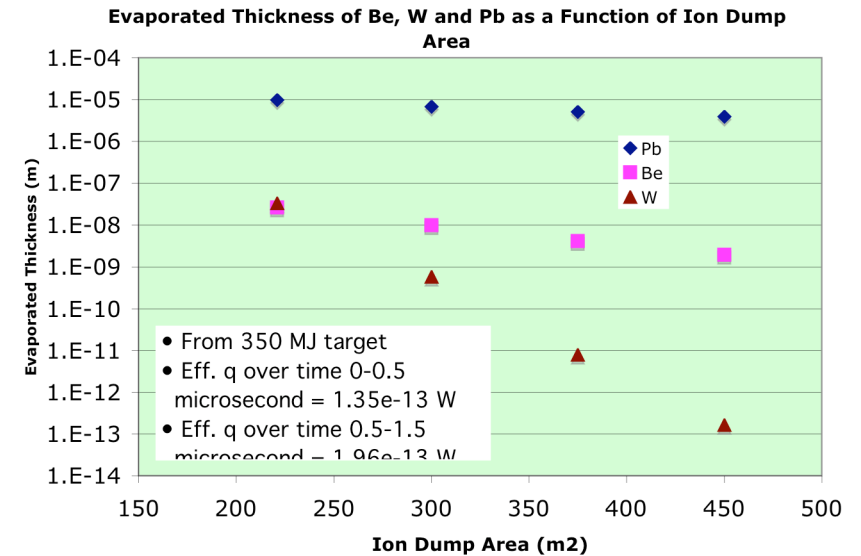
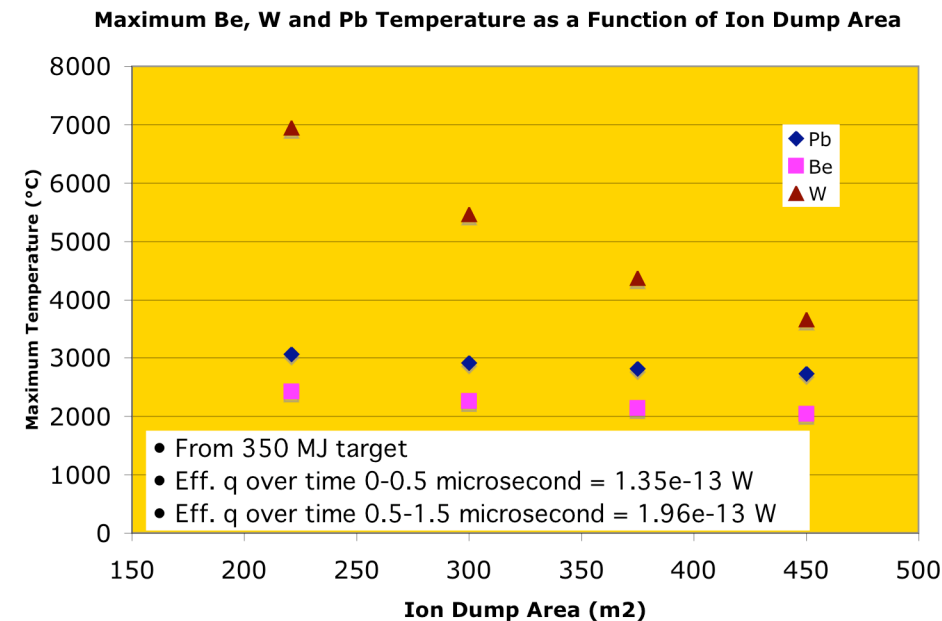
Temperature and Phase Change Thickness Histories for W, Be and Pb for Example Case

- 350 MJ target (ion energy = 87.8 MJ)
- Ion dump area = 300 m²
- From 0 to 0.5 μ s, $q'' = 4.53 \times 10^{10}$ W/m² (7.7% of ion energy)
- From 0.5 to 1.5 μ s, $q'' = 6.56 \times 10^{10}$ W/m² (22.3% of ion energy)



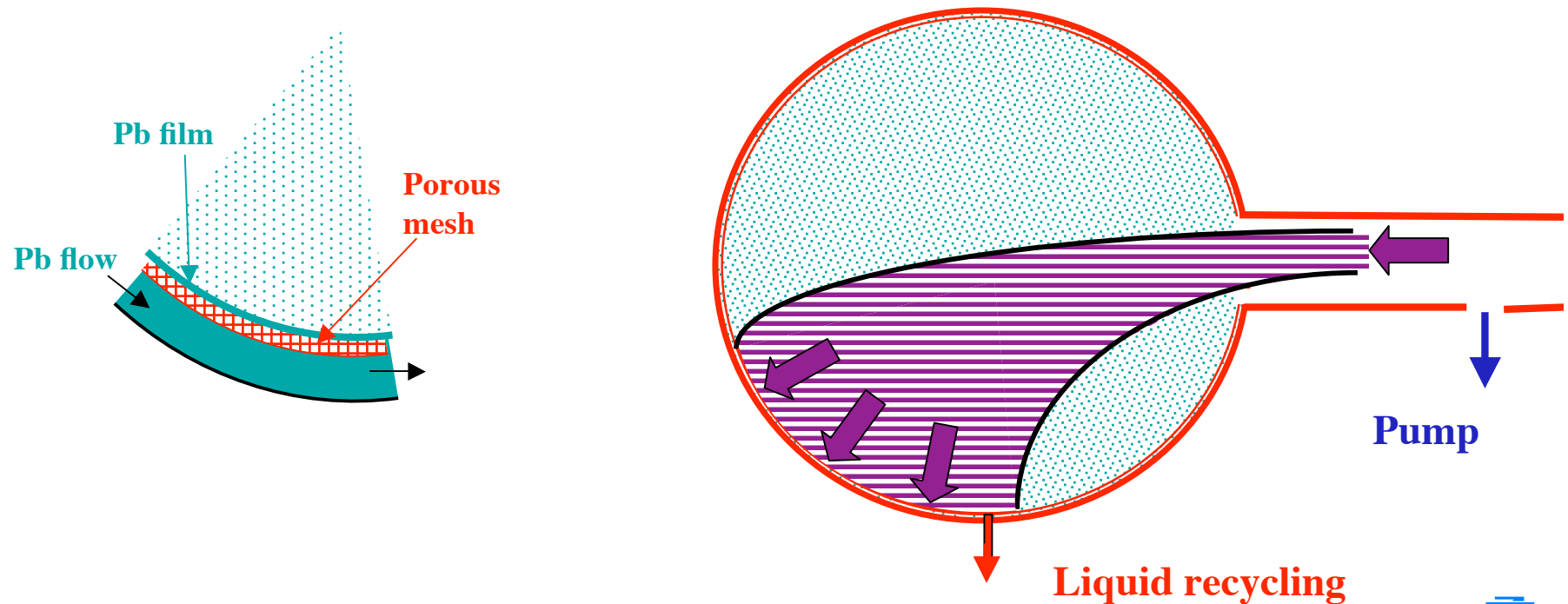
Maximum Temperature and Phase Change Thicknesses for W, Be and Pb as a Function of Ion Dump Area

- 350 MJ target (ion energy = 87.8 MJ)
- Evaporation loss per shot relatively modest for W but could be a concern for Be (1 nm/shot ~ 0.43 mm/day)
- Stability of melt layer is a concern
- Would Be in a porous W matrix be more stable?
- For wetted wall in particular, the evaporated material (e.g. Pb) must recondense within a shot and not contaminate main chamber

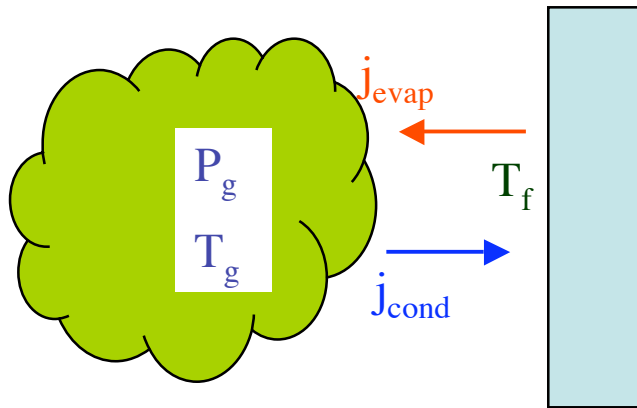


Wetted-Wall Concept Could Consist of a Porous Mesh Through Which Pb Oozes to Form a Protective Film

- Need to make sure that protective film is reformed prior to each shot
 - radial flow through porous mesh
 - circumferential flow of recondensed Pb
 - no concern about any droplets falling in chamber



Film Condensation in Ion Dump Chamber



Example Scoping Calculations

- Ion energy from 350 MJ target = 87.8 MJ
 - 7.7% of ion energy to dump over 0-0.5 μ s
 - 22.3% of ion energy over 0.5-1.5 μ s
- Evaporated thickness and vapor temperature rise from ion energy deposition in ion dump chamber
- Liquid Pb as film material
- Conservatively small ion deposition area = 220 m²
 - e.g. 35% of chamber with $R_{\text{major}} = 8$ m and $R_{\text{minor}} = 2$ m

$$j_{\text{net}} = \left(\frac{M}{R^2} \right)^{0.5} \left(\frac{P_g}{T_g^{0.5}} \right) \left(\frac{P_f}{T_f^{0.5}} \right)$$

j_{net} = net condensation flux (kg/m²-s)

M = molecular weight (kg/kmol)

R = Universal gas constant (J/kmol-K)

ϕ = correction factor for vapor velocity towards film

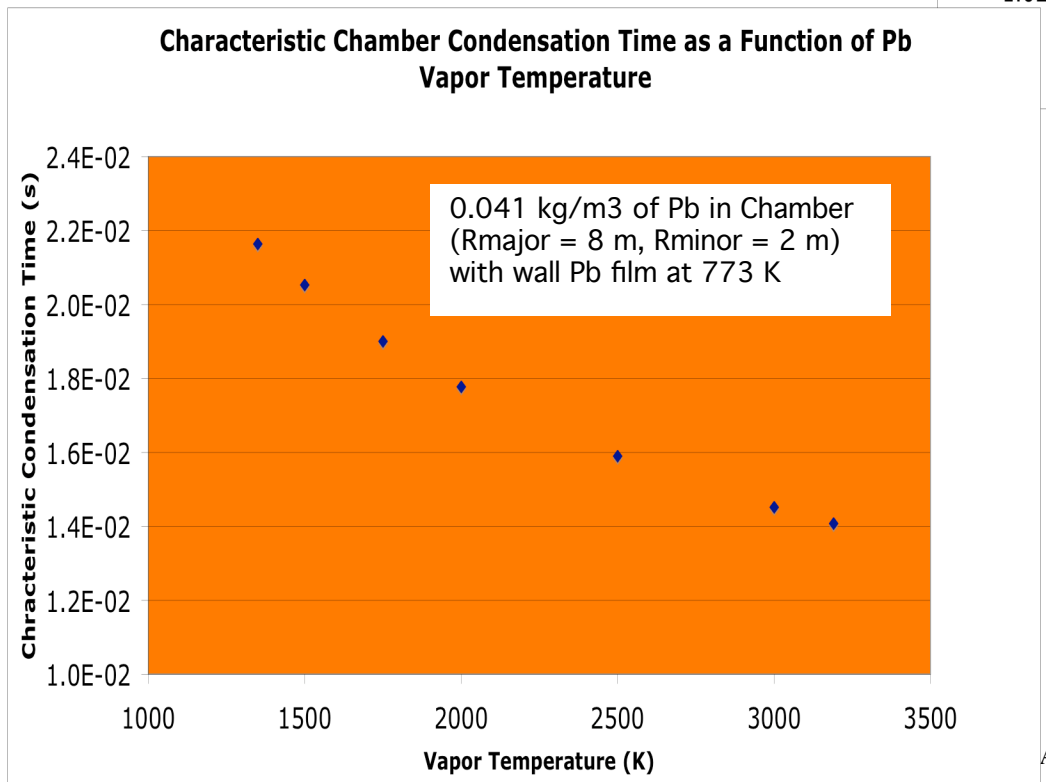
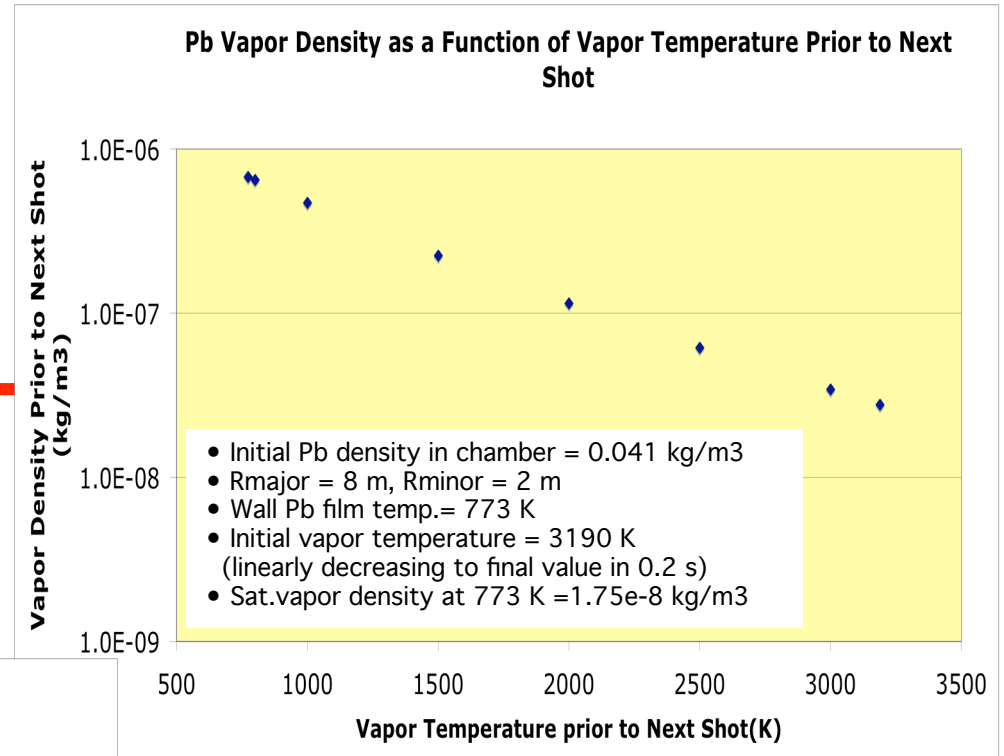
ϕ_c, ϕ_e = condensation and evaporation coefficients

P_g, T_g = vapor pressure (Pa) and temperature (K)

P_f, T_f = saturation pressure (Pa) and temperature (K) of film

Scoping Analysis of Pb Condensation in Example Ring Chamber

- Characteristic condensation time very fast, $\sim 0.01\text{-}0.02$ s



- Depending on final vapor temperature, vapor density prior to next shot is about 1-10 times higher than saturated vapor density at assumed wetted wall temperature of 773 K (1.75×10^{-8} kg/m³ or ~ 0.01 mTorr at ST)

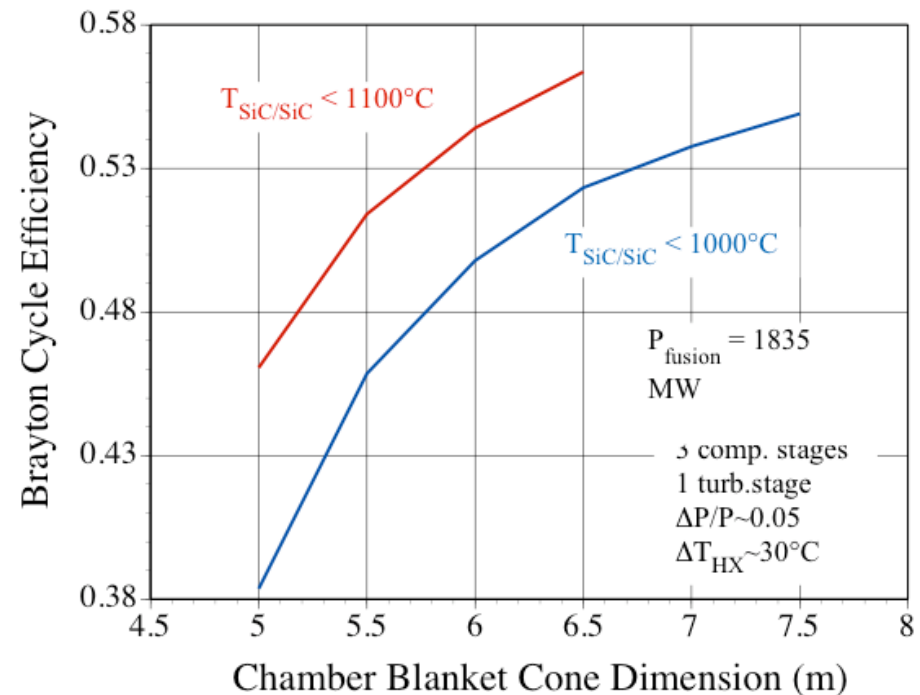
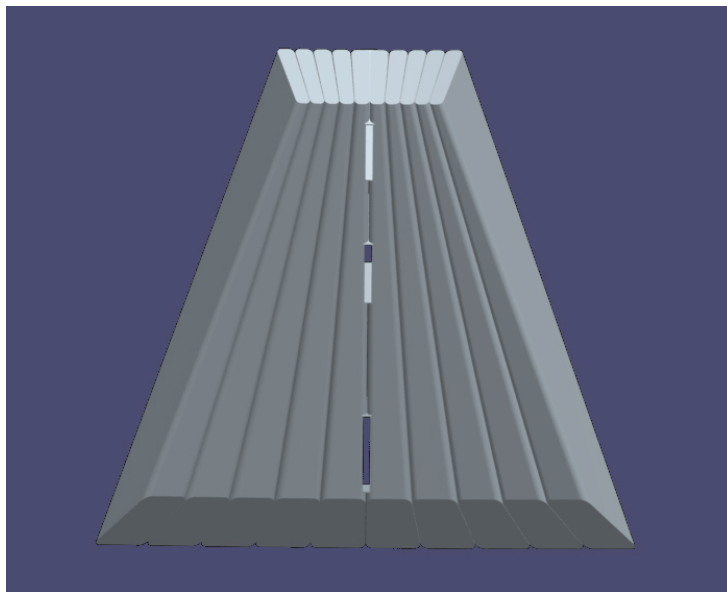
Status of Blanket Study for Magnetic Intervention Chamber

- **More detailed study of blanket using Pb-17Li and SiC_f/SiC**
 - Neutronics
 - Fabrication
 - Assembly and maintenance
 - Thermal-hydraulics
- **Initial study of blanket using flibe and SiC_f/SiC**
 - Possible configurations
 - Neutronics

To be reported by M. Sawan and G. Sviatoslavsky

Self-Cooled Blanket Concept Coupled to a Brayton Cycle (Pb-17Li + SiC_f/SiC and Flibe + SiC_f/SiC)

Blanket	Rchamber	Max. SiC T	Max. SiC/Cool T	Coolant Tin	Coolant Tout	Coolant DP	Cycle eff.
Pb-17Li	6 m	1000°C	900°C	483°C	799°C	~0.3 MPa	50%
Pb-17Li	6 m	1100°C	950°C	580°C	930°C	~ 0.3 MPa	55%
Flibe	6 m	1000°C	912°C	519°C	700°C	~1 MPa	46%
Flibe	6 m	1100°C	1010°C	590°C	790°C	~1 MPa	50%



- From simple estimate for flibe with same blanket configuration as Pb-17Li:
 - Flibe low Re and poor heat transfer properties result in lower cycle η and higher ΔP for given SiC_f/SiC T_{max} constraint.
- Need to perform analysis for optimized flibe configuration

Summary

- **Scoping study of self-cooled Pb-17Li + SiC_f/SiC blanket concept for use in the magnetic-intervention cone-shaped chamber geometry completed**
- **Initial study of flibe + SiC_f/SiC blanket started, needs to be completed based on neutronics calculations and optimized configuration**
- **Separate dump chamber with melted solid wall or wetted wall assessed for magnetic intervention case**
 - Much relaxed atmosphere requirements for separate dump chamber
 - Encouraging results as condensation is very fast
 - Need to ensure no unwanted contaminants in main chamber
 - Need more detailed design of dump chamber configuration including how to recycle liquid for wetted wall concept
- **Future work**
 - Complete flibe+SiC_f/SiC blanket scoping study
 - More detailed design of separate dump chamber