#### Deuterium Ice Layering and Target Injection Studies



D. R. Harding University of Rochester Laboratory for Laser Energetics HAPL Meeting Atlanta, GA 5–6 February 2004



- Update on target-layering efforts
- Target-heating issues
  - response of an OMEGA target to ambient radiation (experiment and model)
  - demonstrate a Monte Carlo model used to estimate gas dynamic loads on an IFE target
    - to define parameter space for experiments
  - planned experiments

# We quantified the accuracy and repeatability of the ice layering and measurement process

We have determined:

- the accuracy threshold of shadowgraphy (CTHS system)
  - ~0.3  $\mu$ m value obtained for a "near perfectly smooth" reference
- the repeatability of the ice-roughness measurement process (7 repeats of a single view)
  - $\pm$ **0.11** µm (95% confidence limit)
  - variables: target vibration, focusing, internal ice defects
- the repeatability of the ice-*layering* process (6 repeats)
  - constant solidification rate (controlled Q<sub>in</sub>, Q<sub>out</sub> and ∆Temp)
  - $\pm$ 0.5  $\mu$ m (smoothest region <2  $\mu$ m); 0.7  $\mu$ m (roughest region ~4  $\mu$ m)
- the ice roughness distribution in the capsule is repeatable

### Submicron rms ice layers were demonstrated; the smoothest layers were confined to a localized region of the target



# The variation in the ice roughness is repeatable AND correlates with the *hole* in the layering sphere



Average of three separate layers.

# The primary source of the azimuthal roughness variation appears to be the illumination nonuniformity

- Layering D<sub>2</sub> ice requires uniform IR radiation integrating sphere.
- The largest source of nonuniformity is the "hole" used to insert and remove the target.
- The effect of the "shadow" on the ice thickness is quantified using ray tracing and a thermal model.
  - Concerns: It causes an initial variation in the ice layer thickness.
    - The target relayers as it is rotated (to acquire 3-D information).

# The lack of illumination from the "hole" causes a mostly uniform 2% decrease in volumetric heating



The focusing effect of the ice and internal reflection from the interior ice surface are responsible for this behavior.

### The nonuniform heat load creates an ice rms roughness of ~4 $\mu$ m



The geometry of the layering sphere/viewing system allows a varying fraction of the perturbed region to be viewed, depending upon the target rotation

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# Target smoothness deteriorated at temperatures more than 1 K below the triple point

• Higher heat loads AND slower cooling rates produced smoother layers 1.7 K below the triple point.



#### **Increased roughness at lower ice temperatures** is primarily observed in modes 1 and 2



- Target exposure to room temperature depends upon the shroud retraction time (0.05 s to 0.25 s).
  - Gas heats at 5 K/s.
- The measured time for the target to burst equals 45 s.
  - $P_{burst} \sim 12 \text{ atm} \rightarrow T_{target} \sim 38 \text{K}$
- How rapidly does the melt zone propagate?



#### New task—IFE-relevant work: estimate the thermal load on a target injected into an IFE chamber

**Issues:** 

- 1. What is the heat load to the target?
  - First step: Monte Carlo calculation of the gas dynamics
    - determine atom flux and temperature ranges
    - effect of sticking probability and accommodation coefficient
    - attempt to measure these values
- 2. How does the ice layer respond to this heat load?
  - CFD model
  - planar cryo target experiment

An IFE-scale capsule can be fielded in the LLE target chamber to measure the time to melt/slump.

### IFE has assumed the highest (most conservative) gas-totarget heat load. A lower value may simplify target fabrication

- Assumption: Xe at 1300 K is fully absorbed onto the 18-K surface.
  - Brown et al., 100% adsorption for N<sub>2</sub>, CO<sub>2</sub>, and Ar when  $T_{surface}$  < 25 K and  $T_{gas}$  < 1400 K
  - Baglin et al., ~1% adsorption for H<sub>2</sub>, CH<sub>4</sub>, CO, and CO<sub>2</sub> when T<sub>surface</sub> < 15 K
- Lower adsorption → lower heat load, AND, what if the accommodation coefficient is also <1, an even lower heat load?</li>
- An insulating outer foam layer would protect the target, but this may not be needed. We need experimental data.

#### Monte Carlo calculations are used to quantify the effect of gas adsorption and the high thermal accommodation of Xe on the target surface

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### Experimental design requires parameter limits that are obtained from calculations

Goal:

- 1. Generate a molecular beam of hot Xe atoms
- 2. How does a cryogenic target respond to the flux?

Status:

- 1. Scale the problem correctly—currently
- 2. Engineering design

### Equipment concept and expected performance



### Currently: (a) Monte Carlo calculation to confirm molecular beam estimates (downstream of nozzle).

(b) heat load calculation



- 1. High-quality ice layers have been demonstrated
- 2. Potential cause of roughness variation in a target identified engineering solution planned
- 3. Ice becomes rougher only > 1 K below the triple point—primarily low modes (1, 2, and 3), may be mitigated by a slow cooling rate (0.5 mK/min)—need more statistics
- 4. Designing a molecular beam nozzle to measure IFE-scaled gas-heating loads on cryogenic targets